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# **VERIFICACIÓN ESTRUCTURAL DE UNA ANTENA GSM FRENTE A ESFUERZOS DE VIENTO**



Memoria y Anejos

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## Resumen

El trabajo realizado abarca el estudio estructural de una antena de telecomunicaciones GSM y su respuesta al esfuerzo de viento al que se encuentra sometida.

A lo largo del análisis llevado a cabo, entre otros, se ha empleado el uso de normativa europea actualmente vigente con el objetivo de corroborar la certeza del resultado obtenido en relación con si resiste o no la estructura. Dicha normativa de uso ha sido destinada al cálculo de la fuerza resultante de viento, teniendo en cuenta tanto factores estructurales como ambientales y topográficos de la zona en la que se halla la antena objeto de estudio.

Una vez calculada dicha fuerza, se ha procedido al análisis tridimensional mediante *Cype 3D*, un programa empleado para el cálculo de estructuras. Con *Cype 3D*, se ha analizado la respuesta de la antena frente a los valores de tensión calculados y sacado las condiciones de contorno post ataque de viento, dejando lugar finalmente a conclusiones y valoración de resultados obtenidos.

## Resum

El treball realitzat abasta l'estudi estructural d'una antena de telecomunicacions GSM i la seva resposta a l'esforç de vent al qual es troba sotmesa.

Al llarg de l'anàlisi dut a terme, entre altres, s'ha emprat l'ús de normativa europea actualment vigent amb l'objectiu de corroborar la certesa del resultat obtingut en relació amb si resisteix o no l'estructura. Aquesta normativa d'ús ha estat destinada al càlcul de la força resultant de vent, tenint en compte tant factors estructurals com ambientals i topogràfics de la zona en la qual es troba l'antena objecte d'estudi.

Una vegada calculada aquesta força, s'ha procedit a l'anàlisi tridimensional mitjançant *Cype 3D*, un programa emprat per al càlcul d'estructures. Amb *Cype 3D* s'ha analitzat la resposta de l'antena enfront dels valors de tensió calculats i tret les conclusions de contorn post atac de vent, deixant lloc finalment a conclusions i valoració de resultats obtinguts.



## Abstract

The work carried out encompasses the structural study of a GSM telecommunications antenna and its response to the wind effort to which it is subjected.

Throughout the analysis carried out, among others, the use current European regulations has been used in order to corroborate the certainty of the results obtained in relation to whether or not it resists the structure. Such rules of use have been intended for the calculation of the resulting wind force, taking into account both structural and environmental and topographical factors of the area in which the antenna under study is located.

Once this force has been calculated, three-dimensional analysis has been carried out using *Cype 3D*, a program used for the calculation of structures. With *Cype 3D*, the antenna response against calculated force values has been analyzed and the post-wind attack contour conditions resulted, finally leaving room for conclusions and assessment of results obtained.

## Agradecimientos

Se reconoce el esfuerzo, las ganas y la motivación enfocada a la correcta realización de la tesis del tutor de esta, Víctor Martínez Valverde. Con su ayuda las horas dedicadas han sido tanto fructíferas como educativas.

También dar las gracias a familiares, amigos y, especialmente, a mi pareja Aina, con la que juntos hemos compartido muchas horas de trabajo y diversión.

Finalmente, mencionar al consejo medioambiental del *Maresme* y a la empresa de telecomunicaciones *Cellnex*, por los datos otorgados y el trato mostrado.

## Glosario

Para los fines de este documento se aplican los siguientes símbolos.

Letras latinas mayúsculas:

$A$	área
$A_{ref}$	área de referencia
$B^2$	factor de respuesta de fondo
$F_w$	fuerza de viento resultante
$I_v$	intensidad de turbulencia
$R^2$	parte resonante de la respuesta
$Re$	número de Reynolds
$R_h, R_b$	admitancia aerodinámica
$S_L$	función de densidad espectral de potencia adimensional

Letras latinas minúsculas:

$b$	anchura de la estructura (la longitud de la superficie perpendicular a la dirección del viento si no se especifica otra cosa)
$c_d$	coeficiente dinámico
$c_{dir}$	factor direccional
$c_e(z)$	coeficiente de exposición
$c_f$	coeficiente de fuerza
$c_{f,o}$	coeficiente de fuerza en estructuras o elementos estructurales sin flujo libre de cola (esbeltez infinita)
$c_p$	coeficiente de presión
$c_{prob}$	factor de probabilidad
$c_r$	factor de rugosidad

$c_o$	coeficiente topográfico
$c_{season}$	factor estacional
$e$	excentricidad de una fuerza o distancia al borde
$f_L$	frecuencia adimensional
$h$	altura de la estructura
$k_p$	factor de pico
$n_{1,x}$	frecuencia fundamental de vibración en la dirección del viento
$n$	frecuencia natural
$p$	probabilidad anual de excedencia
$q_b$	presión correspondiente a la velocidad media de referencia (básica)
$q_p$	presión correspondiente a la velocidad de pico
$v_m$	velocidad media del viento
$v_{b,0}$	valor fundamental de la velocidad básica del viento
$v_b$	velocidad básica del viento
$x$	distancia horizontal de un lugar desde la cima de una cresta
$z$	altura sobre el suelo
$z_0$	longitud de rugosidad
$z_e$	altura de referencia para la acción externa del viento
$z_{m\acute{a}x}$	altura máxima
$z_{m\acute{i}n}$	altura mínima
$z_s$	altura de referencia para la determinación del factor estructural

Letras minúsculas griegas:

$\delta$	decremento logarítmico del amortiguamiento
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$\delta_a$	decremento logarítmico del amortiguamiento aerodinámico
$\delta_d$	decremento logarítmico del amortiguamiento debido a dispositivos especiales
$\delta_s$	decremento logarítmico del amortiguamiento estructural
$\varphi$	relación de solidez
$\nu$	frecuencia media de oscilación
$\Theta$	dirección del viento
$\rho$	densidad del aire
$\sigma_v$	desviación típica de la turbulencia



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# **1. Prefacio**

## **1.1. Origen del trabajo**

A medida que transcurre el tiempo, se opta por rapidez y economía dejando de lado la precisión. Se toma como referencia la unidad de tiempo sin prestar demasiada atención a los pequeños detalles que pueden ocasionar grandes consecuencias.

En el ámbito de las estructuras, dicha mencionada precisión es un parámetro de gran importancia con relación al confort y, sobre todo, a la seguridad. La mayor parte de las estructuras albergan zonas y/o caminos de transcurso para individuos, razón por la cual no se debe de menospreciar la estabilidad de la construcción y la firmeza de su configuración.

Hasta la fecha se han observado multitud de fallos estructurales con consecuencias desastrosas: Edificios derruidos por vibraciones sísmicas, puentes derrumbados por pandeo lateral e incluso elementos arrasados por fatiga de las vigas constituyentes del esqueleto. Este tipo de accidentes deberían de poder preverse con las acciones de mantenimiento adecuadas o, incluso no originarse, resultado de un buen estudio previo y un análisis de factores externos pertinente al caso en concreto.

## **1.2. Motivación**

La confianza esperada tanto en estructuras metálicas como en marquesinas y en otros tipos de conformación es el motivo del estudio realizado cuyo fin pretende demostrar, con un análisis muy particular, pero con conclusiones y valoraciones generalizadas, la validez de cálculo empleado y las carencias y/o excesos presentes en la construcción y diseño actual.

## **1.3. Requerimientos previos**

Para una correcta indagación en el estudio de las condiciones de viento que afectan a la antena en particular, se ha tenido que adquirir cierta información relevante para la realización de cálculos.

Esta información está basada, en gran parte, en datos meteorológicos de la localidad en la que se encuentra situada la estructura (mediciones de viento, variaciones de temperatura, etc.) y en el dimensionamiento de esta, incluyendo los tipos de vigas, auxiliares y refuerzos pertenecientes.

## 2. Introducción

El trabajo presentado comprende, tal y como su título indica, la verificación estructural de una antena de telecomunicaciones en la localidad de *Dosrius, Barcelona* frente a los esfuerzos de viento actuantes en la zona en la que se encuentra.



*Ilustración 1. Antena GSM (Fuente: Alberto Lloveras)*

Se tienen en cuenta los condicionantes del medioambiente, entendiéndose por estos a las mediciones de temperatura, factores topográficos según el terreno y valores de velocidad de viento, y estructurales propios de la construcción objeto de estudio.

Añadiendo al esqueleto de la estructura los auxiliares (antenas parabólicas, cableados, etc.) que, en parte conforman su función de existencia, estos también tienen un papel relevante al equilibrio y fortaleza de la obra.

La normativa de uso a lo largo del trabajo ha sido la norma UNE-EN 1993-3-1<sup>1</sup>, para el caso concreto de la evaluación de torres y mástiles, y UNE-EN 1991-1-4<sup>2</sup>.

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<sup>1</sup> (European Standard, 2006)

<sup>2</sup> European Standard, 'Acciones Generales de Viento', 2007.

## **2.1. Alcance**

Con relación a la estructura desnuda, se han tenido en cuenta las dimensiones geométricas, los tipos de perfil y el material empleado en su construcción.

Paralelamente, referente a los auxiliares constituyentes, se han tenido en consideración todas las antenas individuales de la estructura, el tubo/soporte del pararrayos y la escalera de mantenimiento situada en un lateral de la estructura.

Por último y no menos importante, los factores ambientales afectantes a la antena, tanto los del año en vigor como los de años pasados, han sido valorados de manera coherente y productiva. Estos factores son representantes de valores de velocidad, temperatura, alturas, coordenadas geográficas y presiones, entre otros muchos.

### 3. Análisis geométrico

Primeramente, previo a cualquier cálculo, es necesario analizar las dimensiones de la estructura. Estas han sido proporcionadas por la empresa encargada de su instalación, *Cellnex Telecom*, cuyos planos proporcionados se encuentran en el anejo B del proyecto.

Para obtener resultados más precisos a cerca de la resistencia al viento de la antena, esta se ha distribuido en tramos a medida que sube verticalmente. De esta manera, no solo se presenta un único valor de fuerza del viento sino cinco, que es el número de tramos estudiados.

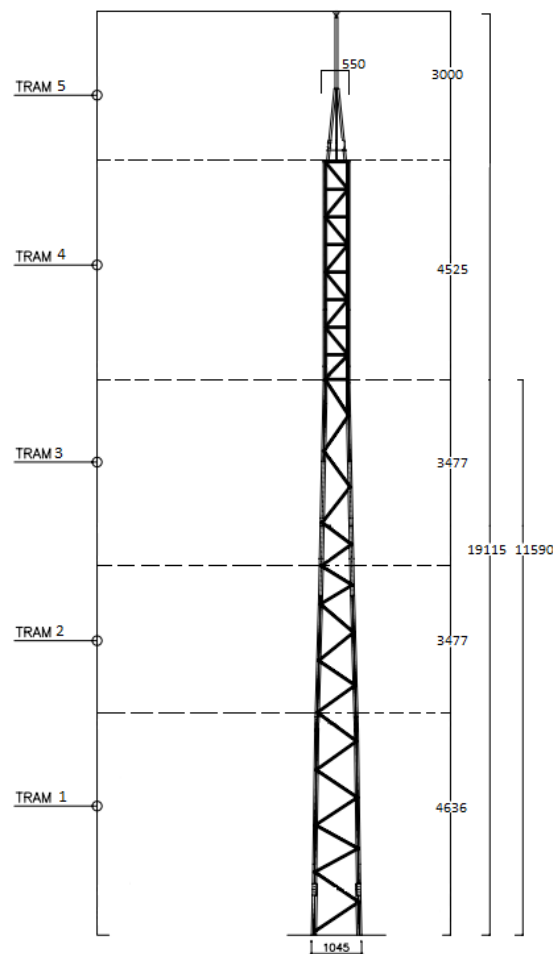


Ilustración 2. Dimensionado y distribución de la antena (Fuente: Cellnex)

En la anterior ilustración pueden observarse las alturas en milímetros de cada uno de los tramos organizados como la anchura de la base de la antena y la superior, la cual permanece constante a lo largo de todo el cuarto tramo. Ahora bien, en el resto de los tramos (a excepción del tramo 5, perteneciente únicamente al tubo/soporte del pararrayos sin influencia estructural alguna) presentan un cierto grado de inclinación a medida que se alza la estructura en el eje vertical.

### 3.1. Ángulo de inclinación

Por trigonometría, se ha substraído el valor constante del ángulo de inclinación de la antena de los tramos 1, 2 y 3.

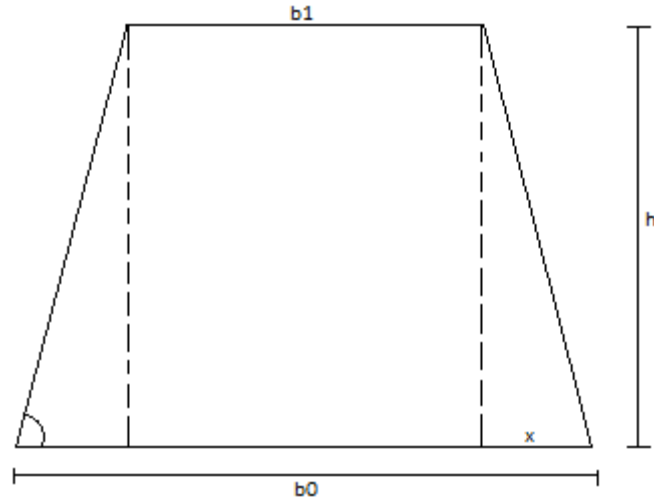


Ilustración 3. Esquema de cálculo del ángulo de inclinación

Según el esquema presentado, la fórmula que obtendrá el ángulo de inclinación será la siguiente:

$$\alpha = \text{Arctan}\left(\frac{h}{x}\right) \quad \text{donde} \quad x = \frac{b_0 - b_1}{2} \quad (1)$$

Por lo tanto, teniendo en cuenta que  $h = 11590\text{mm}$ ,  $b_0 = 1045\text{mm}$  y que  $b_1 = 550\text{mm}$ :

$$x = 247,5\text{mm} \rightarrow \alpha = 88,78^\circ$$

### 3.2. Anchura de tramo

Las alturas individuales de cada tramo se presentan en la ilustración 2. En referencia a la anchura de los tramos 1, 2 y 3, esta se ha obtenido mediante trigonometría:

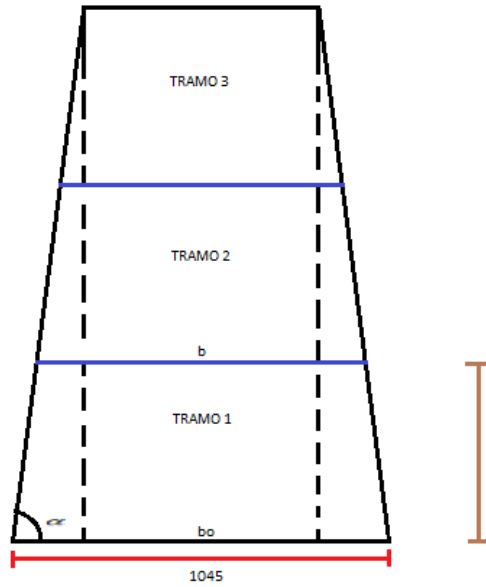


Ilustración 4. Esquema de cálculo del ancho de tramo

Según el esquema de la ilustración 4, el cálculo del ancho  $b$  de tramo queda resumido de la siguiente manera:

NOTA – El ancho de tramo referente a cada sección se ha tomado como la base de esta, es decir, el ancho superior del tramo de estudio.

$$b = \frac{(-2) \cdot h}{\operatorname{tg} \alpha} + b_0 \quad (2)$$

donde

$b$  es el ancho del tramo de estudio.

$b_0$  es el ancho del tramo anterior.

$\alpha$  es el ángulo de inclinación de la estructura, definido en el apartado 3.1.

$h$  es la altura del tramo de estudio.

TRAMO	b (mm)
1	1.045,00
2	896,50
3	748,00
4	550,00
5	550,00

Tabla 1. Ancho de tramo

NOTA – La ecuación 2 del cálculo de ancho de tramo es únicamente válida para los tramos 1, 2 y 3. Para el resto de los tramos, la amplitud viene definida en el apartado 3 y permanece constante en toda su longitud.

### 3.3. Componentes estructurales

Serán necesarios, por lo que concierne al dimensionado, las medidas de longitud y anchura de todos los tipos de perfiles constituyentes: Diagonales, horizontales, montantes y de refuerzo.

Para ello y con las referencias de perfiles obtenidas de *Cellnex Telecom*, se ha hecho uso del catálogo de “*Perfiles y Barras comerciales*”<sup>3</sup> perteneciente a la compañía *ArcelorMittal*, la mayor compañía metalúrgica mundial.

	Perfil		
	Diagonal	Horizontal	Montante
TRAMO 1	L 45 x 45 x 4	-	L 100 x 100 x 8 L 90 x 90 x 8
TRAMO 2	L 45 x 45 x 4	-	L 80 x 80 x 8
TRAMO 3	L 45 x 45 x 4	-	L 80 x 80 x 8
TRAMO 4	L 45 x 45 x 4	L 45 x 45 x 4	L 70 x 70 x 6

Tabla 2. Perfiles de la estructura

La nomenclatura de los perfiles de la tabla 2 es la siguiente: *ancho x ancho x espesor*. Dado que son de caras iguales, el valor del ancho es el mismo en ambas caras.

Los perfiles de las vigas de la antena son todos perfiles angulares de lados iguales. Estos constan de una gran cantidad de peculiaridades frente a otros tipos de perfiles, pero en relación con los valores/características útiles para los cálculos posteriores solo nos interesan sus medidas de longitud y anchura y distribución de peso por unidad de longitud.

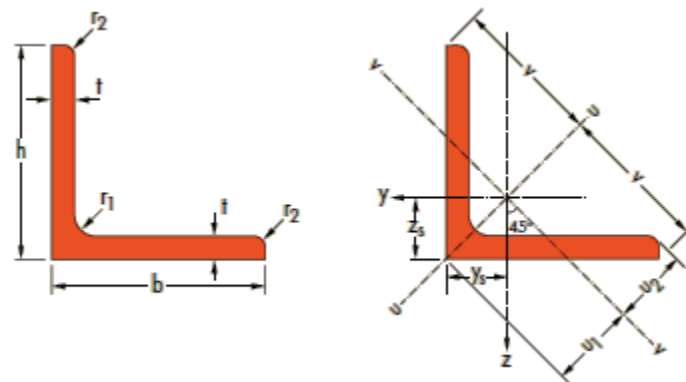


Ilustración 5. Perfil angular de lados iguales (Fuente: ArcelorMittal)

La anchura de la cara de cada uno de los perfiles, al igual que el peso de estos por unidad de longitud, viene mencionada en el catálogo de *ArcelorMittal*, pero la longitud, medida no proporcionada en los planos adjuntos, depende de la disposición de la estructura.

<sup>3</sup> Arcelormittal Europe and Long Products, ‘Perfiles y Barras Comerciales’, 2017.

### 3.3.1. Perfiles diagonales

Una vez obtenido el ángulo de inclinación en el apartado 3.1., se procede al cálculo de la longitud de los perfiles diagonales de la estructura, cuya separación vertical permanece constante entre perfil y perfil.

Por medio del empleo del programa AUTOCAD, un software de diseño asistido por computadora, y el esquema de dibujo del contorno de la estructura, considerando el grado de inclinación de esta calculado anteriormente, ha sido posible la determinación de las longitudes de cada diagonal.

Estas, en la tabla mostrada a continuación, van enumeradas de la 1 a la 22, comenzando desde aquella situada más cerca del suelo hasta la más alta de la estructura.

Elementos diagonales		
longitud (mm)	nº	Tramo perteneciente
1185.50	1	1
1161.40	2	
1140.90	3	
1117.40	4	
1096.10	5	
1076.00	6	
1054.80	7	
1033.40	8	
1012.80	9	2
993.20	10	
972.20	11	
953.40	12	
932.40	13	
913.60	14	
893.90	15	3
875.00	16	
856.40	17	
838.40	18	
820.30	19	
802.90	20	
743.30	21	4
795.69	22 (x7)	

Tabla 3. Longitudes de las diagonales

El área perpendicular a la acción del viento sobre la cara de estudio de la antena equivaldrá al área de un rectángulo de, en el caso de los perfiles en diagonal, 45mm de ancho y de longitudes diferentes para cada uno de los perfiles existentes.

$$\text{Área} = \text{base} \times \text{altura}$$

(3)



	Perfiles diagonales		
	ancho (mm)	longitud (mm)	área (mm <sup>2</sup> )
TRAMO 1	45	8865,50	398947,50
TRAMO 2	45	5777,60	259992,00
TRAMO 3	45	5086,90	228910,50
TRAMO 4	45	6313,14	284091,48

Tabla 4. Área perfiles diagonales

Referente a la masa de cada perfil, se ha tomado el valor  $G$  (kg/m) proporcionado por *ArcelorMittal*. Mediante el producto de la longitud por dicho valor mencionado es posible la determinación del peso de los perfiles pertenecientes a la estructura:

$$M(kg) = G(kg/m) \cdot L(m) \quad (4)$$

	Diagonales			
	Perfil	L (mm)	G (kg/m)	M (kg)
TRAMO 1	L 45 x 45 x 4	8865.50	2,74	24,29
TRAMO 2	L 45 x 45 x 4	5777,60	2,74	15,83
TRAMO 3	L 45 x 45 x 4	5086,90	2,74	13,94
TRAMO 4	L 45 x 45 x 4	6313,14	2,74	17,30

Tabla 5. Masa perfiles diagonales

### 3.3.2. Perfiles horizontales

Los nueve perfiles horizontales, debido a que estos solo están presentes en el tramo 4, cuya anchura permanece constante en toda su altura, tienen una longitud de valor igual al ancho del tramo, de 550 mm.

De nuevo, al igual que en los perfiles diagonales, con el uso de la expresión 3 del área para un rectángulo, ha sido posible la determinación de la altura de los perfiles horizontales:

	Perfiles horizontales			
	ancho (mm)	longitud (mm)	Unidades	área (mm <sup>2</sup> )
TRAMO 1	-	-	-	-
TRAMO 2	-	-	-	-
TRAMO 3	-	-	-	-
TRAMO 4	45	550	9	222750

Tabla 6. Área perfiles horizontales

En cuanto al cálculo de la masa, esta se da por medio de  $G$  y las longitudes de los perfiles:

	Horizontales			
	Perfil	L (mm)	G (kg/m)	M (kg)
TRAMO 1	-	-	-	-
TRAMO 2	-	-	-	-
TRAMO 3	-	-	-	-
TRAMO 4	L 45 x 45 x 4	4950	2,74	13,56

Tabla 7. Masa perfiles horizontales

NOTA – Obsérvese que estos perfiles están únicamente presentes en el cuarto tramo de la estructura.

### 3.3.3. Perfiles montantes

Los perfiles montantes de la torre de celosía serán evaluados de la siguiente manera: Al existir un perfil de refuerzo montante en los primeros 8 metros de la estructura, de la mano de la seguridad, en este primer trecho se tomará en cuenta únicamente el perfil de refuerzo, dando paso al perfil montante a partir del final del segmento. Entonces, en los tramos 1 y 2 y en una pequeña parte del tramo 3 no se atenderá a su influencia.

De nuevo, con el uso de las reglas trigonométricas, somos capaces de determinar la longitud diagonal en sentido vertical ascendente de los perfiles montantes de la estructura.

Conociendo el ángulo de inclinación y las medidas de los tramos escogidos podemos dar con su longitud en diagonal por tramo de estudio:

$$Longitud = \frac{\text{altura del tramo}}{\text{sen}(\alpha)} \quad (5)$$

	Montantes
	longitud (mm)
TRAMO 3	3155,72
TRAMO 4	4526,03

Tabla 8. Longitudes de los montantes

NOTA – El valor de la longitud del tramo 3 es la diferencia entre la longitud del montante en todo el tramo y la del de refuerzo en el mismo tramo, distancia del cual es evaluada en el apartado 3.3.4.

Todos los tramos tienen un único tipo de perfil montante a excepción del primer tramo. Este, en sus primeros 950 mm, consta de un tipo de perfil mientras que, en sus restantes 3686 mm este cambia.

Aplicando la formulación del área y de la masa definidas por las ecuaciones 3 y 4, respectivamente:

	Perfiles montantes		
	ancho (mm)	longitud (mm)	área ( $mm^2$ )
TRAMO 3	3.155,72	80,00	252.457,54
TRAMO 4	4.526,03	70,00	316.822,21

Tabla 9. Área perfiles montantes

	Montantes			
	Perfil	L (mm)	G (kg/m)	M (kg)
TRAMO 3	L 80 x 80 x 8	3.155,72	9,63	30,39
TRAMO 4	L 70 x 70 x 6	4.526,03	6,38	28,88

Tabla 10. Masa perfiles montantes

NOTA – Obsérvese que en el primer tramo constan dos tipos de perfil de montantes.

### 3.3.4. Perfil de refuerzo

En apartados anteriores se ha mencionado un tipo de perfil de refuerzo del cual no se han proporcionado datos algunos. Este tipo de perfil está destinado a la protección de la construcción dada la posible circunstancia de fallo estructural de los elementos de esta.

Es un refuerzo del tipo LPN 90.9 que se extiende 8435 mm en vertical. De la misma manera que hemos calculado las longitudes de los perfiles montantes calculamos la del perfil de refuerzo junto con su área y masa.

	Refuerzo
	Longitud (mm)
TRAMO 1	4.637,06
TRAMO 2	3.477,79
TRAMO 3	322,07

Tabla 11. Longitudes del perfil de refuerzo

	Perfiles de refuerzo		
	ancho (mm)	longitud (mm)	área ( $mm^2$ )
TRAMO 1	4.637,06	90,00	417.335,12
TRAMO 2	3.477,79	90,00	313.001,34
TRAMO 3	322,07	90,00	28.986,61
TRAMO 4	-	-	-

Tabla 12. Área perfiles de refuerzo

	Refuerzo			
	Perfil	L (mm)	G (kg/m)	M (kg)
TRAMO 1	LPN 90.9	4.637,06	12,2	56,57
TRAMO 2	LPN 90.9	3.477,79	12,2	42,43
TRAMO 3	LPN 90.9	322,07	12,2	3,93
TRAMO 4	-	-	-	-

Tabla 13. Masa perfiles de refuerzo

NOTA – Nótese la falta de perfil de refuerzo en el tramo 4, sección a la cual no llega dicho componente.

### 3.4. Auxiliares

En cada una de las caras de la antena existen todo tipo de auxiliares: desde antenas Wifi hasta módulos RRU.

Gracias a la empresa *Cellnex* contamos con información relevante a estos elementos acerca de su distribución en la antena. Entonces, al haber dividido la estructura en cinco secciones distintas es también posible identificar a qué tramo pertenecen cada uno de los auxiliares pertenecientes.

Modelo	Localización	Altura (m)	Área (m <sup>2</sup> )	Tramo	Cara Antena
Antena Panel	Cara Torre 308º	17.00	0,40	5	3
Antena Panel	Cara Torre 038º	17.00	0,03	5	4
Antena Parábola	Cara Torre 128º	16.00	0,07	4	1
Antena Panel	Cara Torre 308º	16.00	0,40	4	3
Antena Panel	Cara Torre 308º	15.00	0,40	4	3
Antena Panel	Cara Torre 308º	15.00	0,40	4	3
Antena Panel	Cara Torre 038º	14.00	0,40	4	4
Antena Panel	Cara Torre 038º	14.00	0,40	4	4
Antena Panel	Cara Torre 038º	14.00	0,40	4	4
Antena Parábola	Cara Torre 128º	14.00	1,13	4	1
Antena Panel	Cara Torre 128º	14.00	0,05	4	1
Antena Panel	Cara Torre 038º	14.00	0,40	4	4
Antena Parábola	Cara Torre 218º	13.00	0,28	4	2
Antena Parábola	Cara Torre 218º	13.00	0,07	4	2
Antena WI-FI	Cara Torre 218º	13.00	0,05	4	2
Antena Panel	Cara Torre 038º	13.00	0,14	4	4
Antena WI-FI	Cara Torre 128º	12.00	0,05	4	1
Antena Panel	Cara Torre 308º	10.00	0,49	3	3
Antena Panel	Cara Torre 308º	10.00	0,49	3	3
Módulo RRU	Cara Torre 308º	10.00	0,24	3	3
Módulo RRU	Cara Torre 308º	10.00	0,24	3	3
Módulo RRU	Cara Torre 308º	10.00	0,24	3	3
Módulo RRU	Cara Torre 308º	10.00	0,24	3	3
Antena Panel	Cara Torre 218º	10.00	0,24	3	2
Antena Panel	Cara Torre 128º	8.50	0,40	3	1
Antena Parábola	Cara Torre 218º	6.00	1,13	2	2

Tabla 14. Distribución auxiliares (Fuente: Cellnex)

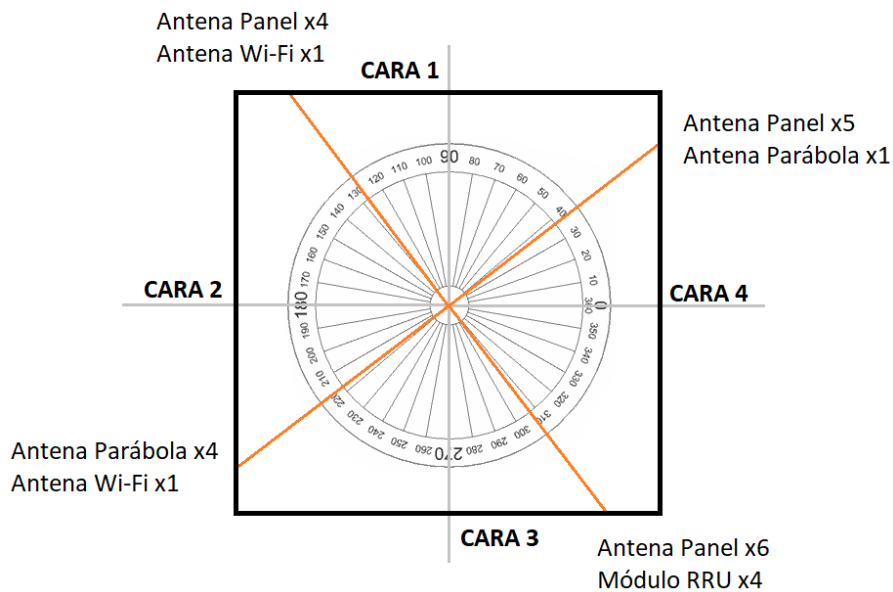


Ilustración 6. Caras de la antena

Por otro lado, lo habitual en el cálculo de las torres de soporte de antenas es incluir la carga al viento de los cables y la escalera de subida como un % estimado extra sobre la superficie de exposición al viento de la estructura. En nuestro caso, se ha establecido un 15 % extra del área estructural sobre el área de los auxiliares en todos los tramos de la torre a excepción del tramo 5 (tubo/soporte pararrayos).

Estos elementos extra se han considerado únicamente en la cara 2 de la estructura, por lo que solo se tendrán en cuenta cuando se evalúe dicha sección.

## 4. Velocidad del viento

El estudio de la velocidad de viento y, consecuentemente el de la fuerza de viento y sus condicionantes en la localización de la torre debe de ser, por norma <sup>4</sup>, mediante el uso de valores medios. Con los resultados obtenidos a partir de estos valores debería de poder tomarse una decisión sólida acerca de la seguridad ofrecida por la estructura.

Por otro lado, la toma de valores medios implica no estimar el posible fallo por condiciones adversas: Cambios bruscos de temperatura, subidas de velocidad de viento y cambios en su dirección, etc.

Al tratarse de una verificación estructural se deben de abarcar todas aquellas situaciones en las que los factores externos puedan exceder el equilibrio de la estructura o incluso provocar su derrumbe. Por lo tanto, en lo que a la velocidad concierna, se han tenido en cuenta valores medios y máximos con el fin de abastecer la norma y el detalle de estudio.

Según la localización de la estructura <sup>5</sup>, la estación meteorológica más cercana es la estación de *Can Massuet, Dosrius*. El instrumento encargado de la medición de la velocidad del viento es el anemómetro que, en esta estación en particular, está a 10m del suelo. Además, los edificios y vegetación próxima a la estación están por debajo de la altura de esta. Este hecho implica que, al no tener obstáculos que impidan el flujo limpio de aire (árboles, edificaciones) se trata, según la tabla 15, de un terreno de categoría II.

Categoría de terreno		$z_0$ m	$z_{min}$ m
0	Mar abierto o zona costera expuesta al mar abierto	0,003	1
I	Lagos o áreas planas y horizontales con vegetación despreciable y sin obstáculos	0,01	1
II	Áreas con vegetación baja, como hierba, y obstáculos aislados (árboles, edificaciones) con separaciones de al menos 20 veces la altura de los obstáculos	0,05	2
III	Áreas con una cobertura de vegetación uniforme o edificaciones o con obstáculos aislados con una separación máxima de 20 veces la altura de los obstáculos (villas, terreno suburbano, bosques permanentes)	0,3	5
IV	Áreas en las que al menos un 15% de la superficie está cubierta por edificios cuya altura media supera los 15 m	1,0	10

Tabla 15. Categoría de terreno (Fuente: UNE-EN 1991-1-4)

Con los datos obtenidos en la estación de *Can Massuet*, se presentan seguidamente los valores de velocidad media y máxima del año en vigor.

NOTA - Los datos recaudados de las velocidades del 2019 carecen de valores en el mes de marzo y diciembre y en ciertos días de los meses de setiembre, octubre y noviembre. Implica pues, que estos datos presentados a continuación no constan de una alta precisión pero que, aun así, son válidos.

<sup>4</sup> Standard, 'Acciones Generales de Viento'.

<sup>5</sup> 'Estaciones Meteorológicas En España - Google My Maps.

NOTA – Los valores diarios a partir de los cuales se han realizado los siguientes cálculos presentados se alojan en los anexos C del proyecto.

Año	Velocidad máx. (km/h)	Fecha	Hora	Velocidad media (km/h)	Fecha
2019	70,92	24-ene	0:02	21,6	19-abr

Tabla 16. Viento 2019

#### 4.1. Factor de probabilidad

Existe un factor que determina la probabilidad  $p$  anual de que se supere la velocidad del viento. Este factor, según norma, viene dado por la siguiente expresión:

$$c_{prob} = \left( \frac{1 - K \cdot \ln(-\ln(1 - p))}{1 - K \cdot \ln(-\ln(0,98))} \right)^n \quad (6)$$

donde

$p$  es la probabilidad anual de que se supere la velocidad del viento.

$K$  es el parámetro de forma que depende del coeficiente de variación de la distribución de los valores extremos considerada. El valor recomendado es de 0,2.

$n$  es el exponente. El valor recomendado es de 0,5.

Primeramente, valoraremos la probabilidad  $p$  anual de ser superada la velocidad del viento. Para ello, es necesario contar con los registros de velocidades de años anteriores, los cuales no nos han sido proporcionados por la estación de *Can Massuet*.

NOTA – El registro de velocidades se encuentra alojado en el anejo C

Por consiguiente, extraídos de la estación de *Arenys de Mar*<sup>6</sup>, la estación más próxima a la estructura de estudio después de la de *Can Massuet*, se presentan los valores medios y máximos de las velocidades de viento registradas a lo largo del siglo XXI:

<sup>6</sup> 'Base de Datos Meteorológica. Consulta de Datos de Viento'.



Año	V. máx. (km/h)	Fecha	Hora	V. media (km/h)	Fecha
2000	63	07-nov	9:30	18	07-nov
2001	105,12	11-nov	4:30	20,16	15-nov
2002	72	04-abr	2:40	14,04	30-abr
2003	83,16	16-oct	21:00	16,92	29-ago
2004	108	03-may	21:10	15,84	03-may
2005	81	10-nov	6:00	15,84	02-dic
2006	78,84	27-feb	3:00	15,84	30-ene
2007	83,16	10-mar	10:50	14,04	23-jul
2008	59,04	26-dic	13:10	11,88	15-ene
2009	79,92	24-ene	9:00	18	24-ene
2010	91,08	07-ene	17:30	14,04	01-ene
2011	59,04	06-nov	10:50	15,12	06-nov
2012	68,04	31-oct	11:10	14,04	30-abr
2013	86,04	01-mar	15:10	18	16-nov
2014	82,08	09-dic	12:40	16,92	30-nov
2015	73,08	22-feb	13:00	12,96	05-jul
2016	74,16	19-dic	22:50	19,08	07-ene
2017	74,16	06-feb	12:40	21,96	22-ene
2018	74,16	01-ene	7:50	16,92	24-mar

Tabla 17. Viento 2000 – 2018 (Fuente: Registro de viento de la estación de Arenys de Mar)

Con los valores anteriormente expuestos, se observa que la velocidad media y máxima del 2019 son superadas en ciertos años anteriores.

La probabilidad  $p$  se puede calcular de la siguiente manera:

$$p = \frac{1}{T} \quad (7)$$

donde

$T$  representa el número de unidades de tiempo que transcurren en promedio entre dos oportunidades en que la variable supere el valor de estudio.

Para el caso de las velocidades máximas, empleando la formulación anterior, tenemos el siguiente resultado:

$$p_{v.máx.} = 0,87$$

En cambio, para las velocidades medias, el valor de esta en el 2019 solo es superado una sola vez a lo largo de todo el siglo. Al no existir un periodo de tiempo en el que se supere dicha velocidad, la probabilidad  $p$  anual de ser superada la velocidad media es nula.

$$p_{v.media} = 0$$

Retomando la ecuación 6 del factor de probabilidad:

$$c_{prob} = \left( \frac{1 - 0,2 \cdot \ln(-\ln(1 - 0,87))}{1 - 0,2 \cdot \ln(-\ln(0,98))} \right)^{0,5} = 0,69$$

## 4.2. Velocidad básica del viento

El valor fundamental de la velocidad básica del viento<sup>7</sup>,  $v_{b,0}$ , es la velocidad media característica del viento. En nuestro caso práctico, valoraremos los dos valores fundamentales: El de la velocidad media y el de la máxima del 2019.

La determinación de la velocidad básica del viento viene definida por la siguiente expresión:

$$v_b = c_{dir} \cdot c_{season} \cdot v_{b,0} \cdot c_{prob} \quad (8)$$

donde

$v_{b,0}$  es el valor fundamental de la velocidad básica, definida en el capítulo 4.

$c_{prob}$  es el factor de probabilidad, definido en el apartado 4.1.

$c_{dir}$  es el factor direccional. El valor recomendado es 1,0.

$c_{season}$  es el factor estacional. El valor recomendado es 1,0.

Con los valores de velocidad del año en vigor (tabla 16) completamos la expresión mostrada:

NOTA – Al ser nula la probabilidad anual de ser superada la velocidad media del 2019, el factor de probabilidad  $c_{prob}$  no se tiene en cuenta en su expresión.

$v_{b,0}$ (m/s)	$c_{prob}$	$v_b$ (m/s)	
19,7	0,69	13,69	V. máxima 2019
6,00	-	6,00	V. media 2019

Tabla 18. Velocidades básicas

## 4.3. Velocidad media del viento

La velocidad media del viento  $v_m(z)$  a una altura  $z$  por encima del terreno, depende de la rugosidad y la orografía, y de la velocidad básica del viento:

$$v_m(z) = c_r(z) \cdot c_o(z) \cdot v_b \quad (9)$$

donde

$v_b$  es la velocidad básica del viento, definida en el apartado 4.2.

$c_r(z)$  es el factor de rugosidad.

$c_o(z)$  es el coeficiente topográfico.

El coeficiente topográfico  $c_o(z)$  se tiene en consideración únicamente cuando nos encontramos en colinas aisladas o en zonas escarpadas. Este tipo de zonas geográficas incrementan la velocidad del

<sup>7</sup> Standard, 'Acciones Generales de Viento'.

viento en más de un 5%, por lo que en estos casos deberá de tenerse en cuenta el coeficiente topográfico.

La estructura de estudio se encuentra situada en lo alto de una región montañosa. Este emplazamiento no da lugar a aumentos de velocidad, motivo por el cual dicho coeficiente topográfico toma el valor de la unidad.

$$c_o(z) = 1$$

#### 4.3.1. Factor de rugosidad

El factor que define la rugosidad del terreno tiene en cuenta la variabilidad de la velocidad media del viento en la localización concreta de la estructura debida a la altura sobre el nivel del suelo.

El procedimiento para calcular el factor de rugosidad  $c_r(z)$  es el siguiente:

$$c_r(z) = k_r \cdot \ln\left(\frac{z}{z_0}\right) \quad \text{para } z_{\min.} \leq z \leq z_{\max.} \quad (10)$$

$$c_r(z) = c_r(z_{\min.}) \quad \text{para } z < z_{\min.} \quad (11)$$

donde

$z_0$  es la longitud de rugosidad, definida por la categoría del terreno.

$z_{\min.}$  altura mínima, definida por la categoría del terreno.

$z_{\max.}$  se toma igual a 200m.

$k_r$  es el factor del terreno, que puede calcularse utilizando:

$$k_r = 0,19 \cdot \left(\frac{z_0}{z_{0,II}}\right)^{0,07} \quad (12)$$

donde

$z_{0,II} = 0,05\text{m}$  (categoría II)

Al tratarse de un terreno de categoría II, este reúne las siguientes condiciones (tabla 15):

Terreno	
tipo	II
$z_0$ (m)	0,05
$z_{\min.}$ (m)	2

Tabla 19. Categoría del terreno

Con estos valores, ya es posible averiguar el valor del factor de terreno:

$$k_r = 0,19 \cdot \left(\frac{0,05}{0,05}\right)^{0,07} = 0,19$$

Al estar la estructura organizada en cinco tramos distintos a diferente altura, dispondremos de cinco factores de rugosidad distintos.

TRAMO	z (mm)
1	4.636
2	8.113
3	11.590
4	16.115
5	19.115

Tabla 20. Alturas por tramo

La tabla 20 muestra la altura máxima en milímetros desde el suelo de cada uno de los tramos de la estructura. En todos los tramos la altura máxima queda comprendida entre 2 y 200, por lo que se hará uso de la primera ecuación de cálculo.

TRAMO	$k_r$	$c_r(z)$
1	0,19	0,86
2		0,97
3		1,03
4		1,10
5		1,13

Tabla 21. Factores de rugosidad

Finalmente, con el hallazgo de estos últimos valores somos capaces de cuantificar la velocidad media del viento por tramo de estudio. Esta, al depender también de la velocidad básica del viento, tendrá dos valores distintos por tramo: Un valor considerando la condición de velocidad media y otro considerando la de velocidad máxima.

	Velocidad media 2019	Velocidad máxima 2019
TRAMO	$v_m(z)$ (m/s)	$v_m(z)$ (m/s)
1	5,16	11,78
2	5,80	13,24
3	6,21	14,17
4	6,58	15,02
5	6,78	15,47

Tabla 22. Velocidades medias

## 5. Turbulencias

La turbulencia equivale a la aparición de pequeños remolinos que viajan en el flujo producto de pequeños movimientos aleatorios en el flujo del aire que se superponen al viento medio.

La intensidad de la turbulencia  $I_v(z)$  es establecida<sup>8</sup> de la siguiente manera:

$$I_v(z) = \frac{\sigma_v}{v_m(z)} \quad \text{para} \quad z_{\min.} \leq z \leq z_{\max.} \quad (13)$$

$$I_v(z) = I_v(z_{\min.}) \quad \text{para} \quad z < z_{\min.} \quad (14)$$

donde

$\sigma_v$  desviación típica de la turbulencia. Puede obtenerse mediante la siguiente expresión:

$$\sigma_v = k_r \cdot v_b \cdot k_1 \quad (15)$$

donde

$k_1$  es el factor de turbulencia cuyo valor recomendado es 1,0.

Con los valores de  $k_r$  y  $v_b$  obtenidos en los apartados 4.3.1. y 4.2. respectivamente, y estableciendo  $k_1$  como la unidad:

$\sigma_v$ (m/s)	
Velocidad media 2019	Velocidad máxima 2019
1,14	2,60

Tabla 23. Desviación típica

Las alturas de cada tramo se encuentran parametrizadas según la primera desigualdad (ecuación 13), por lo que haremos uso de la primera ecuación mostrada:

	V. media 2019	V. máxima 2019
TRAMO	$I_v(z)$	$I_v(z)$
1	0,22	0,22
2	0,20	0,20
3	0,18	0,18
4	0,17	0,17
5	0,17	0,17

Tabla 24. Intensidad de turbulencia

Podemos observar en la tabla 24 que los valores de intensidad de turbulencia tanto para el caso del uso de la velocidad media como la máxima del 2019 son idénticos. Este hecho es debido a la

<sup>8</sup> Standard, 'Acciones Generales de Viento'.

proporción existente consecuencia del parámetro de velocidad básica  $v_b$ , perteneciente tanto a la expresión de la desviación típica como a la de la velocidad media.

## 6. Presión correspondiente a la velocidad de pico

El viento, a su paso por obstáculos, ejerce presión sobre estos. En función de la velocidad de este, su presión será mayor o menor, influyendo a su vez la densidad del aire presente y la intensidad de turbulencia.

$$q_p(z) = [1 + 7 \cdot I_v(z)] \cdot \frac{1}{2} \cdot \rho \cdot v_m(z) = c_e(z) \cdot q_b \quad (16)$$

donde

$q_p(z)$  es la presión correspondiente a la velocidad de pico.

$I_v(z)$  es la intensidad de turbulencia, determinada en el capítulo 5.

$v_m(z)$  es la velocidad media del viento, determinada en el apartado 4.3.

$\rho$  es la densidad del aire.

$c_e(z)$  es el factor de exposición. Su expresión es:

$$c_e(z) = \frac{q_p(z)}{q_b} \quad (17)$$

con

$q_b$  es la presión correspondiente a la velocidad media de referencia del viento, dada por:

$$q_b = \frac{1}{2} \cdot \rho \cdot v_b^2 \quad (18)$$

$v_b$  es la velocidad básica del viento, definida en el apartado 4.2.

La presión correspondiente a la velocidad de pico es el único valor de presión actuante sobre la superficie de la estructura. La presión del viento sobre superficies exteriores,  $w_e$ , al igual que la actuante sobre las superficies internas  $w_i$ , no se tendrán en cuenta ya que, la antena consta de un tipo de estructura abierta.

### 6.1. Densidad

De la misma manera que se ha efectuado un estudio teniendo en cuenta tanto velocidades medias como velocidades máximas del 2019, en el caso de la densidad del aire se da una situación parecida: La densidad<sup>9</sup> depende de la altura del objeto como de la temperatura del ambiente en el cual se encuentra. La altura es invariable, pero la temperatura varía a medida que transcurren las estaciones.

$$\rho = 348.42 \cdot \frac{1 - H \cdot 1,05 \cdot 10^{-4}}{T + 273} \quad (19)$$

<sup>9</sup> 'Densidad Del Aire'.

donde

$\rho$  es la densidad.

$H$  es la altura.

$T$  es la temperatura en °C.

Observamos entonces, que cuanto menor sea la temperatura, mayor lo será la densidad y, por consiguiente, mayor será la presión correspondiente a la velocidad de pico  $q_p(z)$ . Así pues, valoraremos el estudio según dos densidades distintas: Una de acuerdo con temperaturas medias (según norma) y otra con temperaturas mínimas. La densidad a proporción de la temperatura máxima carece de valor en el trabajo ya que su uso de cálculo sería menos severo que el aplicado por norma.

Las temperaturas, al igual que las velocidades de viento, han sido registradas en la estación de *Can Massuet, Dosrius*:

NOTA – Los registros de temperatura se encuentran en el anejo C.

NOTA – El registro carece de valores al completo, aunque los resultados obtenidos son del todo funcionales.

Año 2019	T (°C) media	T (°C) mínima
Enero	6,1	-2,2
Febrero	9,1	0,1
Marzo	-	-
Abril	10,8	0,9
Mayo	13,7	5,1
Junio	20,4	7,6
Julio	23,2	13,4
Agosto	23	14,9
Septiembre	19,7	11,4
Octubre	16,5	9,6
Noviembre	8,3	2,8
Media	15,08	6,36

Tabla 25. Temperaturas

En la tabla 25 se muestran las temperaturas registradas en el año 2019 y su media aritmética, la cual se empleará para los cálculos siguientes.

La altura actuante en la ecuación 19 de la densidad equivale a la altura media de cada tramo respecto del nivel del mar. La antena se encuentra a 402 m del nivel del mar, por lo que será necesario calcular la altura relativa por sección:



	H (m) media desde el suelo	H (m) desde el nivel del mar
Tramo 1	2,32	404,32
Tramo 2	6,37	408,37
Tramo 3	9,85	411,85
Tramo 4	13,85	415,85
Tramo 5	17,62	419,62

Tabla 26. Alturas relativas al nivel del mar

Aplicando la ecuación 19, con las medias de las temperaturas calculadas y las alturas medias respecto del nivel del mar de cada tramo de estudio (tabla 26), obtenemos:

	$\rho \text{ (kg/m}^3\text{)}$	
	Temperatura media	Temperatura mínima
Tramo 1	1,16	1,19
Tramo 2	1,16	1,19
Tramo 3	1,16	1,19
Tramo 4	1,16	1,19
Tramo 5	1,16	1,19

Tabla 27. Densidades

Con la densidad  $\rho$ , la intensidad de turbulencia  $I_v(z)$  y la velocidad media del viento  $v_m(z)$  ya es posible el cálculo de la presión correspondiente a la velocidad de pico.

Esta, llegados al punto donde existen distintas situaciones, dependerá de la densidad empleada (según si se aplica temperatura media o mínima) y de la velocidad del viento (según si se consideran valores medios o máximos de velocidad). Los resultados atinentes a cada caso son los tabulados a continuación:

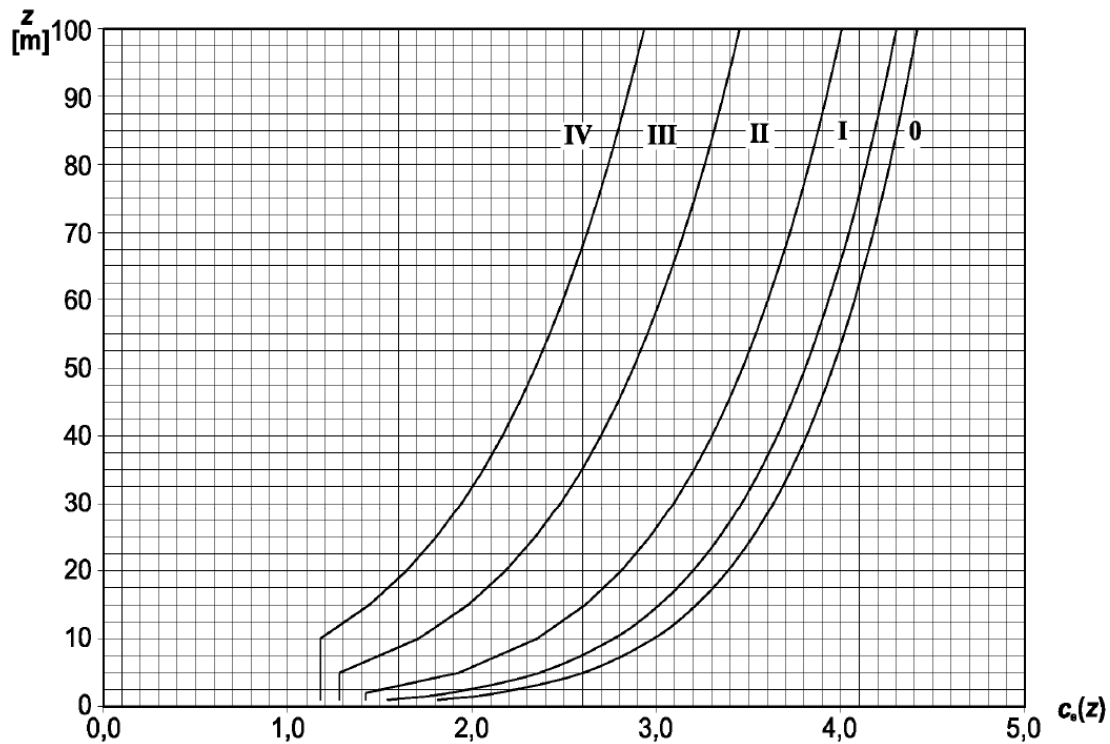
TRAMO	Velocidad media 2019					
	Temperatura mínima			Temperatura media		
	$q_p(z) \text{ (Pa)}$	$c_e(z)$	$q_b \text{ (Pa)}$	$q_p(z) \text{ (Pa)}$	$c_e(z)$	$q_b \text{ (Pa)}$
1	40,53	1,89	21,50	39,30	1,89	20,85
2	47,72	2,22		46,28	2,22	
3	52,55	2,44		50,96	2,44	
4	57,19	2,66		55,46	2,66	
5	59,64	2,77		57,83	2,77	

Tabla 28. Presiones para la velocidad media 2019

TRAMO	Velocidad máxima 2019					
	Temperatura mínima			Temperatura media		
	$q_p(z)(Pa)$	$c_e(z)$	$q_b(Pa)$	$q_p(z)(Pa)$	$c_e(z)$	$q_b(Pa)$
1	210,98	1,89	111,91	204,59	1,89	108,52
2	248,44	2,22		240,92	2,22	
3	273,59	2,44		265,31	2,44	
4	297,71	2,66		288,69	2,66	
5	310,47	2,77		301,08	2,77	

Tabla 29. Presiones para la velocidad máxima 2019

También se alojan en las tablas ilustradas la presión correspondiente a la velocidad media de referencia del viento  $q_p(z)$  y el factor de exposición  $c_e(z)$ . El valor de este último es posible comprobarlo mediante el gráfico 1 proporcionado por la UNE-EN 1991-1-4<sup>10</sup>, mostrado para todos los tipos de terreno:

Gráfico 1. Coeficiente de exposición  $c_e(z)$  para  $c_o=1,0$ ,  $k_1=1,0$  (Fuente: UNE-EN 1991-1-4)

<sup>10</sup> Standard, 'Acciones Generales de Viento'.

## 7. Coeficiente de fuerza de viento

En la normativa EN 1993-3-1<sup>11</sup> se define al coeficiente de fuerza de viento en la dirección del viento sobre una sección de la estructura como:

$$\sum c_f = c_{f,s} + c_{f,A} \quad (20)$$

donde

$c_{f,s}$  es el coeficiente de fuerza de viento sobre la sección de estructura desnuda.  
 $c_{f,A}$  es el coeficiente de fuerza de viento de los accesorios.

### 7.1. Componentes estructurales

Para una estructura de celosía de base cuadrada o triangular, teniendo áreas idénticas en cada una de las caras, el coeficiente de fuerza de viento de los componentes estructurales se puede tomar como:

$$c_{f,s} = K_\theta \cdot c_{f,s,0} \quad (21)$$

donde

$c_{f,s,0}$  es el coeficiente de arrastre.  
 $K_\theta$  es el factor de incidencia del viento que, en caso de base cuadrada, se obtiene por medio de la siguiente expresión:

$$K_\theta = 1,0 + K_1 \cdot K_2 \cdot \sin^2 2\theta \quad (22)$$

con

$$K_1 = \frac{0,55 \cdot A_f}{A_s} + \frac{0,8 \cdot (A_c + A_{c,sup})}{A_s} \quad (23)$$

$$\begin{aligned} K_2 &= 0,2 \text{ si } 0 \leq \varphi \leq 0,2 \text{ y } 0,8 \leq \varphi \leq 1,0 \\ &= \varphi \text{ para } 0,2 < \varphi \leq 0,5 \\ &= 1 - \varphi \text{ para } 0,5 < \varphi < 0,8 \end{aligned} \quad (24)$$

en los cuales

$\theta$  es el ángulo de incidencia del viento.  
 $\varphi$  es el ratio de solidificación.  
 $A_f$  es el área total proyectada de los miembros de cara plana en la cara.  
 $A_c$  es el área total proyectada de los miembros de cara circular en la cara.  
 $A_{c,sup}$  es el área total proyectada de los miembros de cara circular en la cara en regímenes supercríticos.

#### 7.1.1. Factor de incidencia

Las áreas, definidas para todos los tipos de perfiles existentes en el capítulo 3, son todas de cara plana, por lo que  $A_c$  y  $A_{c,sup}$  tendrán valor nulo en las ecuaciones del apartado 7.1.

<sup>11</sup> Standard, Torres y Mástiles.

Al ser la estructura simétrica en sus cuatro caras, el área permanecerá invariable en el análisis individual de cada una de las caras.

TRAMO	Área estructura (m <sup>2</sup> )
1	0,82
2	0,57
3	0,51
4	0,82
5	0,00

Tabla 30. Área por tramos

NOTA – El área total por tramo es la suma de áreas de los perfiles existentes en cada sección según se establece en el capítulo 3.

La relación de solidez viene dada por:

$$\varphi = \frac{A}{A'_c} \quad (25)$$

donde

$A$  es la suma de las áreas proyectadas de los elementos estructurales en dirección normal a la superficie.  
 $A'_c$  es el área encerrada por el contorno de la superficie proyectada en dirección normal a la cara.

El área encerrada se determina por medio del empleo del ángulo de inclinación de la estructura establecido en el apartado 3.1. La ecuación que define el área es el sumatorio del área de dos triángulos rectángulos más el de un rectángulo. La expresión resultante es la mostrada a continuación:

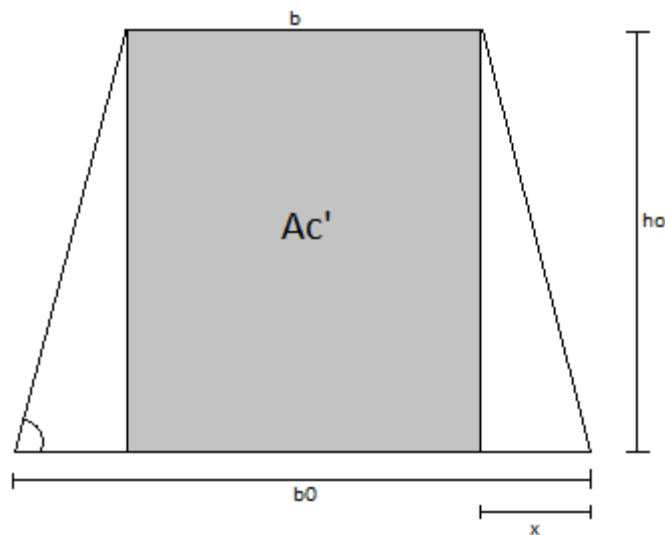


Ilustración 7. Cálculo del área de sección

$$A'_c = \frac{b - b_0}{-2} \cdot h_0 + b \cdot h_0 \quad (26)$$

TRAMO	A (m <sup>2</sup> )	L (mm)	b (mm)	A <sub>c</sub> ' (mm <sup>2</sup> )	φ
1	0,82	4.636,00	1.045,00	4.500.397,00	0,18
2	0,57	3.477,00	896,50	2.858.963,25	0,20
3	0,51	3.477,00	748,00	2.256.573,00	0,23
4	0,82	4.525,00	550,00	2.488.750,00	0,33
5	0,00	3.000,00	550,00	1.650.000,00	0,00

Tabla 31. Relación de solidez

NOTA – Las áreas y dimensiones de ancho y alto de tramo vienen dadas en el capítulo 3.

TRAMO	K <sub>1</sub>	K <sub>2</sub>
1	0,55	0,20
2	0,55	0,20
3	0,55	0,23
4	0,55	0,33
5	-	0,20

Tabla 32. Factores K1 y K2

NOTA – Nótese la falta de información en el tramo 5 de la tabla 32. Al no haber componentes estructurales en el quinto tramo de la antena, este no consta de factor de incidencia K<sub>1</sub>.

Finalmente, el factor de incidencia de viento, al depender este del ángulo de incidencia del viento, tendrá valores distintos en función del ángulo tomado.

La dirección de incidencia del viento es variable entre 0° y ± 45° en horizontal, según lo establece la norma UNE-EN 1991-1-4<sup>12</sup> (estructura de base cuadrada). Para una adecuada precisión de cálculo, se valorarán ambos extremos del intervalo propuesto:

TRAMO	K <sub>θ</sub>	
	0°	45°
1	1,00	1,11
2	1,00	1,11
3	1,00	1,12
4	1,00	1,18
5	-	-

Tabla 33. Factor de incidencia del viento

<sup>12</sup> Standard, 'Acciones Generales de Viento'.

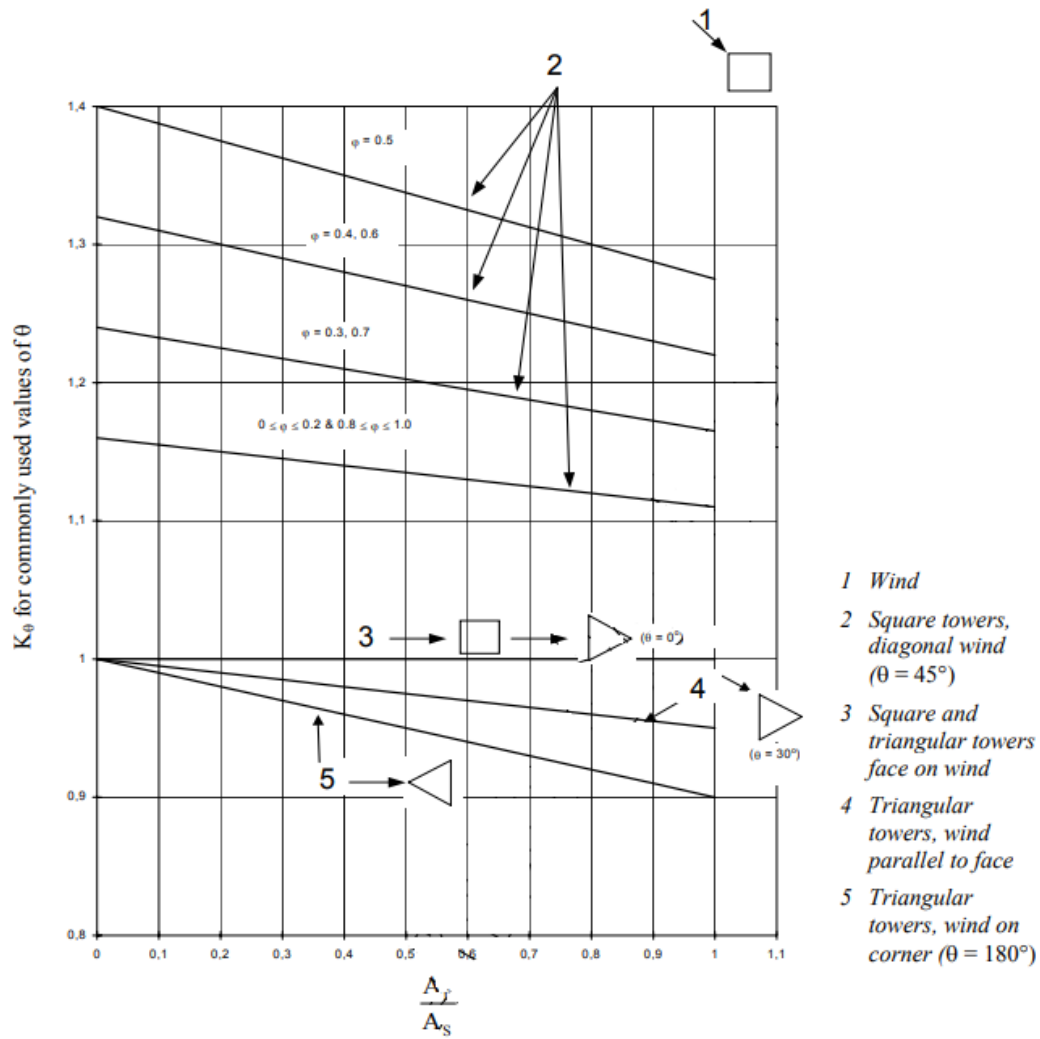


Gráfico 2.  $K_\theta$  en función de las áreas (Fuente: UNE-EN 1993-3-1)

El gráfico 2 refleja la relación del factor de incidencia de viento respecto a la relación de áreas de elementos de sección plana y del área total de los elementos de la estructura. Con los datos obtenidos en la tabla 33 verificamos según el gráfico los valores obtenidos.

### 7.1.2. Coeficiente de arrastre

Los valores del coeficiente de arrastre que son aplicables al marco de referencia de una estructura tanto de base cuadrada como triangular, compuesta por miembros de sección circular y plana deberían tomarse por:

$$c_{f,s,0} = c_{f,0,f} \cdot \frac{A_f}{A_s} + c_{f,0,c} \cdot \frac{A_c}{A_s} + c_{f,0,c,sup} \cdot \frac{A_{c,sup}}{A_s} \quad (27)$$

donde

$c_{f,0,f}$ ,  $c_{f,0,c}$  y  $c_{f,0,c,sup}$

son los coeficientes de fuera para secciones compuestas por miembros de sección plana, circulares subcríticos y circulares supercríticos, respectivamente, dados por:

$$c_{f,0,f} = 1,76 \cdot C_1 \cdot [1 - C_2 \cdot \varphi + \varphi^2] \quad (28)$$

$$c_{f,0,c} = C_1 \cdot (1 - C_2 \cdot \varphi) + (C_1 + 0,875) \cdot \varphi^2 \quad (29)$$

$$c_{f,0,c,sup} = 1,9 - \sqrt{(1 - \varphi) \cdot (2,8 - 1,14 \cdot C_1 + \varphi)} \quad (30)$$

con

$C_1$  = 2,25 para estructuras de base cuadrada.

= 1,9 para estructuras de base triangular.

$C_2$  = 1,5 para estructuras de base cuadrada.

= 1,4 para estructuras de base triangular.

Con las áreas y la relación de solidez establecidas en el apartado 7.1.1., los valores de coeficiente de arrastre son los tabulados a continuación:

TRAMO	$c_{f,0,f}$	$c_{f,0,c}$	$c_{f,0,c,sup}$	$c_{f,s,0}$
1	3,01	1,74	1,32	3,01
2	2,93	1,70	1,31	2,93
3	2,82	1,65	1,30	2,82
4	2,43	1,48	1,28	2,43
5	3,96	2,25	1,42	-

Tabla 34. Coeficientes de arrastre

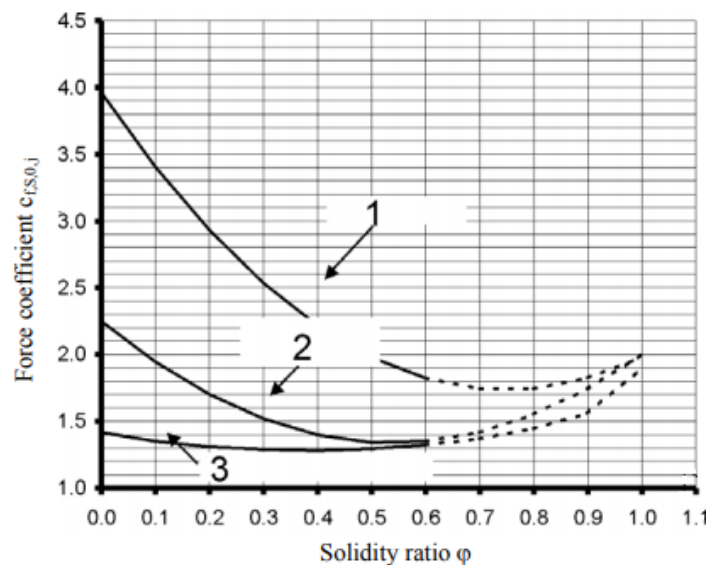


Gráfico 3. Coeficiente de arrastre (Fuente: UNE-EN 1993-3-1)

En el gráfico 3, con los valores de la relación de solidez de la tabla 31 observamos que, para el caso de elementos de sección plana (nº1 del gráfico 3), los valores de ambos factores se adecuan.

Entonces, con los coeficientes de arrastre calculados y el factor de incidencia del viento dependiente del tramo de sección y el ángulo de incidencia del viento (apartado 7.1.1.), empleando la ecuación 21:

TRAMO	$c_{f,s}$	
	0°	45°
1	3,01	3,34
2	2,93	3,25
3	2,82	3,17
4	2,43	2,87
5	-	-

Tabla 35. Coeficiente de fuerza de viento de la sección desnuda

## 7.2. Auxiliares

El coeficiente de fuerza  $c_{f,A}$  en la dirección del viento de cualquier parte auxiliar varía según si se trata de auxiliares lineales o discretos.

Se entiende por auxiliares lineales a aquellos pertenecientes a la misma categoría de las guías de onda, alimentadores, etc. Contrariamente, los discretos se asemejan más a platos reflectores de todo tipo.

La antena GSM de *Dosrius* no solo está conformada por su esqueleto estructural sino por una serie de antenas (Wifi, panel, parábola) y de módulos RRU. Al corresponderse todos ellos a la categoría de auxiliares discretos, la formulación del coeficiente de fuerza es la siguiente:

$$c_{f,A} = c_{f,A,0} \cdot K_A \quad (31)$$

donde

$c_{f,A,0}$  es el coeficiente de arrastre del elemento apropiado para la dirección y velocidad del viento.  
 $K_A$  es el factor de reducción.

### 7.2.1. Coeficiente de arrastre

El coeficiente de arrastre es un número adimensional que depende de la forma del objeto y de su orientación con respecto a la corriente de aire. Variará, por lo tanto, en función del elemento de estudio.

Las antenas parabólicas son comúnmente empleadas para el enlace de radio por microondas. Estas, según el ángulo de incidencia del viento, presentan un coeficiente de arrastre distinto:



Angulo de ataque del viento ( $\alpha$ ) en °C	$C_a$
0	1.5508
10	1.5391
20	1.5469
30	1.5547
40	1.5938
50	1.6641
60	1.6484
70	1.3672
80	0.7617
90	-0.0117
100	-0.4023
110	-0.4609
120	-0.457
130	-0.4688
140	-0.5742
150	-0.7734
160	-0.8672
170	-0.9453
180	-1.0547

Tabla 36. Coeficientes de arrastre para antenas de microondas sin reflector (Fuente: "Cálculo de los soportes para la instalación de antenas receptoras")

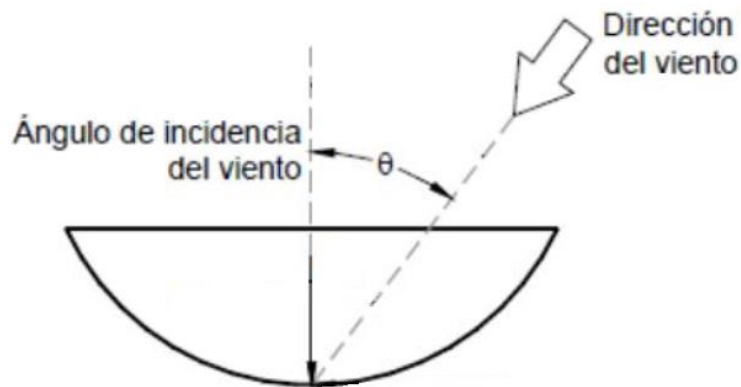


Ilustración 8. Ángulo del viento sobre las antenas parabólicas (Fuente: "Cálculo de los soportes para la instalación de antenas receptoras")

En el apartado 7.1.1. se ha establecido el estudio del ataque del viento entre  $0^\circ$  y  $\pm 45^\circ$ , evaluando los extremos del intervalo. En la tabla 36 pero, se aumenta de 10 en 10 grados, por lo que será necesario interpolar entre sus valores con tal de sonsacar el valor de los extremos del intervalo de estudio deseado:

$$y = \frac{x - x_1}{x_2 - x_1} \cdot (y_2 - y_1) + y_1 \quad (32)$$

donde

$x, y$  hacen referencia a las columnas de, en este caso, la tabla 34.

Ángulo de ataque	$c_{f,A,0}$
0°	1,5508
45°	1,62895

Tabla 37. Coeficientes de arrastre en función de la incidencia del viento

Las antenas Wifi y panel y los módulos RRU son todos de forma rectangular. Dichos elementos, al formar parte de la definición de placa plana perpendicular al flujo (3D)<sup>13</sup> tendrán un mismo valor de coeficiente de arrastre igual a 1,28:

$$c_{f,A,0_{Wifi,panel,RRU}} = 1,28$$

En relación con el cálculo del coeficiente de fuerza de viento de los auxiliares, se tomará como  $c_{f,A,0}$  a la media aritmética de los coeficientes de arrastre de los auxiliares existentes en la cara de estudio evaluada en cada caso.

### 7.2.2. Factor de reducción

El factor de reducción  $K_A$  es un factor para tener en cuenta acerca del blindaje del componente a la estructura y viceversa.

Position of ancillaries	Reduction factor, $K_A$	
	Square or rectangular plan form	Triangular plan form
Internal to the section	0,8	0,8
External to the section	0,8	0,8

Tabla 38. Factor de reducción (Fuente: UNE-EN 1993-3-1)

La tabla 36, proporcionada por la normativa UNE-EN 1993-3-1<sup>14</sup>, diferencia el valor del factor de reducción para estructuras de base triangular o cuadrada con posiciones internas o externas a la sección de los auxiliares presentes.

Por otro lado, la información de la tabla 38 no es el único evento que considerar para dar valor al factor de estudio. Existen tres posibles casos en los que su no cumplimiento conllevaría a tomar el valor de  $K_A$  como 1,0:

- El área total proyectada de los auxiliares adyacentes a la cara bajo consideración es menor que el área total proyectada de los miembros estructurales en la misma cara.
- El área total proyectada normal en cualquier cara de la estructura de cualquier auxiliar es menor que la mitad de la superficie bruta de la cara del panel.
- Cualquier auxiliar no se extiende más de un 10% del ancho total de la cara de la estructura.

<sup>13</sup> Drag Coefficient for plane elements.

<sup>14</sup> Standard, Torres y Mástiles.

NOTA – En el apartado 7.1.1. se han dado los valores correspondientes al área encerrada de cada tramo, al igual que su ancho total inferior. Las áreas individuales de los auxiliares y de los componentes estructurales se pueden encontrar en el capítulo 3.

Finalmente, valorando en función de lo expuesto anteriormente, se han substraído los siguientes resultados en base a las caras y tramos de la estructura:

	$K_A$			
	Cara 1	Cara 2	Cara 3	Cara 4
TRAMO 1	0,8	0,8	0,8	0,8
TRAMO 2	0,8	1	0,8	0,8
TRAMO 3	1	1	1	0,8
TRAMO 4	1	1	1	1
TRAMO 5	1	1	1	1

Tabla 39. Factores de reducción

Entonces, con el coeficiente de arrastre obtenido en el apartado 7.2.1. y los valores de  $K_A$  de la tabla 39 ya es posible la determinación del coeficiente de fuerza  $c_{f,A}$ . Al ser variante con la cara estudiada y el ángulo de inclinación del viento, se darán múltiples valores para el coeficiente:

	$c_{f,A}$			
	Cara 1		Cara 2	
TRAMO	0°	45°	0°	45°
1	0,00	0,00	0,00	0,00
2	1,24	1,30	1,55	1,63
3	1,28	1,28	1,28	1,28
4	1,35	1,37	1,35	1,37
5	1,28	1,28	1,28	1,28
	Cara 3		Cara 4	
	0°	45°	0°	45°
1	0,00	0,00	0,00	0,00
2	1,24	1,30	1,24	1,30
3	1,28	1,28	1,02	1,02
4	1,35	1,37	1,35	1,37
5	1,28	1,28	1,28	1,28

Tabla 40. Coeficiente de fuerza de viento de los auxiliares

NOTA – En el tramo 1 de todas las caras de la estructura consta un valor del coeficiente de fuerza nulo. Esto es debido a la falta de auxiliares en el primer tramo de la torre.

### 7.3. Coeficiente total

Ya hemos obtenido el coeficiente de fuerza de los elementos estructurales según el ángulo de incidencia del viento y el coeficiente relativo a los auxiliares, también según el ángulo de ataque y, además, en función de la cara de estudio.

Es posible, pues, el empleo de la ecuación 20 con el fin de dar valor al coeficiente total de fuerza de viento  $c_f$ :

	$c_f$			
	Cara 1		Cara 2	
TRAMO	0°	45°	0°	45°
1	3,01	3,34	3,01	3,34
2	4,17	4,55	4,48	4,88
3	4,10	4,45	4,10	4,45
4	3,78	4,24	3,78	4,24
5	1,28	1,28	1,28	1,28
	Cara 3		Cara 4	
TRAMO	0°	45°	0°	45°
1	3,01	3,34	3,01	3,34
2	4,17	4,55	4,17	4,55
3	4,10	4,45	3,84	4,19
4	3,78	4,24	3,78	4,24
5	1,28	1,28	1,28	1,28

Tabla 41. Coeficiente total de fuerza

Obsérvese que en el tramo 5 siempre se mantiene el mismo valor del coeficiente total de fuerza de viento. Este valor equivale al valor del coeficiente de fuerza de los auxiliares debido a la falta de estructura en este tramo, lo que conlleva a que sea el único tipo de coeficiente de fuerza actuante en la sección.

En el resto de los tramos, con el aumento de inclinación del ángulo de incidencia del viento aumenta el coeficiente de fuerza. Las secciones más propensas al ataque de viento son la 2, 3 y 4. En las dos primeras, este hecho es consecuencia de la distribución de los auxiliares en la estructura. En el tramo 4, el coeficiente es elevado como resultado de los componentes estructurales pertenecientes a la sección.

## 8. Factor estructural

El factor estructural  $c_s c_d$  concierne las condiciones del esqueleto de la estructura evaluada. Este es uno de los condicionantes de fuerza de viento resultante, por lo que su análisis debe de ser detallado y exhaustivo.

El estudio de la antena abarca, tal y como se ha hecho referencia en apartados anteriores, una serie de casos posibles según la toma de unos valores u otros: Velocidades medias o máximas del 2019, temperaturas medias o mínimas, la evaluación por separado de cada una de las cuatro caras de la estructura y el ángulo de incidencia del viento. Esto hecho conlleva a la evaluación de una gran cantidad de resultados en función de los casos mencionados.

A consecuencia de los numerosos valores posibles, a partir de este punto se evaluará en todos los tramos y caras de la torre de celosía únicamente el caso principal en el que:

- Velocidad máxima del 2019
- Temperatura mínima

El resto de los casos con sus respectivos valores de cada uno de los parámetros influyentes a la resolución de la fuerza de viento se dan en el anexo A. Aun así, la certificación de resistencia de la torre en el caso principal supondría también la verificación en el resto de los casos posibles, puesto que es el caso más desfavorable.

La selección de los parámetros del caso principal va en relación con la criticidad de la acción del viento: Con mayores velocidades se obtienen mayores fuerzas y cuanto menor sea la temperatura, mayor lo será la densidad que, al igual que la velocidad, al aumentar lo hace también la fuerza del viento.

Volviendo, pues, a la determinación del factor estructural, este se da en la expresión<sup>15</sup>:

$$c_s c_d = \frac{1 + 2 \cdot k_p \cdot I_v(z_s) \cdot \sqrt{B^2 + R^2}}{1 + 7 \cdot I_v(z_s)} \quad (33)$$

donde

$k_p$  es el factor de pico.

$I_v(z_s)$  es la intensidad de turbulencia, definida en el apartado 4.4., en función de la altura de referencia  $z_s$  para la determinación del factor estructural.

$B^2$  es el factor de respuesta de fondo.

$R^2$  es el factor de respuesta debido a la resonancia.

<sup>15</sup> Standard, 'Acciones Generales de Viento'.

## 8.1. Factor de respuesta de fondo

El factor de respuesta de fondo  $B^2$  tiene en cuenta la falta de correlación total de la presión en la superficie de la estructura. Se determina mediante la expresión:

$$B^2 = \frac{1}{1 + 0,9 \cdot \left( \frac{b+h}{L(z_s)} \right)^{0,63}} \quad (34)$$

donde

$b$  es la anchura de la estructura, definida en el apartado 3.2.

$h$  es la altura de la estructura, definida en el apartado 3.

$L(z_s)$  es la escala integral de longitud de turbulencia a una altura de referencia  $z_s$ .

### 8.1.1. Longitud de turbulencia

La escala integral de la longitud de turbulencia  $L(z)$ , por otro lado, representa el tamaño medio de la ráfaga para vientos naturales. Cuando se trata de alturas por debajo de los 200 m, la expresión de la determinación de la escala es:

$$L(z) = L_t \cdot \left( \frac{z}{z_t} \right)^\alpha \quad \text{para } z \geq z_{min} \quad (35)$$

$$L(z) = L(z_{min}) \quad \text{para } z < z_{min} \quad (36)$$

donde

$L_t$  es la escala de longitud de referencia igual a 300m.

$z_t$  es la altura de referencia igual a 200m.

$z$  es la altura máxima desde el suelo.

$z_{min}$  es una condición del tipo de terreno. En nuestro caso se toma como 2m, valor de la tabla 17.

$\alpha$  viene definido por:

$$\alpha = 0,67 + 0,05 \cdot \ln(z_0) \quad (37)$$

$z_0$  es la rugosidad, dependiente del tipo de terreno considerado. En nuestro caso se toma como 0,05m, valor definido en el apartado 4.3.1.

En vista del uso de alturas de referencia  $z_s$  en la expresión de la escala integral de longitud de turbulencia, veremos su definición:

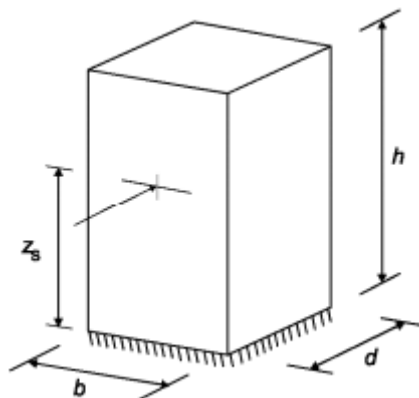


Ilustración 9. Altura de referencia (Fuente: UNE-EN 1991-1-4)

$$z_s = 0,6 \cdot h \geq z_{min} \quad (38)$$

TRAMO	$z_s$ (mm)
1	2.781,60
2	4.867,80
3	6.954,00
4	9.669,00
5	11.469,00

Tabla 42. Alturas de referencia

Las alturas de referencia por tramo de la tabla 42 cumplen con el requisito de ser igual o mayores que  $z_{min}$ , por lo que se dan como válidas y, a su vez, de acuerdo con las dos posibles ecuaciones de la longitud de referencia, se aplica la primera (ecuación 35):

TRAMO	$L(z_s)$ (m)
1	32,45
2	43,42
3	52,27
4	62,04
5	67,81

Tabla 43. Escala de longitud de turbulencia

Ahora, con los valores obtenidos tanto de longitud de turbulencia como de anchura por tramo, ya somos capaces de determinar el factor de respuesta de fondo  $B^2$ :

TRAMO	$B^2$
1	0,77
2	0,83
3	0,84
4	0,84
5	0,88

Tabla 44. Factor de respuesta de fondo

## 8.2. Factor de respuesta debido a la resonancia

El factor de respuesta  $R^2$  debido a la resonancia tiene en cuenta la resonancia del modo de vibración con la turbulencia.

$$R^2 = \frac{\pi^2}{2 \cdot \delta} \cdot S_L(z_s, n_{1,x}) \cdot R_h(\mathbb{Z}_h) \cdot R_b(\mathbb{Z}_b) \quad (39)$$

donde

$\delta$  es el decremento logarítmico total del amortiguamiento.

$S_L$  es la función de densidad espectral de potencia adimensional.

$R_h, R_b$  son las funciones de admitancia aerodinámica. Estas, para una forma modal, se pueden aproximar mediante las siguientes expresiones:

$$R_h = \frac{1}{\eta_h} - \frac{1}{2 \cdot \eta_h^2} (1 - e^{-2 \cdot \eta_h}); \quad R_h = 1 \text{ para } \eta_h = 0 \quad (40)$$

$$R_b = \frac{1}{\eta_b} - \frac{1}{2 \cdot \eta_b^2} (1 - e^{-2 \cdot \eta_b}); \quad R_b = 1 \text{ para } \eta_b = 0 \quad (41)$$

Donde

$$\eta_h = \frac{4,6 \cdot h}{L(z_s)} \cdot f_L(z_s, n_{1,x}) \quad y \quad \eta_b = \frac{4,6 \cdot b}{L(z_s)} \cdot f_L(z_s, n_{1,x}) \quad (42)$$

$f_L$  es una frecuencia adimensional.

$n_{1,x}$  es la frecuencia natural de la estructura en Hz.

$e$  es la excentricidad de la fuerza resultante.

### 8.2.1. Frecuencia y densidad espectral de potencia adimensional

$$f_L(z_s, n_{1,x}) = \frac{n_{1,x} \cdot L(z_s)}{v_m(z_s)} \quad (43)$$

donde

$L(z_s)$  es la longitud de turbulencia, definida en el apartado 4.6.1.2.

$v_m(z_s)$  es la velocidad media del viento, definida en el apartado 4.3.

$n_{1,x}$  es la frecuencia natural de vibración de la estructura.

La frecuencia adimensional anteriormente presentada está en función, entre otras, de la altura relativa. Este hecho es debido a la implicación de su uso frente al cálculo del coeficiente estructural de la antena, sustituyendo pues al valor real de la altura.

Carece de sentido tener en consideración la frecuencia de natural de vibración a razón de la ausencia de cargas variables. En nuestro caso, como se trata de una carga continua de viento actuante en la frecuencia de resonancia, el caso más crítico y el posteriormente estudiado es aquel en que:

$$n_{1,x} = n_1 \quad (44)$$

donde

$n_1$  es la frecuencia natural de la estructura cuya expresión es:

$$n_1 = \frac{1}{2 \cdot \pi} \cdot \sqrt{\frac{g}{x_1}} \quad (45)$$

con

$g$  es la aceleración de la gravedad = 9,81 m/s<sup>2</sup>.

$x_1$  es el desplazamiento máximo en metros.

Normalmente en el diseño de torres de soporte de antenas, por parte de los fabricantes se incluye una limitación de desviación en punta de como máximo 1°.



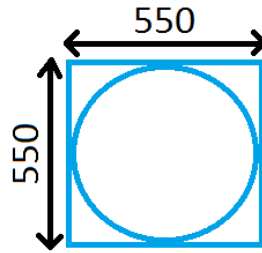


Ilustración 10. 360° de la base superior

El perímetro de la superficie de la base superior (ilustración 10) es el equivalente a 360°<sup>16</sup>. La desviación de 1° es determinable por una simple regla de tres:

lado(mm)	P(m)	1°
550,00	2,20	0,01

Tabla 45. Perímetro y desviación máxima en punta

Entonces, con la aplicación de la ecuación 45, podemos extraer el valor de la frecuencia fundamental:

$$n_1 = \frac{1}{2 \cdot \pi} \cdot \sqrt{\frac{g}{x_1}} = 6,38 \text{ Hz}$$

En función de la velocidad máxima del 2019 y el tramo de estudio:

TRAMO	$f_L(z_s, n_{1,x})$
1	19,80
2	23,25
3	25,97
4	28,89
5	30,58

Tabla 46. Frecuencias adimensionales

La densidad espectral de potencia adimensional  $S_L$  abarca la distribución del viento en frecuencias. Como en la frecuencia adimensional, la densidad espectral se determina a partir de la altura relativa de cada tramo (requerimiento del factor estructural):

$$S_L(z_s, n_{1,x}) = \frac{6,8 \cdot f_L(z_s, n_{1,x})}{(1 + 10,2 \cdot f_L(z_s, n_{1,x}))^{5/3}} \quad (46)$$

<sup>16</sup> Equivalencia de Metros y Arcos de Segundo y Minuto.

TRAMO	$S_L(z_s, n_{1,x})$
1	0,02
2	0,02
3	0,02
4	0,01
5	0,01

Tabla 47. Densidad espectral de potencia adimensional

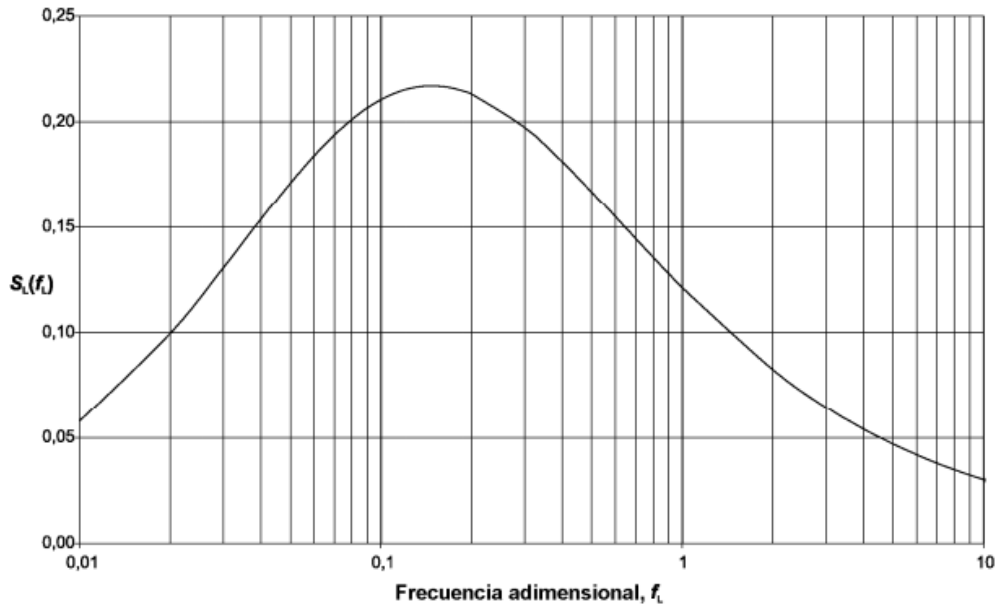


Gráfico 4. frecuencia y densidad adimensional (Fuente: UNE-EN 1991-1-4)

### 8.2.2. Funciones de admitancia aerodinámica

Las funciones de admitancia aerodinámica dependen de la excentricidad.

La excentricidad estructural<sup>17</sup> es la distancia entre el punto de aplicación de la carga y aquel donde se concentra la fuerza resultante. Si la concentración de carga de viento se sitúa en el punto más álcido de la estructura (vértice superior del tramo 4) y el punto de aplicación de la carga es en el centro de cada tramo de estudio:

TRAMO	$e$ (m)
1	13,80
2	9,74
3	6,26
4	2,26
5	1,50

Tabla 48. Excentricidad

<sup>17</sup> Eric W Weisstein and Eric W Weisstein, 'Excentricidad'.

Con la función de densidad espectral de potencia y la frecuencia adimensionales (apartado 8.2.1.) es posible la determinación de  $\eta_h$  y  $\eta_b$ , con los cuales se procede a la resolución de las funciones de admitancia aerodinámica del caso principal:

TRAMO	$\eta_h$	$\eta_b$	$R_h$	$R_b$
1	13,01	2,93	0,07	0,28
2	19,98	2,21	0,05	0,35
3	26,48	1,71	0,04	0,41
4	34,52	1,18	0,03	0,54
5	39,66	1,14	0,02	0,64

Tabla 49. Funciones de admitancia para velocidad máxima 2019

### 8.2.3. Decremento logarítmico del amortiguamiento

El decremento logarítmico total del amortiguamiento  $\delta$  para el modo fundamental de flexión se puede estimar por:

$$\delta = \delta_s + \delta_a + \delta_d \quad (47)$$

donde

$\delta_s$  es el decremento logarítmico del amortiguamiento estructural.

$\delta_a$  es el decremento logarítmico aerodinámico para el modo fundamental.

$\delta_d$  es el decremento logarítmico del amortiguamiento producido por dispositivos especiales, entendiéndose por especiales a los amortiguadores de masas acopladas, tanques de agua con disipación por oleaje, etc.

El decremento  $\delta_d$  no tiene papel en el estudio, por lo que no consta de su aplicación.

El decremento logarítmico del amortiguamiento estructural  $\delta_s$  está tabulado en la norma UNE-EN 1991-1-4<sup>18</sup> y mostrado a continuación:

<sup>18</sup> Standard, 'Acciones Generales de Viento'.

Tipo de estructura		Amortiguamiento estructural, $\delta$
Edificios de hormigón armado		0,10
Edificios de acero		0,05
Estructuras mixtas: acero + hormigón		0,08
Torres y chimeneas de hormigón armado		0,03
Pilas de acero estructural soldadas no alineadas sin aislamiento térmico exterior		0,012
Pilas de acero estructural soldadas no alineadas con aislamiento térmico exterior		0,020
Pila de acero con una camisa de rigidización y aislamiento térmico exterior <sup>a</sup>	$h/b < 18$	0,020
	$20 \leq h/b < 24$	0,040
	$h/b \geq 26$	0,014
Pila de acero con dos o más camisas de rigidización y aislamiento térmico exterior <sup>a</sup>	$h/b < 18$	0,020
	$20 \leq h/b < 24$	0,040
	$h/b \geq 26$	0,025
Pilas de acero con camisa interior enladrillada		0,070
Pilas de acero gunitadas interiormente		0,030
Pilas arriostradas sin camisas de rigidización interiores		0,015
Pilas de acero atirantadas sin camisa de rigidización interior		0,04
Puentes de acero + torres de celosía metálica	Soldados	0,02
	Tomillos de alta resistencia	0,03
	Tomillos ordinarios	0,05
Puentes mixtos		0,04
Puentes de hormigón	Pretensados y no fisurados	0,04
	Fisurados	0,10
Puentes de madera		0,06 – 0,12
Puentes de aleaciones de aluminio		0,02
Puentes de fibra de vidrio o carbono		0,04 – 0,08
Cables	Cables en paralelo	0,006
	Cables en espiral	0,020
NOTA 1 – Los valores de puentes de madera y fibra de carbono o vidrio únicamente son indicativos. En aquellos casos en los que los efectos aerodinámicos puedan ser significativos en el diseño, se necesita un análisis especial para la determinación de los valores adecuados (sujeto a acuerdo con la autoridad competente si fuera apropiado).		
NOTA 2 – En puentes atirantados o colgados es necesario que los valores mostrados en la tabla F.2 se multipliquen por un factor 0,75.		
<sup>a</sup> Para valores intermedios de $h/b$ , se puede emplear la interpolación lineal		

Tabla 50. Valores aproximados del decremento logarítmico del amortiguamiento estructural para la forma modal fundamental (Fuente: UNE-EN 1991-1-4)

La antena GSM forma parte de la categoría de las torres de celosía metálica. La tornillería existente en esta es ordinaria en todos los tramos a excepción del cuarto tramo, en el cual las uniones son soldadas. Según la tabla 50:

$$\delta_{s\_tramo\ 1,2,3} = 0,05 \quad ; \quad \delta_{s\_tramo\ 4} = 0,02$$

El amortiguamiento aerodinámico aumenta con la velocidad media y contribuye grandemente en el amortiguamiento total de la estructura.

Las deformaciones modales  $\Phi(y, z)$  son constantes para cada altura  $z$ , razón por la cual es posible la obviedad de esta variable y la aplicación de la siguiente expresión para el cálculo de dicho decremento:

$$\delta_a = \frac{c_{f,s} \cdot \rho \cdot b \cdot v_m(z_s)}{2 \cdot n_1 \cdot m_e} \quad (48)$$

donde

$c_{f,s}$  es el coeficiente de fuerza del viento sobre los componentes de la estructura.

$\rho$  es la densidad del aire, definida en el apartado 6.1.

$b$  es la anchura de tramo, definida en el apartado 3.2.

$v_m(z_s)$  es la velocidad media de viento respecto a la altura de referencia.

$n_1$  es la frecuencia natural.

$m_e$  es la masa equivalente por unidad de longitud del modo fundamental.

De los parámetros actuantes en la ecuación anterior solo nos resta el valor de la frecuencia fundamental de flexión de la estructura y el de la masa equivalente por unidad de longitud.

En la antena GSM, según fuentes de la empresa de *Cellnex*, no hay respuesta dinámica, por lo que es posible tomar la masa definida en el apartado 3.3.

Al tratarse de una estructura simétrica en sus cuatro caras, el decremento logarítmico del amortiguamiento  $\delta$  permanecerá invariable en todas sus caras, pero en función del caso de estudio, tendrá valores distintos. Por lo indicado al inicio del capítulo, se evaluará explícitamente el caso principal, siendo adjuntos el resto de los casos en el anejo A.

Haciendo uso de la formulación del decremento logarítmico del amortiguamiento aerodinámico y añadiendo su valor a la expresión de  $\delta$  obtenemos:

TRAMO	$\delta$	
	0°	45°
1	0,09	0,09
2	0,10	0,11
3	0,10	0,11
4	0,05	0,05
5	-	-

Tabla 51. Decremento logarítmico

NOTA – El tramo 5 no tiene valores del decremento logarítmico  $\delta_a$  y consecuentemente en el  $\delta$  a falta de componentes estructurales.

Una vez resueltos todos aquellos datos modificadores del factor de respuesta debido a la resonancia  $R^2$ , ya es posible darle valor al factor para el caso principal.

El factor  $R^2$  para el caso de velocidades máximas (caso principal) queda presentado por:

TRAMO	$R^2$	
	0°	45°
1	0,02	0,02
2	0,01	0,01
3	0,01	0,01
4	0,02	0,02
5	-	-

Tabla 52. Factor de respuesta debido a la resonancia

NOTA – Los valores del factor de respuesta debido a la resonancia son prácticamente idénticos (varianza centesimal) tanto para 0° como para 45° debido a la única diferencia de valor del decremento logarítmico en su ecuación, el cual ya consta de valores similares para ambas direcciones.

### 8.3. Intensidad de turbulencia

La intensidad de turbulencia ya viene definida en el capítulo 5 del proyecto. En este caso, para la determinación del factor estructural es necesario comprender su cálculo en base a la altura de referencia  $z_s$ .

Haciendo uso de la ecuación 13 del capítulo 5, cambiando la referencia de la altura por la de referencia de la tabla 42, resultan los valores presentados a continuación:

TRAMO	$I_v(z_s) (m)$
1	0,25
2	0,22
3	0,20
4	0,19
5	0,18

Tabla 53. Intensidad de turbulencia para una altura de referencia

NOTA – La intensidad de turbulencia para una altura de referencia  $z_s$  es constante en todos los casos de estudio.

### 8.4. Factor de pico

El factor de pico se define tal que la relación entre el valor máximo de la fracción fluctuante de la respuesta con respecto a su desviación típica. Dicho factor debe obtenerse a partir de:

$$k_p = \sqrt{2 \cdot \ln(v \cdot T)} + \frac{0,6}{\sqrt{2 \cdot \ln(v \cdot T)}} \quad \text{o} \quad k_p = 3, \text{ el que sea mayor} \quad (49)$$

donde

$T$  es el tiempo promedio para la velocidad del viento,  $T=600s$ .

$V$  es la frecuencia media de oscilación cuya expresión se define por:

$$v = n_{1,x} \cdot \sqrt{\frac{R^2}{B^2 + R^2}} \quad ; \quad v \geq 0,08 \text{ Hz} \quad (50)$$

con

$R^2$  es el factor de respuesta debido a la resonancia, definido en el apartado 8.2.

$B^2$  es el factor de respuesta de fondo, definido en el apartado 8.1.

$n_{1,x}$  es la frecuencia natural de la estructura, definida en el apartado 8.2.1. como 2 Hz.

De nuevo, haciendo hincapié en la única valoración del caso principal de estudio, se presentan seguidamente los valores de la frecuencia media de oscilación y los factores de pico provenientes:

TRAMO	$k_p$	$v$ (Hz)
1	3,76	1,05
2	3,69	0,82
3	3,66	0,73
4	3,74	1,00
5	-	-

Tabla 54. Factores de pico

NOTA – Nótese la escasez de resultados en el tramo 5 de estudio debido a la falta de estructura en dicha sección.

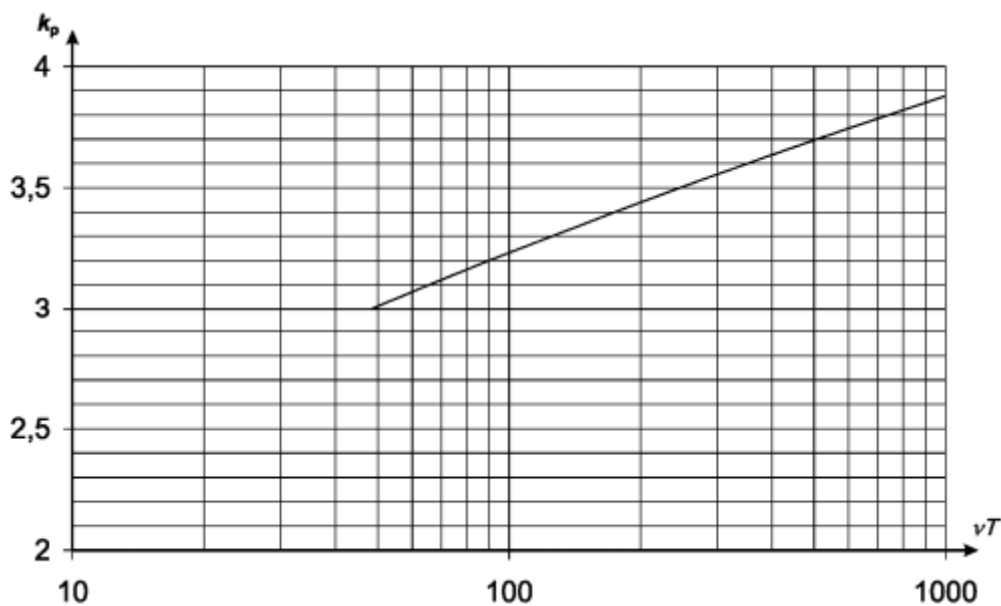


Gráfico 5 Factor  $k_p$  (Fuente: UNE-EN 1991-1-4)

Llegados a este punto, ya somos capaces de cuantificar el factor estructural de la antena para el caso principal. De nuevo, no se toma en consideración su quinto tramo en virtud de la falta de componentes estructurales.

TRAMO	$c_s c_d$
1	0,97
2	0,98
3	0,98
4	1,00

Tabla 55. Factor estructural



## 9. Fuerza de viento

La fuerza de viento correspondiente a estructuras es relativa en función del tipo de estructura (chimeneas, torres de edificios, etc.) junto con su área expuesta, la velocidad registrada y, consecuentemente, según la presión de pico y el coeficiente de fuerza del viento actuante.

Su valor se puede expresar por medio de la siguiente configuración<sup>19</sup>:

$$F_w = c_s c_d \cdot c_f \cdot q_p(z_e) \cdot A_{ref} \quad (51)$$

donde

$c_s c_d$  es el factor estructural definido en el capítulo 8.

$c_f$  es el coeficiente de fuerza para el elemento estructural o estructura, definido en el capítulo 7.

$q_p(z_e)$  es la presión correspondiente a la velocidad de pico (definida en el apartado 6.) a la altura de referencia  $z_e$ .

$A_{ref}$  es el área de referencia para el elemento estructural o la estructura.

Las nueva altura de referencia  $z_e$  y el área de referencia  $A_{ref}$  resultan del tipo de distribución generada en el cuerpo de la estructura de la antena GSM. Por lo tanto, las alturas de referencia serán las alturas máximas en el eje vertical respecto del suelo de cada uno de los tramos, que irán de la mano de cada una de sus áreas individuales de estudio.

Las áreas de cada tramo constituyentes de la torre están expuestas por familias de perfiles en el capítulo 3, con suma total en conjunto por sección en la tabla 30. El resto de los parámetros también han sido determinados, por lo que la fuerza del caso principal queda descrita de tal manera que:

	$F_w(N)$			
	Cara 1		Cara 2	
TRAMO	0°	45°	0°	45°
1	504,63	559,36	504,36	559,36
2	582,05	634,94	625,35	680,36
3	562,13	609,27	562,13	609,27
4	926,62	1037,20	926,62	1037,20
	Cara 3		Cara 4	
TRAMO	0°	45°	0°	45°
1	504,63	559,36	504,63	559,36
2	582,05	634,94	582,05	634,94
3	562,13	609,27	527,02	574,22
4	926,62	1037,20	926,62	1037,20

Tabla 56. Fuerza de viento

NOTA – El tramo 5 no es representado en la tabla por su falta de componentes estructurales.

<sup>19</sup> Standard, 'Acciones Generales de Viento'.

En la mayoría de los tramos y caras se repiten los valores debido a la configuración de los auxiliares en la torre. Estos afectan diminutamente sobre el resultado final ya que, son pocos y, por lo general, de tamaño reducido.

Otro factor influyente en la similitud de los datos obtenidos en la tabla 56 y en la mayoría de las tablas del estudio es la simetría de las caras: Los parámetros actuantes únicamente al esqueleto de la estructura, al ser idéntica vista desde cualquier posición, son de igual valor en el mismo tramo de cualquiera de las caras.

## 10. Verificación estructural

Con la fuerza de viento ejercida sobre la estructura (capítulo 9) procedemos a la comprobación de resistencia de la torre en las condiciones establecidas.

*Cype* es, principalmente, un software técnico de diseño para el cálculo de estructuras, instalaciones de edificios y gestión de la construcción. Es capaz de, entre otras funciones, reproducir la respuesta de una estructura frente a las fuerzas a las que está expuesta, describiendo cada uno de los movimientos y/o roturas producidas en cualquiera de sus elementos estructurales.

La precisión es uno de los pilares primordiales del proyecto, razón por la cual se ha optado por el uso del software de diseño *Cype*.

### 10.1. Descripción de la geometría

Primeramente, procederemos al dimensionado de la estructura en *Cype*, junto con su material de construcción y perfiles de las vigas.

Para ello, será necesario dirigirnos al entorno del *Cype 3D*, a partir del cual, desde cero, generaremos la antena GSM.

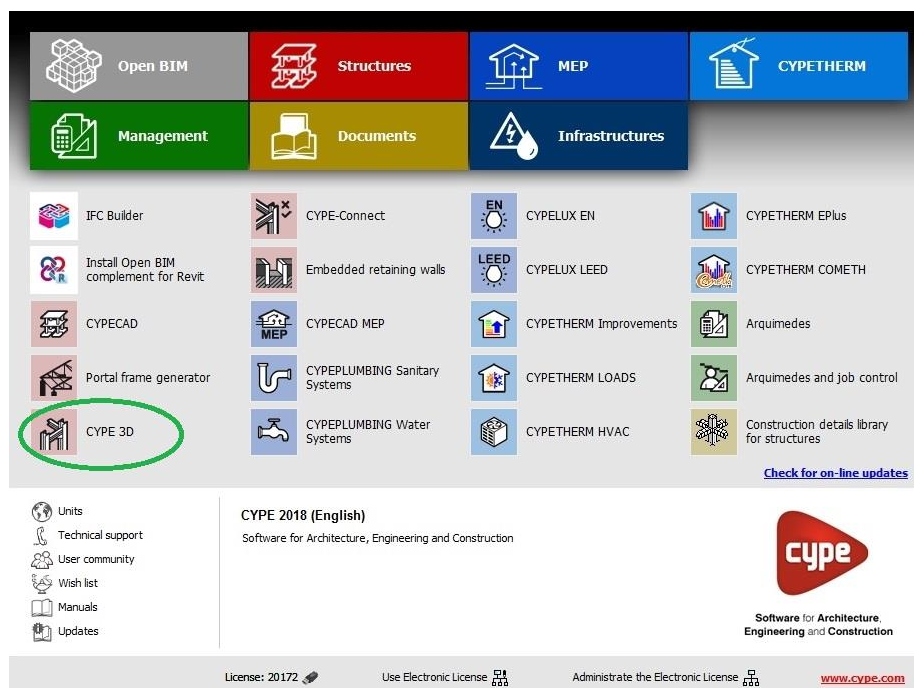


Ilustración 11. Menú desplegable en Cype (Fuente: Cype)

Dentro del entorno de *Cype 3D* y antes de empezar a diseñar, deberemos seleccionar la normativa aplicable a nuestro caso de estudio y aquellas características influyentes en él.

**General data**

**Codes:** Eurocode 2, Eurocodes 3 and 4, Eurocode 5 and Eurocode 9

**Sections**

- Rolled steel** (highlighted with a green circle): S275 (EN 1993-1-1)
- Cold formed steel: Fe360
- Timber: Sawn, from conifers or poplars - C24
- Aluminium: EN AW-5083 - F
- Concrete: C25/30

**Reinforced concrete**

- Concrete for columns: C25/30
- Concrete for floor slab beams: C25/30
- Concrete for foundation elements: C25/30
- Bar steel: S-400
- Aggregate properties: Quartzite (15 mm), 30 mm
- Cover: [ ]
- Fabrication losses: [ ]

**Foundation soil**

- ☐ Verify footing sliding
- Adherence (a'): 0.000 MPa
- Soil- footing friction angle (d'): 25.00 degrees
- Persistent situations: 0.200 MPa
- Seismic and accidental situations: 0.300 MPa

**Options**

- Columns: [ ]
- Foundations: [ ]
- Beams: [ ]
- Joints: [ ]

**Environment**

- Beams: X0

**Accept**

Ilustración 12. General data (Fuente: Cype)

En la ilustración anterior están marcadas en verde aquellos apartados del menú relevantes al caso de estudio: La normativa de uso y el material estructural.

Las normas con las que se ha procedido al cálculo de la fuerza de viento en la torre de celosía han sido EU-EN 1991-1-4<sup>20</sup> y EU-EN 1993-3-1<sup>21</sup>. El material original de construcción de la torre es de acero A42b. Este tipo de acero resiste  $2600 \text{ kg/cm}^2$  ( $254,9729 \text{ N/mm}^2$ ). Debido a que está hoy en día obsoleto, se ha aprovechado su equivalente, el acero S275, el más típico de los laminados, que soporta  $275 \text{ N/mm}^2$ .

### 10.1.1. Dimensionado y perfiles

Con lo descrito en el apartado 10.1. ya es posible adentrarnos en el marco de diseño que, por medio del dibujo y dimensionado de barras y nodos, produciremos la geometría.

<sup>20</sup> Standard, 'Acciones Generales de Viento'.

<sup>21</sup> Standard, *Torres y Mástiles*.

Los nodos de la base de la torre han sido establecidos como nudos articulados. Entre tanto, los nudos relativos a las barras interiores son del tipo empotrados con extremos articulados.

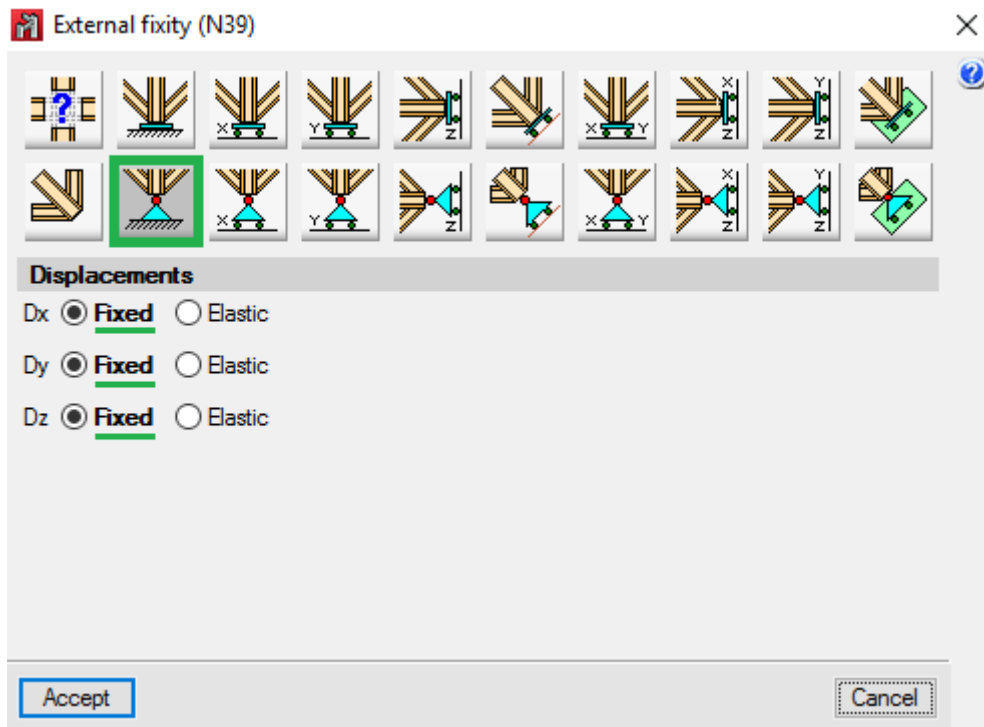


Ilustración 13. Nudos de la base (Fuente: Cype)

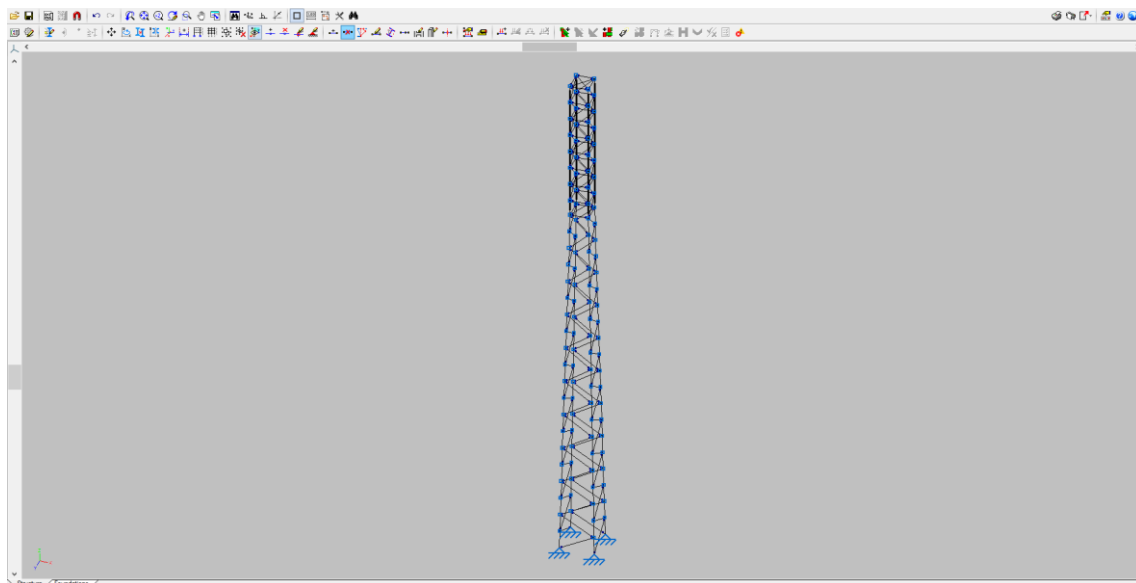


Ilustración 14. Antena en Cype (Fuente: Cype)

Los perfiles de los componentes estructurales, todos ellos detalladamente definidos en el capítulo 3, también serán de obligada descripción.

Hay que recordar que contamos con cuatro tipos de componentes: Diagonales, horizontales, montantes y de refuerzo. Todos comparten el mismo perfil (angular de lados iguales) pero con distintas medidas de ancho y espesor.

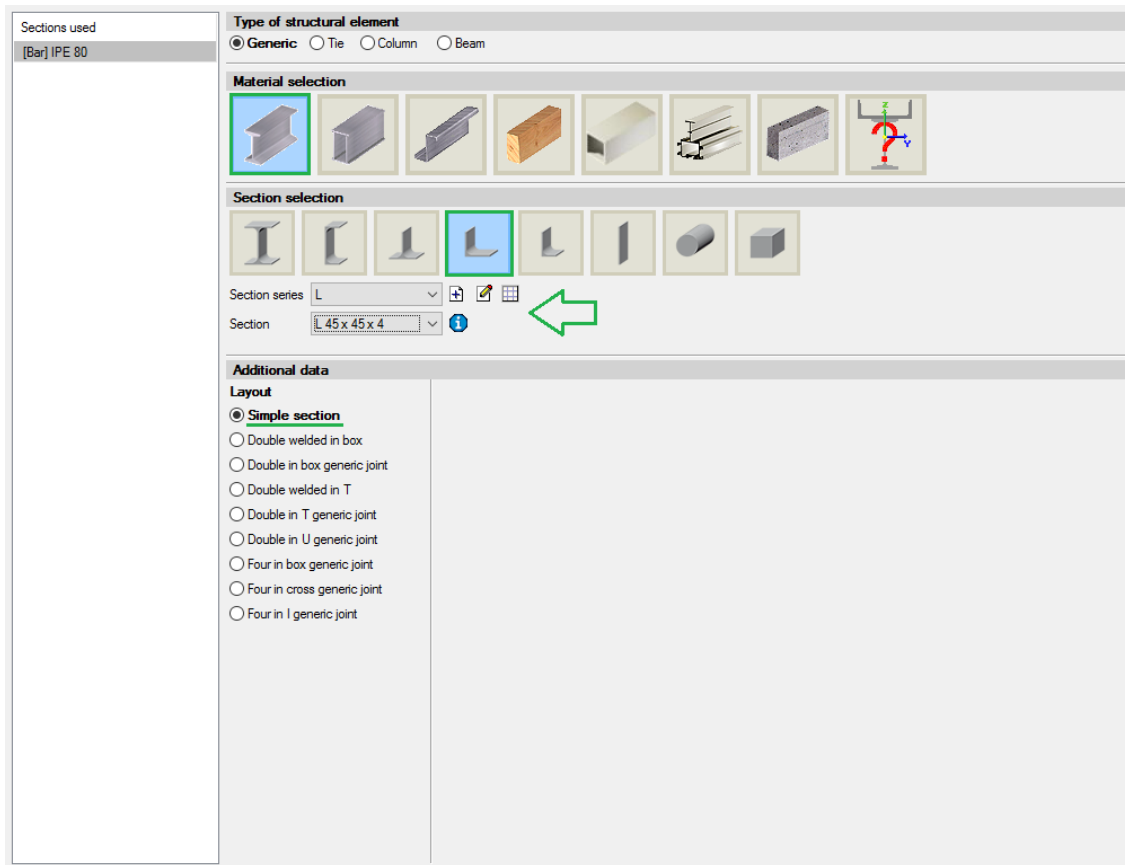


Ilustración 15. Parametrización de los perfiles diagonales (Fuente: Cype)

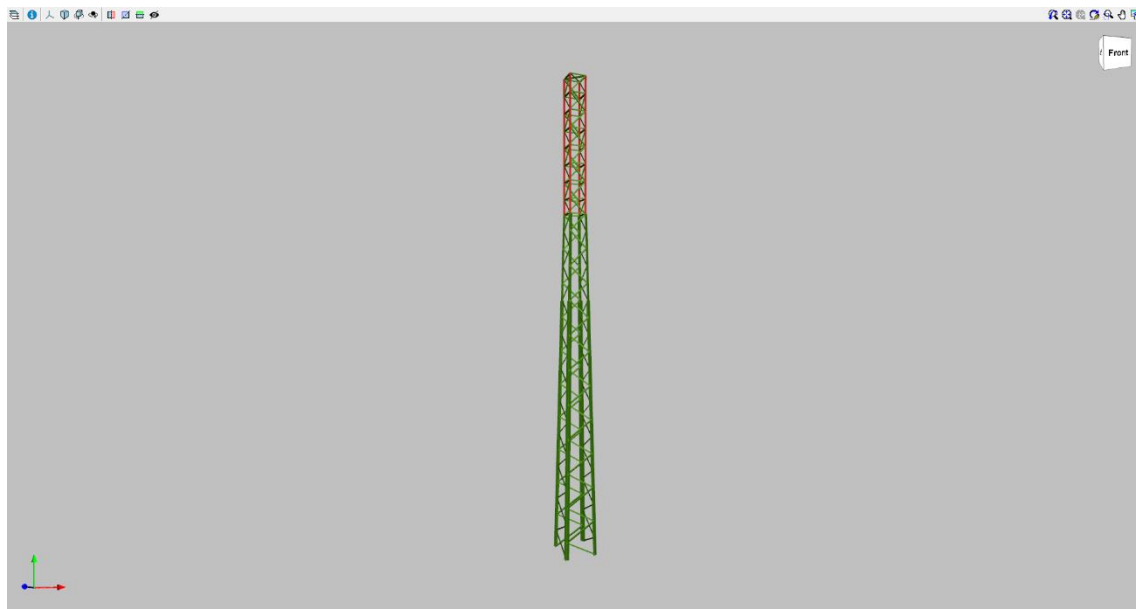


Ilustración 16. Renderizado de la antena en Cype (Fuente: Cype)

## 10.2. Hipótesis de cálculo

En Cype evaluaremos la respuesta de la estructura frente al viento considerando una fuerza resultante.

La nombrada fuerza resultante es aquella fruto de las fuerzas actuantes en cada uno de los tramos de la estructura. Habrá una fuerza resultante por cara de la estructura y ángulo de inclinación de la fuerza de viento.

Se han valorado dos incidencias de viento distintas ( $0^\circ$  y  $45^\circ$ ) por cada cara de la torre. Tendremos, por lo tanto, un total de 8 hipótesis de viento a calcular en el programa *Cype*. Todas estas fuerzas resultantes se concentran en lo alto del tramo 4, en cuya base se ha diseñado un conjunto de vigas en cruz con tal de abastecer la concentración de todas estas fuerzas en un mismo punto.

*NOTA – El nuevo conjunto de vigas en cruz comparte el mismo perfil que los componentes horizontales del cuarto tramo.*

Respecto a la evaluación del pandeo de la estructura, su coeficiente ha sido tomado del valor de la unidad al tratarse de una estructura en celosía.

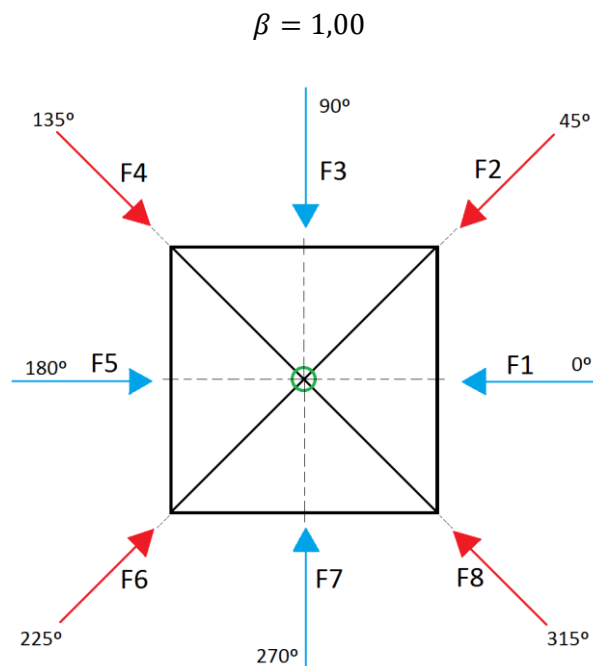


Ilustración 17. Hipótesis de cálculo

### 10.2.1. Fuerza resultante

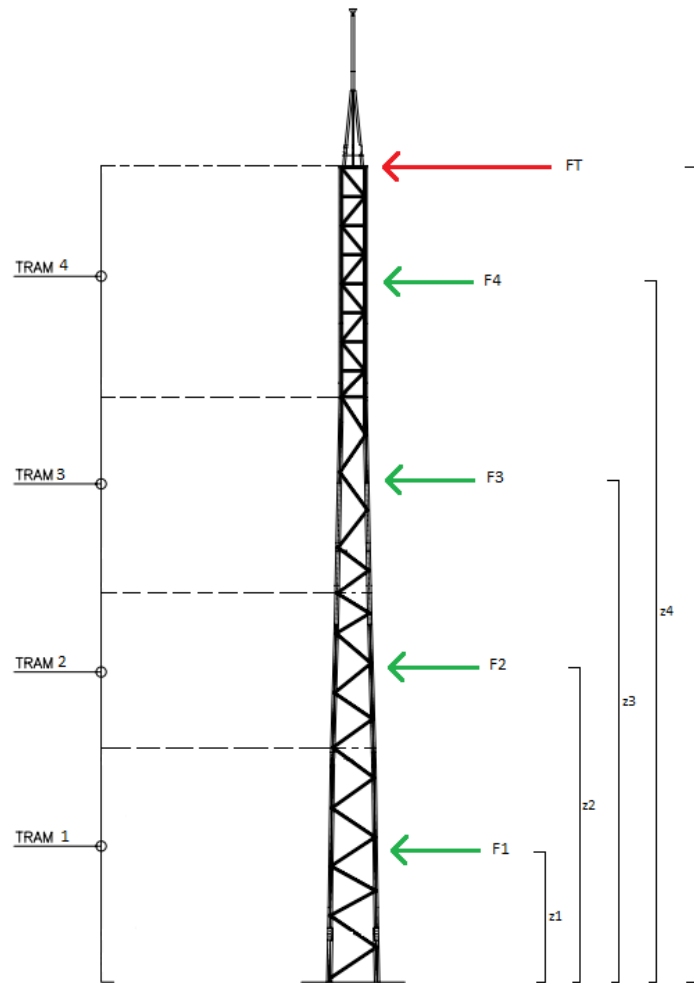


Ilustración 18. Esquema de fuerzas (Fuente: Cellnex)

El esquema ilustrado representa la fuerza de viento por tramo, situada en el centro de cada tramo, junto con su altura respecto del nivel del suelo. También es trazada la fuerza total resultante, fruto de las fuerzas por tramo, que se concentra en lo alto de la estructura.

La ecuación descriptiva de la fuerza total resultante de viento es la siguiente:

$$F_T = \frac{M_T}{z} \quad (52)$$

donde

$F_T$  es la fuerza total.  
 $z$  es la altura de la fuerza respecto del nivel del suelo.  
 $M_T$  es el momento total, que viene descrito por:

$$M_T = M_1 + M_2 + M_3 + M_4 \quad (53)$$

con

$M_1, M_2, M_3, M_4$  son los momentos del tramo 1, 2, 3 y 4, respectivamente.



Partiendo de la misma ecuación 52 de la fuerza resultante y aislando el momento, determinamos cual es el momento de fuerza correspondiente a cada uno de los tramos de estudio.

TRAMO	$M \text{ (Nm)}$			
	Cara 1		Cara 2	
	0°	45°	0°	45°
1	1.169,73	1.296,59	1.169,73	1.296,59
2	3.710,26	4.047,41	3.986,28	4.336,93
3	5.537,83	6.002,26	5.537,83	6.002,26
4	12.835,98	14.367,81	12.835,98	14.367,81
TRAMO	Cara 3		Cara 4	
	0°	45°	0°	45°
	0°	45°	0°	45°
1	1.169,73	1.296,59	1.169,73	1.296,59
2	3.710,26	4.047,41	3.710,26	4.047,41
3	5.537,83	6.002,26	5.191,98	5.656,95
4	12.835,98	14.367,81	12.835,98	14.367,81

Tabla 57. Momentos de fuerza

NOTA – Obsérvese la similitud de valores de momento de fuerza en los tramos de la estructura. Al igual que en el caso de las fuerzas, esta similitud se debe a la casi simetría de las caras junto con la disposición de los auxiliares.

Entonces, con los momentos por tramo parametrizados en la tabla 57 y aplicando la expresión 53 del momento total:

	$F_T \text{ (N)}$			
	Cara 1	Cara 2	Cara 3	Cara 4
0°	1.442,99	1.460,12	1.442,99	1.421,53
45°	1.595,66	1.613,63	1.595,66	1.574,23

Tabla 58. Fuerza total resultante

Según las hipótesis de la ilustración 17, las fuerzas totales de la tabla 58 hacen referencia a:

	(KN)
F1	1,42
F2	1,57
F3	1,44
F4	1,60
F5	1,46
F6	1,61
F7	1,44
F8	1,60

Tabla 59. Fuerzas de hipótesis

### 10.3. Cómputo de comprobación

Con las fuerzas resultantes obtenidas en la tabla 59 procedemos a la evaluación de la respuesta de la antena frente a su ataque.

Primeramente, con la geometría descrita y generada en *Cype* en el apartado 10.1. deberemos añadir las hipótesis mencionadas.

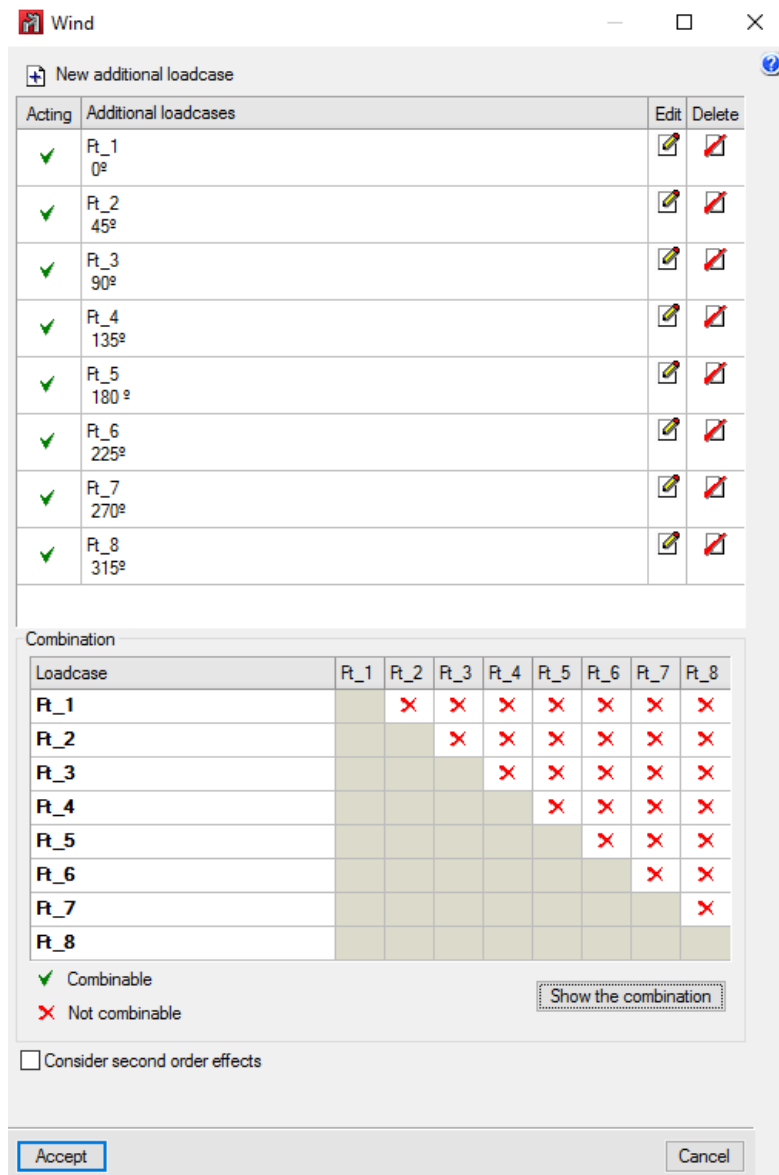


Ilustración 19. Hipótesis de viento (Fuente: Cype)

Una vez establecidas, y comprobando que estas no se combinen las unas con las otras (ilustración 19), estableceremos la dirección de la fuerza, el punto de aplicación y su valor.

El punto de aplicación será el generado en la base superior de la estructura, por lo que se introducirán las cargas de manera nodal en el nodo central de la cruz diseñada.

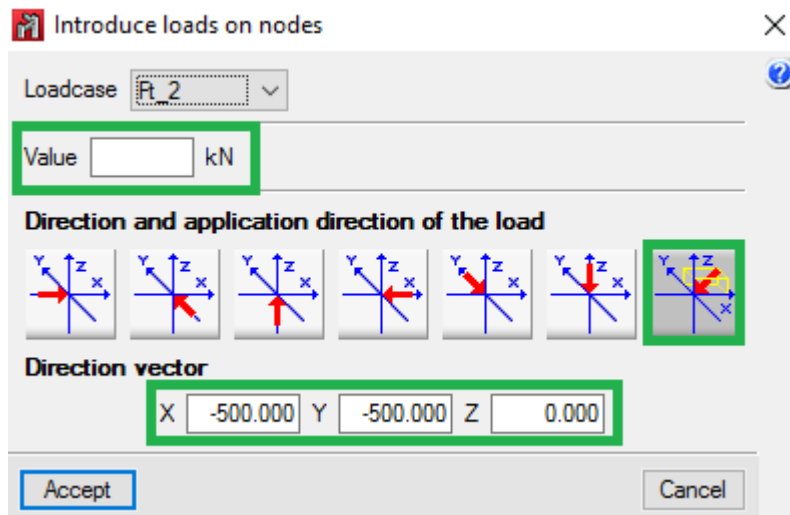


Ilustración 20. Inserción de carga diagonal en el nodo (Fuente: Cype)

Llegados a este punto, lo único que hace falta es calcular y comprobar el estado de la antena después del ataque considerado.

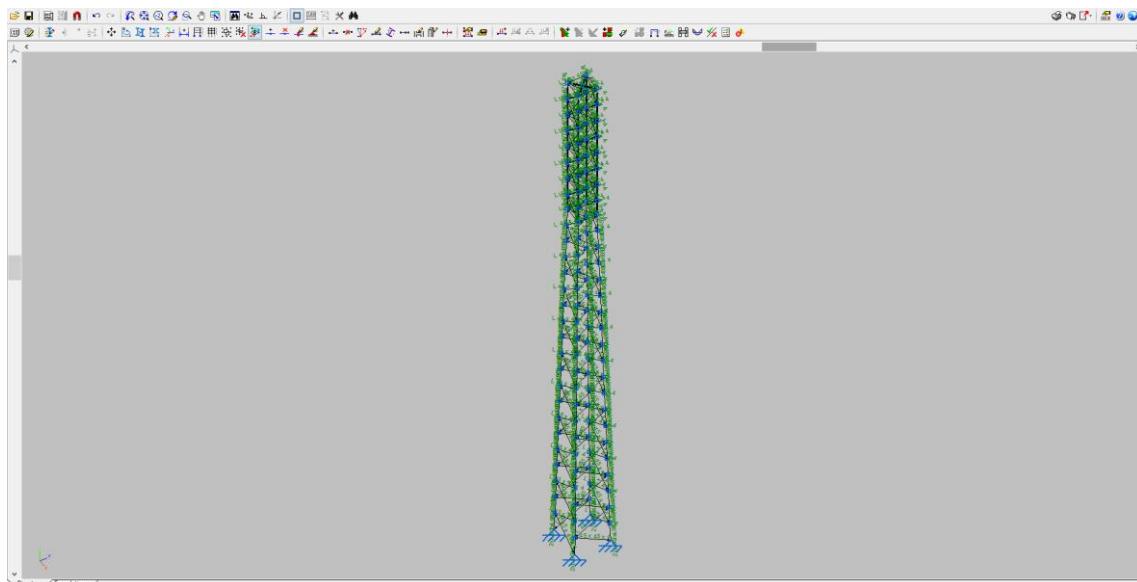


Ilustración 21. Estructura cumple (Fuente: Cype)

En la ilustración 21 se muestra que la estructura cumple en todas sus secciones y componentes.

Es posible la comprobación individual de cada uno de los perfiles por separado, aunque todos y cada uno de ellos cumplen estrictamente la tensión soportada.

N14/N18 (x: 0.288 m)

Section: L 70 x 70 x 6 Material: Steel (S275 (EN 1993-1-1))										
Nodes		Length (m)	Mechanical characteristics							
Initial	Final		Area (cm <sup>2</sup> )	I <sub>y</sub> <sup>(1)</sup> (cm <sup>4</sup> )	I <sub>z</sub> <sup>(1)</sup> (cm <sup>4</sup> )	I <sub>yz</sub> <sup>(4)</sup> (cm <sup>4</sup> )	I <sub>t</sub> <sup>(2)</sup> (cm <sup>4</sup> )	y <sub>c</sub> <sup>(3)</sup> (mm)	z <sub>c</sub> <sup>(3)</sup> (mm)	α <sup>(5)</sup> (degrees)
N14	N18	0.575	8.13	36.88	36.88	21.72	0.96	15.70	-15.70	-45.0
Notes: <sup>(1)</sup> Inertia with respect to the indicated axis <sup>(2)</sup> Uniform torsional moment of inertia <sup>(3)</sup> Centre of gravity coordinates <sup>(4)</sup> Product of inertia <sup>(5)</sup> Is the angle between the main axis of inertia U with respect to the Y axis, positive in the counter-clockwise sense.										
			Buckling		Lateral buckling					
			XY plane	XZ plane	Top fl.	Bot. fl.				
β			1.00	1.00	0.00	0.00				
L <sub>K</sub>			0.575	0.575	0.000	0.000				
C <sub>m</sub>			1.000	1.000	1.000	1.000				
C <sub>1</sub>			-		1.000					
Notation: β: Buckling coefficient L <sub>K</sub> : Buckling length (m) C <sub>m</sub> : Moment coefficient C <sub>1</sub> : Critical moment modification factor										

### Resistance to axial tension (Eurocode 3 EN 1993-1-1: 2005, Article 6.2.3)

The following criteria must be satisfied:

$$\eta = \frac{N_{t,Ed}}{N_{t,Rd}} \leq 1$$

$$\eta : \underline{0.040} \quad \checkmark$$

The worst case design force occurs for load combination SW+1.5·Ft\_2.

**N<sub>t,Ed</sub>**: Worst case design axial tensile force.

$$N_{t,Ed} : \underline{9.02} \text{ kN}$$

The design tensile resistance **N<sub>t,Rd</sub>** is given by:

$$N_{t,Rd} = A \cdot f_{yd}$$

$$N_{t,Rd} : \underline{223.58} \text{ kN}$$

Where:

**A**: Gross transverse section of the bar.

$$A : \underline{8.13} \text{ cm}^2$$

**f<sub>yd</sub>**: Steel design strength.

$$f_{yd} : \underline{275.00} \text{ MPa}$$

$$f_{yd} = f_y / \gamma_{Mo}$$

Where:

**f<sub>y</sub>**: Yield strength. (Eurocode 3 EN 1993-1-1: 2005, Table 3.1)

$$f_y : \underline{275.00} \text{ MPa}$$

**γ<sub>Mo</sub>**: Partial safety factor of the material.

$$\gamma_{Mo} : \underline{1.00}$$

Ilustración 22. Comprobación perfil montante (Fuente: Cype)

### 10.3.1. Deformación

Indagando en el tema de la deformación resultante del ataque de viento actuante sobre la estructura, con el empleo de Cype ha sido posible la determinación de las deformaciones en los tres ejes.

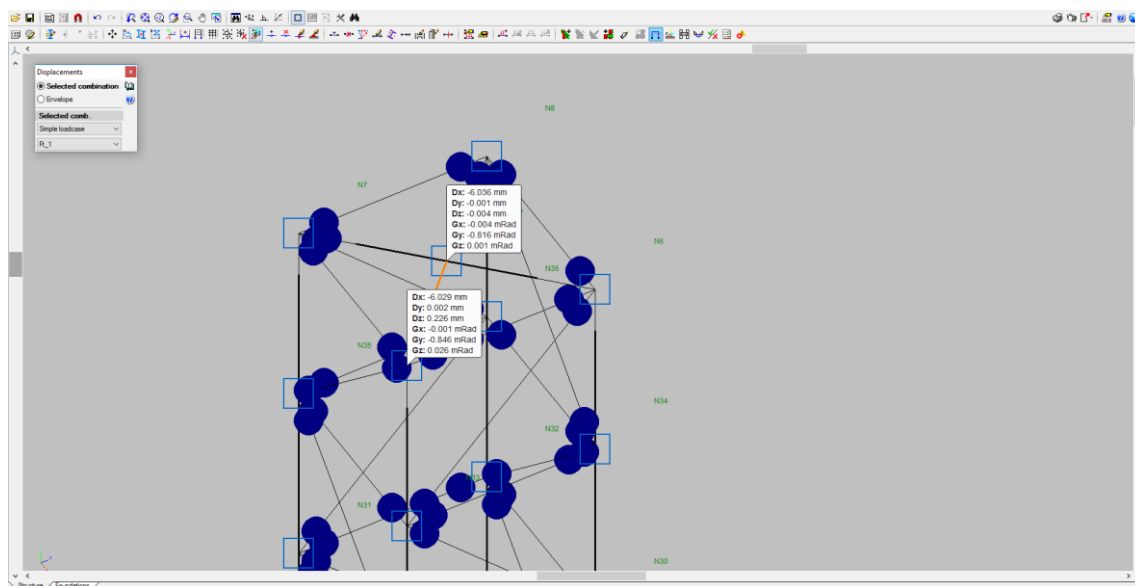


Ilustración 23. Desplazamientos de la hipótesis 1 (Fuente: Cype)

En la ilustración 23 se muestra que, en base a la hipótesis generada (incluyendo en todos los casos la fuerza del peso propio de los perfiles de la estructura), aparecen los desplazamientos de, en este caso, el nudo de la base superior objeto de estudio del programa.

A continuación, se muestran tabulados los desplazamientos según la hipótesis requerida:

	$kN$	$D_x (mm)$	$D_y (mm)$	$D_z (mm)$
$F1$	1,42	-6,036	-0,001	-0,056
$F2$	1,57	-4,72	-4,72	-0,054
$F3$	1,44	-0,001	-6,122	-0,051
$F4$	1,60	4,808	-4,809	-0,048
$F5$	1,46	6,206	0,001	-0,047
$F6$	1,61	4,839	4,841	-0,049
$F7$	1,44	0,001	6,122	-0,053
$F8$	1,60	-4,809	4,809	-0,056

Tabla 60. Desplazamientos del nudo superior

## 11. Comprobación a flexión simple

La estructura, tal y como hemos sido capaces de comprobar anteriormente, resiste la carga de viento soportada, presenta leves deformaciones en el punto de aplicación de la fuerza y sus perfiles constituyentes presentan aprovechamientos relativamente pequeños.

De todos modos, es necesario comprobar por flexión simple la respuesta de los perfiles con tal de asegurar un correcto funcionamiento y respuesta al ataque solicitado. Deberíamos comprobar todas y cada una de las secciones de las barras de la estructura, pero pudiendo únicamente verificar el comportamiento de aquella más crítica ahorraremos cantidades de cálculo, corroborando igualmente el uso del resto de perfiles si el más crítico resiste.

La sección crítica adecuada es referente a la diagonal más larga de la torre de celosía que, en nuestro caso, es la primera diagonal desde el suelo, con una longitud de 1185,50 mm.

Elementos de chapa comprimidos internos						
				Eje de flexión		
Clase	Chapa flectada	Chapa comprimida	Chapa flexo-comprimida			
Ley de tensiones en las chapas (compresión positiva)						
1	$c/t \leq 72\varepsilon$	$c/t \leq 33\varepsilon$	cuando $\alpha > 0,5$ : $c/t \leq \frac{396\varepsilon}{13\alpha - 1}$ cuando $\alpha \leq 0,5$ : $c/t \leq \frac{36\varepsilon}{\alpha}$			
2	$c/t \leq 83\varepsilon$	$c/t \leq 38\varepsilon$	cuando $\alpha > 0,5$ : $c/t \leq \frac{456\varepsilon}{13\alpha - 1}$ cuando $\alpha \leq 0,5$ : $c/t \leq \frac{41,5\varepsilon}{\alpha}$			
Ley de tensiones en las chapas (compresión positiva)						
3	$c/t \leq 124\varepsilon$	$c/t \leq 42\varepsilon$	cuando $\psi > -1$ : $c/t \leq \frac{42\varepsilon}{0,67 + 0,33\psi}$ cuando $\psi \leq -1$ : $c/t \leq 62\varepsilon(1 - \psi)\sqrt{(-\psi)}$			
$\varepsilon = \sqrt{235/f_y}$	$f_y$	235	275	355	420	460
	$\varepsilon$	1,00	0,92	0,81	0,75	0,71

Tabla 61. Clase de sección (Fuente: Código Técnico de la Edificación<sup>22</sup>)

<sup>22</sup> Gobierno de España, 'DB SE- AE Seguridad Estructural, Acciones En La Edificación.', *Boletín Oficial Del Estado*, 2009, 1-42.

Los factores que se tienen en cuenta en la tabla 61 a la hora de escoger la clase de la sección son el factor de reducción  $\varepsilon$  y el límite de esbeltez  $c/t$  en función del grosor y longitud.

$$\varepsilon = \sqrt{\frac{235}{f_y}} \quad (54)$$

donde

$f_y$  es la tensión de límite elástico en  $\frac{N}{mm^2}$ .

El CTE (Código Técnico de la Edificación) establece que, para un acero S275, la tensión de límite elástico  $f_y$  es de  $275 \frac{N}{mm^2}$ . Entonces, al ser este tipo de acero el equivalente al A42b (véase capítulo 10), se tomará el mismo valor de tensión.

Aplicando la ecuación 54 para el factor de reducción:

$$\varepsilon = 0,92$$

Considerando las dimensiones del perfil de la tabla 3 y la tabla 61:

$$c/t = 11,25 \leq 72\varepsilon \rightarrow \text{Clase 1}$$

<b>Clase 1: Plástica</b>	Permiten la formación de la rótula plástica con la capacidad de rotación suficiente para la redistribución de momentos.
<b>Clase 2: Compacta</b>	Permiten el desarrollo del momento plástico con una capacidad de rotación limitada.
<b>Clase 3: Semicompacta o Elástica</b>	En la fibra más comprimida se puede alcanzar el límite elástico del acero pero la abolladura impide el desarrollo del momento plástico
<b>Clase 4: Esbelta</b>	Los elementos total o parcialmente comprimidos de las secciones esbeltas se abollan antes de alcanzar el límite elástico en la fibra más comprimida.

Tabla 62. Clasificación de secciones transversales solicitadas por momentos flectores (Fuente: Código Técnico de la Edificación)

Una vez determinada la clase plástica (tabla 62) de la sección procederemos a la comprobación por flexión simple<sup>23</sup>:

$$\frac{M_{y,Rd}}{W_{pl,y}} \leq f_{yd} \quad (55)$$

donde

$M_{y,Rd}$  es la resistencia de la sección bruta.

$W_{pl,y}$  es el módulo resistente plástico correspondiente a la fibra con mayor tensión.

$f_{yd}$  es la resistencia de cálculo, definida por el cociente de la tensión de límite elástico y el coeficiente de seguridad del metal.

La resistencia de cálculo viene expresada por la tensión de límite elástico y el coeficiente de seguridad, variable en cada tipo de metal.

<sup>23</sup> Gobierno de España.

$$f_{yd} = \frac{f_y}{\gamma_M} \quad (56)$$

donde

$\gamma_M$  es el coeficiente de seguridad parcial para determinar la resistencia.

En el ámbito de estudio propuesto, la flexión simple es equiparable a un fenómeno de inestabilidad, por lo que el CTE establece:

$$\gamma_M = \gamma_{M1} = 1,05 \rightarrow f_{yd} = \frac{275}{1,05} = 261,91 \left( \frac{N}{mm^2} \right) = 261,91 \cdot 10^6 \left( \frac{N}{m^2} \right)$$

El módulo resistente viene determinado por el fabricante, en este caso *ArcelorMittal*. El perfil de las barras diagonales (apartado 3.3.1.) ofrece:

$$W_{el,y} = W_{el,z} = 1,97 \cdot 10^3 mm^3 = 1,97 \cdot 10^{-6} m^3$$

NOTA – De forma conservadora, se toma el módulo resistente elástico para la comprobación a flexión.

Para el cálculo de la resistencia de la sección bruta  $M_{y,Rd}$ , será necesario conocer cuál es la fuerza distribuida en el tramo 1, tramo donde se encuentra alojado el perfil objeto de estudio.

Evaluaremos la fuerza de viento en el tramo 1 a 45° extraída de la tabla 56. Esta carga es idéntica en las cuatro caras de la estructura y la mayor soportada por el tramo de estudio, razón por la cual ha sido seleccionada, de nuevo, para el caso más crítico.

Será necesario obtener la fuerza distribuida a lo largo del tramo. De la tabla 30 se extrae el valor del área del tramo 1 con el que se procede al cálculo:

$$F_w = \frac{559,36}{0,82} = 685,25 \frac{N}{m^2}$$

Considerando al perfil diagonal como una barra biapoyada con una carga lineal, el momento de resistencia de la sección bruta viene dado por:

$$M_{y,Rd} = \frac{P \cdot L^2}{8} \quad (57)$$

donde

$P$  es la carga lineal = 685,25 N/m<sup>2</sup>.

$L$  es la longitud de la viga = 1185,50 mm.

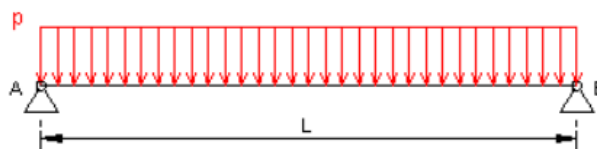


Tabla 63. Viga biapoyada con carga lineal (Fuente: "Cálculo de momentos flectores")

$$M_{y,Rd} = 120,38 Nm$$



Finalmente, con la ecuación 55 ya somos capaces de comprobar si el perfil mayor en diagonal de la estructura resiste a flexión simple:

$$\frac{M_{y,Rd}}{W_{pl,y}} \leq f_{yd} \rightarrow \frac{120,38}{1,97 \cdot 10^{-6}} = 61,11 \cdot 10^6 \leq f_{yd} = 261,91 \cdot 10^6$$

## Análisis del impacto ambiental

Para la realización del proyecto ha sido única y exclusivamente necesario el empleo de un ordenador portátil, a excepción de un solo traslado desde *Sant Andreu de Llavaneres* a *Dosrius*, localidad donde se encuentra la antena GSM.

El ordenador portátil utilizado se trata de un PC de gama media, con un consumo de 220 W. De media, se ha hecho de él una media de 3 horas diarias durante un transcurso medio total de 100 días, por lo que:

$$220 \text{ W} \cdot 100 \text{ días} \cdot \frac{3 \text{ horas}}{1 \text{ día}} = 66 \text{ kWh}$$

El Ministerio de Energía<sup>24</sup> del estado español establece que 1 kWh equivale a la emisión de 0,331 kg de Co<sub>2</sub>. Por lo tanto, el impacto ambiental del ordenador es:

$$66 \text{ kWh} \cdot \frac{0,331 \text{ kg de Co}_2}{1 \text{ kWh}} = 21,85 \text{ kg de Co}_2$$

Por otro lado, el vehículo empleado para el transporte desde *Sant Andreu de Llavaneres* a *Dosrius*, cuya separación es de 19,2 km, ha sido una motocicleta impulsada por un motor a gasolina. Los motores de gasolina emiten 2,3 kg de Co<sub>2</sub><sup>25</sup> por cada litro de gasolina quemado.

Según el consumo del vehículo, este gasta 6l/100 km. Entonces, con los datos anteriores, ya es posible el análisis de su impacto ambiental:

$$2 \cdot 19,2 \text{ km} \cdot 6 \frac{\text{litros}}{100 \text{ km}} \cdot \frac{2,3 \text{ kg de Co}_2}{1 \text{ litro}} = 5,3 \text{ kg de Co}_2$$

Entonces, en su totalidad, el impacto ambiental generado por la realización del proyecto es la suma del impacto del ordenador portátil más la del vehículo de transporte:

$$\text{Impacto ambiental} = 27,15 \text{ kg de Co}_2$$

---

<sup>24</sup> Ecoembes.

<sup>25</sup> Emisión de CO<sub>2</sub> Por Kilómetro Recorrido.

## Conclusiones

La antena GSM de *Dosrius* ha soportado las cargas establecidas del caso principal.

Este caso principal era, según se ha descrito al inicio del capítulo 8, el más crítico de los esfuerzos de viento posibles sobre la estructura: Tiene en cuenta velocidades máximas registradas tanto del 2019 como de años anteriores y valora el registro de temperaturas mínimas en lugar de las medias con el fin de aumentar la presión correspondiente a la velocidad de pico y, consecuentemente, incrementar el valor de la fuerza de viento.

Con estas condiciones establecidas, la torre de celosía ha soportado con creces el peor caso de ataque de viento al cual puede encontrarse sometida, experimentando unos desplazamientos mínimos en el nodo central de la base superior de la estructura.

Podemos concluir que, aun no habiendo valorado los parámetros de la normativa europea al pie de la letra (evaluación del caso más estricto), la construcción presenta las condiciones adecuadas para su uso en la localización geográfica en la que se encuentra situada. De todas maneras, si se hubiera simulado el caso según norma (velocidades medias de registro), estos serían igualmente bastante restrictivos, dando origen a resultados muy superiores a los existentes en la realidad.

La estructura, al superar el caso principal establecido, se mantiene estable según lo establecido en la normativa europea, razón que conlleva a afirmar su correcta metodología de uso.



*Ilustración 24. Antena (Fuente: Alberto Lloveras)*

## Presupuesto

El impacto económico de este trabajo tiene en cuenta aspectos de diseño y simulación.

Por un lado, es necesaria la evaluación del tiempo dedicado, por parte del ingeniero, a todos los cálculos y simulaciones realizadas durante toda la duración del proyecto. De igual manera, es considerable a su vez las licencias de *Cype* y *Microsoft Excel*, ambos programas requeridos de la adquisición de licencia anual.

Concepto	Cantidad	Coste unitario	Coste total (€)
Horas de diseño	100	20 €/h	2.000
Horas de simulación	48	30 €/h	1.440
licencia Cype	1	1.890 € <sup>26</sup>	1.890
licencia Excel	1	99 €	99
			5.429

Tabla 64. Presupuesto

<sup>26</sup> 'Software de CYPE Ingenieros Para Arquitectura, Ingeniería y Construcción'.

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## Anexo A. Valores adicionales

En el anejo A se muestran el conjunto de valores referentes a los diferentes casos de estudio posibles, a excepción del caso principal de estudio, definido en el apartado 8.

Es a partir del apartado 8 que se muestran dichos resultados posibles de todos y cada uno de los parámetros actuantes directa e indirectamente sobre la ecuación de la fuerza de viento ejercida sobre la estructura. Aquellos apartados previos al octavo muestran el abanico entero de posibilidades de cálculo existentes.

### Frecuencia y densidades adimensionales

TRAMO	Velocidad media del 2019	
	$f_L(z_s, n_{1,x})$	$S_L(z_s, n_{1,x})$
1	45,17	0,01
2	53,04	0,01
3	59,24	0,01
4	65,92	0,01
5	69,78	0,01

Tabla 65. Frecuencias y densidades adimensionales con velocidad media

### Decremento logarítmico aerodinámico

TRAMO	Velocidad media	Velocidad media	Velocidad máxima
	Temperatura media	Temperatura mínima	Temperatura media
	$\delta_a$		
1	0,02	0,02	0,04
2	0,02	0,02	0,05
3	0,03	0,03	0,06
4	0,01	0,01	0,03

Tabla 66. Decremento logarítmico aerodinámico para los casos adicionales

## Factor de respuesta debido a la resonancia

	Velocidad media	Velocidad media	Velocidad máxima
	Temperatura media	Temperatura mínima	Temperatura media
TRAMO	$R^2$		
1	0,00	0,00	0,02
2	0,00	0,00	0,01
3	0,00	0,00	0,01
4	0,00	0,00	0,02

Tabla 67. Factor de respuesta debido a la resonancia

## Factor de pico y frecuencia media de oscilación

	Velocidad media	Velocidad media	Velocidad máxima
	Temperatura media	Temperatura mínima	Temperatura media
TRAMO	$k_p$		
1	3,52	3,52	3,76
2	3,46	3,46	3,69
3	3,44	3,43	3,66
4	3,54	3,54	3,75
5	-	-	-

Tabla 68. Factores de pico de cada caso

	Velocidad media	Velocidad media	Velocidad máxima
	Temperatura media	Temperatura mínima	Temperatura media
TRAMO	$\nu$		
1	0,44	0,44	1,06
2	0,36	0,36	0,82
3	0,33	0,33	0,73
4	0,48	0,47	1,01
5	-	-	-

Tabla 69. Frecuencias medias de oscilación de cada caso

## Funciones de admitancia aerodinámica

TRAMO	Velocidad media			
	$\eta_h$	$\eta_b$	$R_h$	$R_b$
1	29,68	6,69	0,03	0,14
2	45,60	5,04	0,02	0,18
3	60,43	3,90	0,02	0,22
4	78,76	2,69	0,01	0,30
5	90,49	2,60	0,01	0,32

Tabla 70. Funciones de admitancia aerodinámica de cada caso

## Factor estructural

TRAMO	Velocidad media	Velocidad media	Velocidad máxima
	Temperatura media	Temperatura mínima	Temperatura media
	$c_s c_d$		
1	0,93	0,93	0,97
2	0,94	0,94	0,98
3	0,94	0,94	0,98
4	0,96	0,96	1,00
5	-	-	-

Tabla 71. Factor estructural de cada caso

## Fuerza de viento

TRAMO	$F_w (N)$ para velocidad media y temperatura media			
	Cara 1		Cara 2	
	0°	45°	0°	45°
1	89,60	99,39	89,60	99,39
2	103,91	113,42	111,64	121,54
3	100,64	109,15	100,64	109,15
4	166,23	186,28	166,23	186,28
TRAMO	Cara 3		Cara 4	
	0°	45°	0°	45°
	0°	45°	0°	45°
1	89,60	99,39	89,60	99,39
2	103,91	113,42	103,91	113,42
3	100,64	109,15	94,36	102,87
4	166,23	186,28	166,23	186,28

Tabla 72. Fuerza de viento para velocidad y temperatura media



$F_w (N)$ para velocidad media y temperatura mínima				
	Cara 1		Cara 2	
TRAMO	0°	45°	0°	45°
1	92,38	102,47	92,38	102,47
2	107,13	116,93	115,10	125,30
3	103,76	112,53	103,76	112,53
4	171,37	192,04	171,37	192,04
	Cara 3		Cara 4	
TRAMO	0°	45°	0°	45°
1	92,38	102,47	92,38	102,47
2	107,13	116,93	107,13	116,93
3	103,76	112,53	97,28	106,06
4	171,37	192,04	171,37	192,04

Tabla 73. Fuerza de viento para velocidad media y temperatura mínima

$F_w (N)$ para velocidad máxima y temperatura media				
	Cara 1		Cara 2	
TRAMO	0°	45°	0°	45°
1	489,55	542,65	599,73	542,65
2	564,66	615,98	1.058,76	660,04
3	545,33	591,08	1.068,53	591,08
4	899,01	1.006,32	1.091,48	1.006,32
	Cara 3		Cara 4	
TRAMO	0°	45°	0°	45°
1	489,55	542,65	489,55	542,65
2	564,66	615,98	564,66	615,98
3	545,33	591,08	511,27	557,07
4	899,01	1.006,32	899,01	1.006,32

Tabla 74. Fuerza de viento para velocidad máxima y temperatura media

## Fuerza de viento resultante

$F_T (N)$ para velocidad media y temperatura media				
	Cara 1	Cara 2	Cara 3	Cara 4
0°	258,40	261,46	258,40	254,56
45°	286,02	289,23	286,02	282,18

Tabla 75. Fuerza de viento resultante para velocidad media y temperatura media

$F_T (N)$ para velocidad media y temperatura mínima				
	Cara 1	Cara 2	Cara 3	Cara 4
0°	266,40	269,56	266,40	262,44
45°	294,87	298,17	294,87	290,91

Tabla 76. Fuerza de viento resultante para velocidad media y temperatura mínima

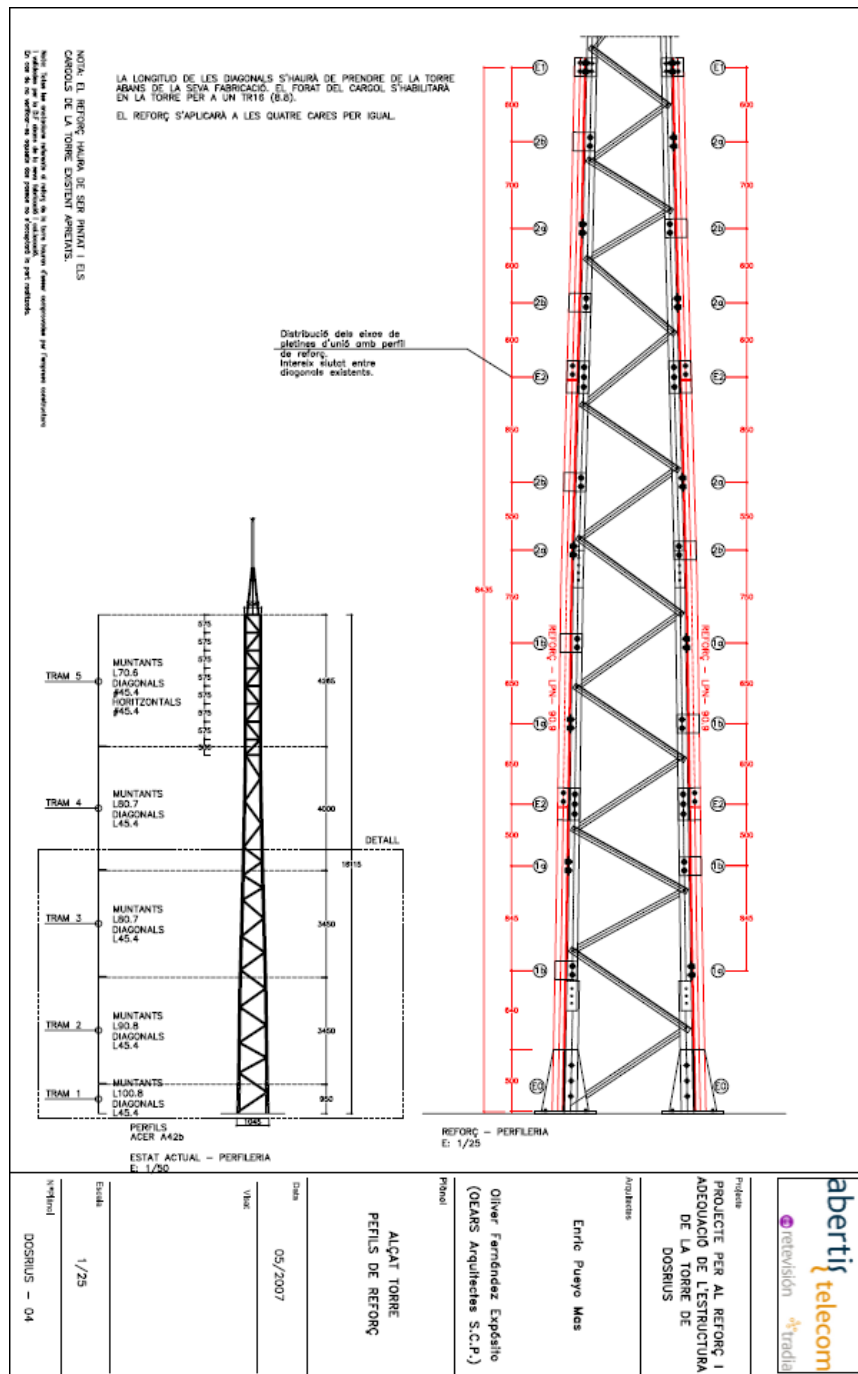
$F_T (N)$ para velocidad máxima y temperatura media				
	Cara 1	Cara 2	Cara 3	Cara 4
0°	1.399,94	1.416,56	1.399,94	1.379,12
45°	1.548,09	1.565,52	1.548,09	1.527,30

Tabla 77. Fuerza de viento resultante para velocidad máxima y temperatura media

## Anexo B. Planos

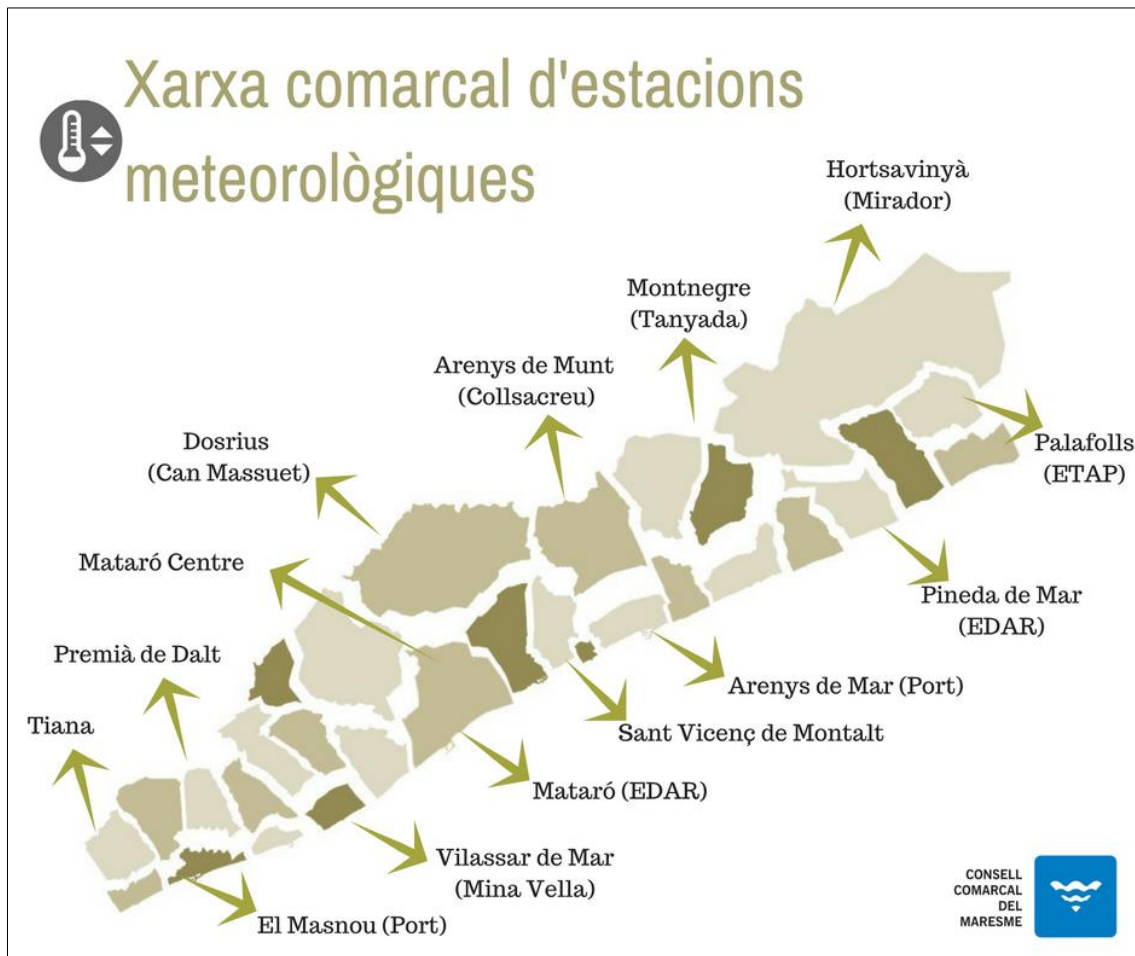
En el anexo B se mostrarán todos los planos topográficos y de la estructura relevantes a la toma de valores y condiciones de contorno para los cálculos realizados.

### Estructura



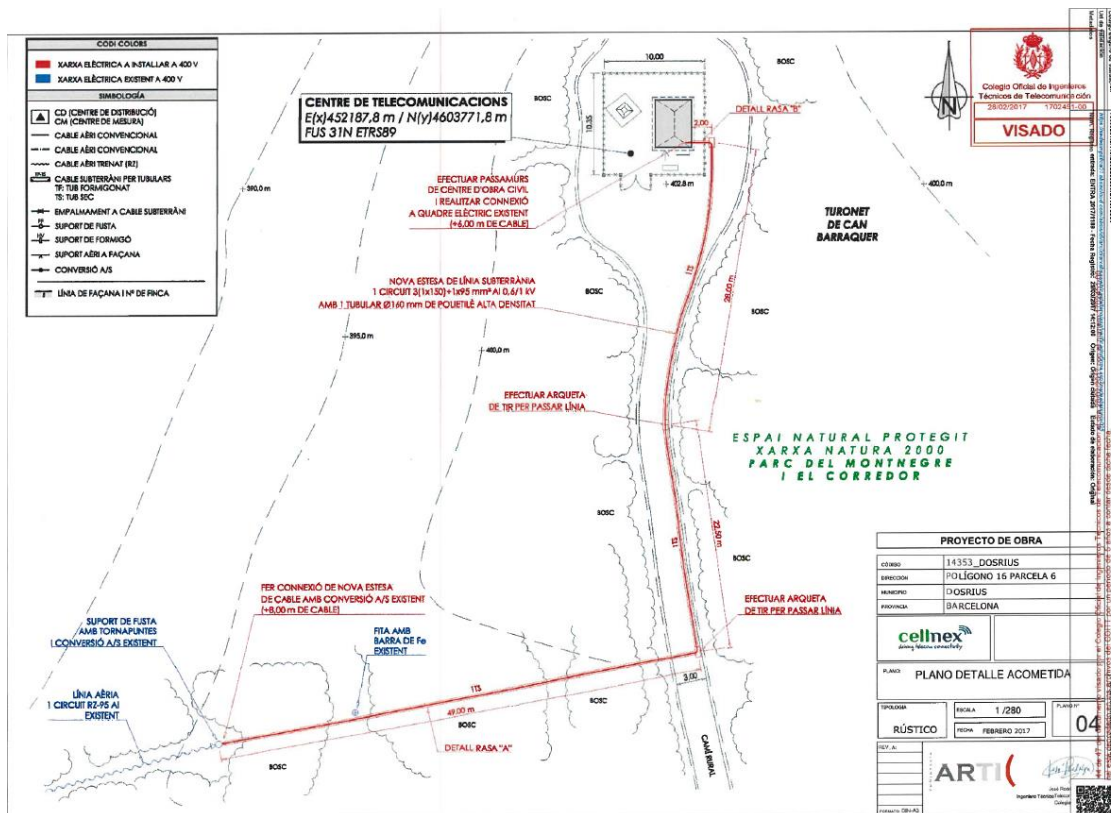
Plano 1. Antena GSM

## Red comarcal de estaciones meteorológicas



Plano 2. Estaciones meteorológicas

## Topografia



Plano 3. Zona geográfica

## Anexo C. Datos de viento

En el anexo C se encuentran los registros de viento a partir de los cuales se han hecho los cálculos correspondientes.

### Estación meteorológica de Arenys de Mar

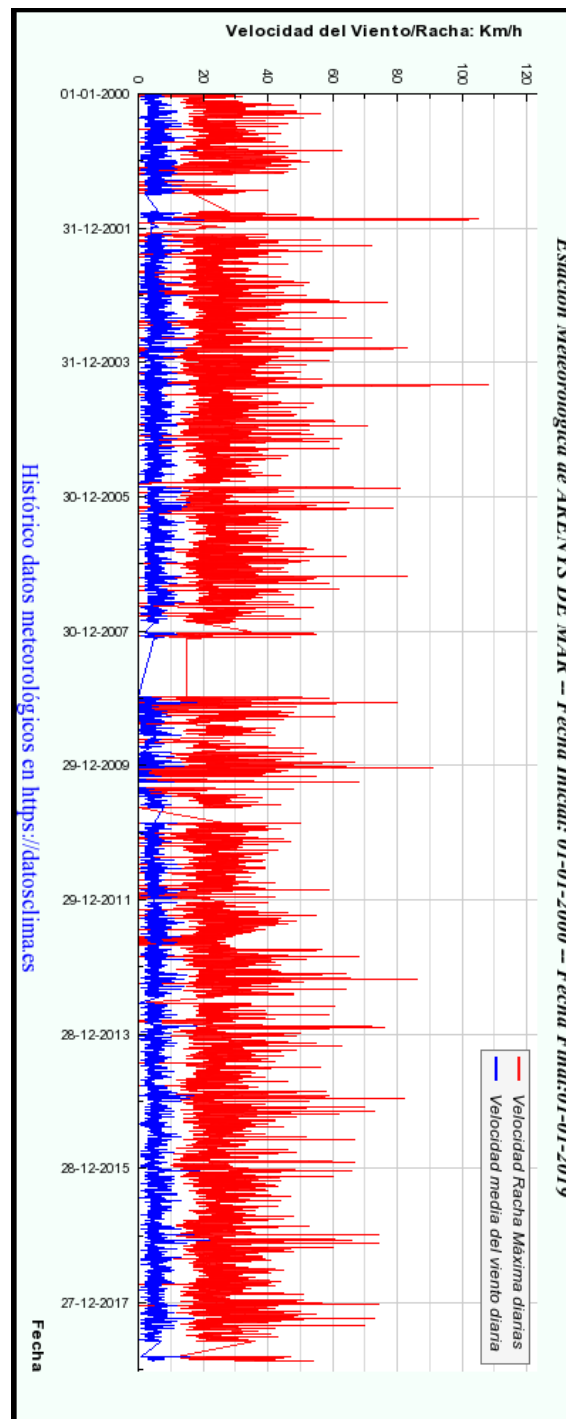


Gráfico 6. Registro de viento 2000 – 2019

## Estación de Can Massuet

MONTHLY CLIMATOLOGICAL SUMMARY for JAN. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	10.0	13.2	13:41	5.7	22:15	8.3	0.0	0.0	2.1	6.7	23:31	N
2	7.9	11.8	11:37	4.8	2:07	10.4	0.0	0.0	1.6	6.7	16:30	N
3	7.3	10.6	12:30	4.2	5:24	11.1	0.0	0.0	1.4	6.3	12:59	N
4	5.8	9.3	12:53	3.5	7:28	12.6	0.0	0.0	1.8	7.2	7:36	N
5	7.2	12.4	12:48	2.4	4:48	11.2	0.0	0.0	2.4	8.9	8:25	N
6	10.2	15.1	15:35	5.4	6:35	8.1	0.0	0.0	2.2	8.9	5:02	N
7	7.1	11.3	13:44	3.9	6:37	11.3	0.0	0.0	1.6	8.5	11:32	N
8	5.1	10.1	14:17	0.0	7:36	13.3	0.0	0.0	1.7	6.3	4:59	N
9	5.9	11.8	13:17	2.4	7:25	12.4	0.0	0.0	2.2	11.6	21:55	N
10	4.0	7.9	13:18	1.6	7:42	14.3	0.0	0.0	2.6	12.1	0:50	N
11	2.3	7.0	12:48	-2.2	6:56	16.1	0.0	0.0	1.5	6.7	3:27	N
12	4.5	9.9	12:34	0.4	3:01	13.8	0.0	0.0	2.2	8.0	20:53	N
13	6.6	11.6	13:45	1.7	5:20	11.7	0.0	0.0	2.4	7.6	19:25	N
14	9.2	15.1	12:41	6.4	0:58	9.1	0.0	0.0	1.3	7.2	7:23	N
15	7.2	12.4	12:03	2.8	6:02	11.1	0.0	0.0	1.3	5.4	19:11	N
16	7.3	11.0	13:54	4.3	6:33	10.6	0.0	0.0	2.3	8.5	14:30	N
17	8.0	13.1	12:43	5.3	6:29	10.3	0.0	0.0	1.5	7.2	15:21	N
18	4.3	7.7	13:49	2.3	23:58	14.1	0.0	0.0	1.5	5.8	22:26	N
19	5.2	9.9	13:02	2.3	0:01	13.1	0.0	0.0	1.7	5.4	0:32	N
20	4.9	6.1	5:34	2.7	23:59	13.4	0.0	9.2	3.4	14.8	14:50	NNE
21	4.4	9.4	13:32	1.2	6:47	13.9	0.0	0.8	2.2	6.7	14:21	N
22	3.2	6.9	13:15	-0.7	6:18	15.2	0.0	0.0	2.0	6.7	21:34	N
23	3.6	8.2	12:25	0.7	5:05	14.7	0.0	0.2	3.2	18.3	23:57	N
24	4.7	9.3	14:10	0.9	5:46	13.6	0.0	0.2	4.3	19.7	0:02	N
25	6.6	12.1	13:43	1.6	4:03	11.8	0.0	0.0	1.6	7.2	11:45	N
26	8.5	13.6	13:30	5.4	7:01	9.8	0.0	0.0	1.9	7.2	13:54	N
27	6.9	11.7	14:28	3.1	23:57	11.4	0.0	0.0	2.7	8.5	12:27	N
28	5.1	10.3	12:26	1.4	3:11	13.2	0.0	0.0	3.8	16.1	12:45	N
29	4.3	5.8	10:00	1.9	2:53	14.1	0.0	0.0	2.4	13.4	23:21	N
30	5.2	9.4	13:59	1.7	7:12	13.1	0.0	0.0	3.7	11.2	1:39	N
31	7.9	12.5	15:03	3.8	1:23	10.4	0.0	0.0	3.9	11.2	5:05	N
<hr/>												
	6.1	15.1	6	-2.2	11	377.5	0.0	10.4	2.3	19.7	24	N

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 3

Min <= -18.0: 0

Max Rain: 9.19 ON 20/01/19

Days of Rain: 4 (> .2 mm) 1 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 1. Enero 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for FEB. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	9.3	13.1	12:59	3.6	23:50	9.0	0.0	2.0	3.9	13.0	9:54	N
2	4.2	7.3	15:16	2.4	6:59	14.1	0.0	0.2	2.8	10.7	0:24	N
3	5.0	10.2	14:00	1.8	3:27	13.3	0.0	0.0	2.1	6.7	14:54	N
4	4.9	11.1	13:09	0.1	5:08	13.4	0.0	0.0	1.7	6.3	6:06	N
5	8.2	14.3	13:19	4.0	7:29	10.1	0.0	0.0	1.3	4.9	7:26	N
6	10.1	15.7	13:11	7.1	3:43	8.2	0.0	0.0	1.6	5.4	3:06	N
7	9.0	13.9	13:20	6.1	3:36	9.3	0.0	0.0	1.3	5.8	14:33	N
8	8.4	13.9	14:45	4.4	6:50	9.9	0.0	0.0	2.4	9.4	13:15	N
9	9.2	15.8	13:01	6.1	2:28	9.2	0.0	0.0	1.6	8.0	2:56	N
10	9.6	14.4	15:46	6.0	3:38	8.8	0.0	0.0	4.0	15.6	13:03	N
11	8.3	12.4	13:48	5.8	23:55	10.1	0.0	0.0	1.7	8.0	14:16	N
12	7.6	13.6	15:20	2.6	5:27	10.8	0.0	0.0	2.1	7.2	13:25	N
13	7.5	11.8	14:20	3.9	3:14	10.8	0.0	0.0	2.1	7.6	11:18	N
14	7.0	13.5	13:44	3.4	4:14	11.3	0.0	0.0	2.0	6.7	15:31	N
15	8.6	14.9	14:16	3.3	3:48	9.8	0.0	0.0	2.0	7.2	13:26	N
16	10.3	16.6	12:29	7.3	22:46	8.1	0.0	0.0	1.3	5.8	12:56	N
17	8.3	13.6	13:47	5.1	6:09	10.1	0.0	0.0	1.8	7.2	12:32	N
18	7.9	13.4	13:29	4.4	4:23	10.4	0.0	0.0	1.4	6.3	16:08	N
19	8.3	12.2	11:21	6.3	0:26	10.0	0.0	0.0	2.0	6.7	13:05	N
20	8.0	11.4	15:01	5.8	22:26	10.3	0.0	0.0	1.2	6.3	15:19	N
21	8.2	14.6	13:15	3.9	5:19	10.1	0.0	0.0	1.5	5.8	13:29	N
22	13.9	20.7	12:53	6.8	1:17	4.7	0.2	0.0	2.0	6.7	0:18	N
23	13.1	19.6	13:00	8.9	23:59	5.3	0.0	0.0	2.3	7.6	0:27	N
24	9.1	15.2	12:29	6.4	22:33	9.2	0.0	0.0	2.2	7.2	6:12	N
25	9.9	16.7	13:26	5.2	6:54	8.4	0.0	0.0	1.3	5.4	13:38	N
26	12.4	17.9	11:25	9.0	23:21	5.9	0.0	0.0	1.9	6.7	12:59	N
27	14.2	22.2	13:17	8.6	3:37	4.6	0.4	0.0	1.9	6.7	7:22	N
28	13.9	19.1	12:51	10.2	23:59	4.5	0.0	0.0	2.0	6.3	13:58	NE
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	9.1	22.2	27	0.1	4	259.6	0.6	2.2	2.0	15.6	10	N

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 2.01 ON 01/02/19

Days of Rain: 2 (> .2 mm) 1 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 2. Febrero 2019 (Fuente: Can Massuet)



## MONTHLY CLIMATOLOGICAL SUMMARY for APR. 2019

NAME: CanMassuetDosrius CITY: STATE:  
 ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	11.1	16.7	11:43	8.1	5:11	7.2	0.0	0.0	2.1	8.5	13:59	S
2	11.0	17.1	9:50	7.7	1:22	7.3	0.0	2.0	2.2	7.6	15:26	W
3	8.7	13.0	11:54	3.4	23:07	9.6	0.0	10.8	1.8	9.8	12:26	S
4	5.7	11.4	11:38	0.9	5:51	12.6	0.0	0.0	2.2	9.4	13:31	SSE
5	8.3	10.6	14:40	5.3	1:55	10.1	0.0	4.2	3.0	12.1	14:52	SSW
6	8.2	13.6	14:01	4.4	5:45	10.1	0.0	1.4	3.4	13.4	10:02	W
7	7.8	14.4	11:10	5.1	6:21	10.6	0.0	4.2	2.0	7.6	9:57	NNW
8	10.6	17.3	12:53	5.8	4:34	7.7	0.0	0.0	2.6	9.8	12:19	WNW
9	9.0	12.1	8:24	6.4	18:49	9.3	0.0	2.4	2.4	9.4	16:04	NE
10	9.5	15.9	10:59	6.3	2:08	8.8	0.0	3.0	2.1	8.5	12:47	NNW
11	11.3	16.3	13:14	7.3	5:53	7.0	0.0	0.2	1.9	8.0	14:06	NW
12	10.7	15.0	9:36	7.5	5:28	7.6	0.0	0.0	2.4	10.7	11:29	S
13	11.4	17.4	11:13	7.2	4:24	6.9	0.0	0.0	2.2	7.6	13:26	S
14	11.7	15.2	9:21	8.2	3:54	6.7	0.0	0.0	2.5	9.8	5:52	S
15	10.3	14.3	10:07	6.7	5:35	8.1	0.0	0.0	1.9	7.6	11:12	S
16	10.7	16.3	14:28	7.4	0:11	7.6	0.0	0.0	1.8	7.2	14:59	S
17	11.2	15.8	10:54	7.9	4:06	7.2	0.0	0.0	2.1	7.2	12:15	S
18	11.6	15.1	15:04	9.1	3:04	6.7	0.0	0.0	4.8	15.2	14:17	ENE
19	12.8	16.8	14:02	10.7	5:25	5.5	0.0	0.0	6.0	17.0	11:50	ENE
20	12.3	14.4	11:28	9.1	19:26	6.1	0.0	0.2	5.5	17.4	22:59	ENE
21	12.4	15.1	12:45	10.8	1:00	5.9	0.0	0.0	5.7	17.4	12:30	NE
22	12.1	14.1	9:43	10.3	20:45	6.3	0.0	0.0	5.2	18.8	9:31	NE
23	12.4	16.9	14:35	10.6	0:39	5.9	0.0	1.0	2.7	10.3	16:03	S
24	11.6	15.8	14:58	9.3	6:31	6.7	0.0	0.0	3.7	14.3	13:29	SSW
25	11.7	16.3	13:51	9.9	23:56	6.6	0.0	0.0	3.6	11.2	3:10	SSW
26	11.9	17.2	11:02	8.8	6:03	6.4	0.0	0.0	3.8	13.0	6:13	WNW
27	12.3	17.6	12:01	8.6	5:27	6.1	0.0	0.0	2.2	8.5	12:24	NE
28	10.3	12.7	12:46	8.8	4:26	8.1	0.0	0.0	1.7	8.9	14:34	S
29	11.8	16.9	12:42	9.3	0:39	6.6	0.0	0.0	1.7	7.2	11:25	S
30	13.0	17.8	13:09	9.8	5:25	5.3	0.0	0.0	2.2	8.9	13:35	S
	10.8	17.8	30	0.9	4	226.6	0.0	29.4	2.9	18.8	22	S

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 10.80 ON 03/04/19

Days of Rain: 10 (> .2 mm) 6 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 3. Abril 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for MAY. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	13.7	19.3	12:37	10.0	4:43	4.6	0.0	0.0	2.5	9.4	14:08	W
2	12.8	16.3	9:06	10.8	1:46	5.6	0.0	0.0	2.4	9.4	11:06	S
3	9.3	12.3	7:14	6.9	00:00	9.1	0.0	26.0	1.8	8.5	15:23	NW
4	10.7	16.6	12:05	5.1	4:59	7.7	0.0	0.0	2.6	10.3	23:44	SSE
5	10.3	14.8	10:17	5.7	5:23	8.1	0.0	0.0	3.4	10.3	13:21	SE
6	10.4	15.8	10:44	6.4	5:11	7.9	0.0	0.0	3.1	10.7	13:20	S
7	11.9	16.6	11:20	7.4	4:33	6.4	0.0	0.0	2.6	8.9	12:27	SSW
8	16.0	22.4	15:09	11.9	2:54	2.9	0.6	0.2	2.8	11.6	16:29	WSW
9	13.6	17.9	15:20	10.1	0:57	4.8	0.0	0.0	3.0	9.8	12:54	S
10	16.8	21.8	15:59	13.1	5:06	2.0	0.4	0.0	2.3	8.9	23:43	S
11	15.1	19.1	12:10	11.1	23:28	3.2	0.0	0.0	2.1	9.8	14:59	SSW
12	13.5	18.2	16:43	10.3	4:16	4.8	0.0	0.0	2.1	8.9	13:34	S
13	14.3	20.4	11:58	9.7	4:38	4.2	0.1	0.0	2.3	9.4	12:04	SSW
14	14.2	19.0	9:41	10.4	0:09	4.1	0.0	0.0	2.5	11.6	12:03	S
15	12.8	18.5	9:20	9.1	23:03	5.6	0.0	0.0	3.0	12.5	13:17	SE
16	13.6	19.6	13:56	9.4	2:48	4.8	0.0	0.0	2.9	9.8	14:02	SSW
17	10.8	12.9	15:13	9.1	22:01	7.5	0.0	6.4	2.7	12.1	12:32	NE
18	10.7	14.8	14:51	8.8	5:39	7.7	0.0	0.8	2.2	8.9	10:57	S
19	9.7	15.1	10:32	6.8	4:51	8.6	0.0	2.0	1.8	8.0	12:29	NNW
20	12.3	18.4	11:06	7.4	3:41	6.0	0.0	0.0	2.2	8.0	12:38	S
21	15.0	19.9	11:01	11.0	0:05	3.4	0.1	0.0	2.1	8.5	13:05	NNW
22	15.8	21.5	10:37	10.9	3:42	2.8	0.3	0.0	2.3	7.6	12:50	S
23	16.7	24.0	11:43	12.4	3:21	2.5	0.8	0.0	2.4	8.5	8:51	S
24	13.4	17.0	10:45	11.2	22:56	4.9	0.0	7.2	1.4	7.6	12:32	NNW
25	14.4	22.5	13:45	11.0	1:55	4.1	0.2	1.0	1.9	6.3	7:29	NNW
26	16.4	23.2	15:19	12.3	5:25	2.4	0.6	0.4	1.7	7.2	13:11	WNW
27	16.4	22.6	9:54	12.4	3:07	2.4	0.5	0.0	2.2	8.9	14:08	S
28	14.0	18.8	12:25	12.2	23:58	4.3	0.0	0.0	2.3	10.3	14:23	S
29	14.2	19.3	12:05	10.8	5:09	4.2	0.0	0.0	2.4	10.3	13:15	S
30	15.8	20.7	13:15	11.5	4:49	2.8	0.3	0.0	2.2	7.6	13:35	S
31	18.6	24.0	10:18	13.9	0:43	1.2	1.5	0.0	3.0	10.7	11:29	S
	13.7	24.0	23	5.1	4	150.8	5.4	44.0	2.4	12.5	15	S

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 26.01 ON 03/05/19

Days of Rain: 8 (> .2 mm) 4 (> 2 mm) 1 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 4. Mayo 2019 (Fuente: Can Massuet)

## MONTHLY CLIMATOLOGICAL SUMMARY for JUN. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	19.4	26.1	10:49	14.0	3:42	1.1	2.1	0.0	2.5	8.5	15:15	SSE
2	19.6	25.3	13:57	13.8	3:44	1.1	2.2	0.0	2.9	8.5	10:37	W
3	20.2	27.0	11:03	14.5	4:01	0.9	2.8	0.0	3.1	9.8	12:55	SSW
4	19.9	25.1	12:59	15.1	4:57	0.7	2.3	0.0	2.5	8.5	9:47	SSW
5	18.1	24.3	12:21	12.5	23:57	1.7	1.4	0.0	2.5	15.2	15:03	SSW
6	14.4	18.6	9:42	11.5	3:03	3.9	0.0	0.0	2.5	9.8	11:44	S
7	18.4	25.9	15:27	14.1	4:52	1.8	1.8	0.0	3.2	12.1	14:25	SSW
8	18.3	22.9	13:18	13.4	4:40	1.2	1.1	0.0	3.4	9.8	13:55	NE
9	19.6	26.3	14:04	16.0	22:55	0.3	1.6	0.0	2.9	10.3	9:21	NE
10	18.9	25.7	10:06	14.5	21:30	1.3	1.9	0.0	2.9	11.6	15:22	S
11	11.2	15.0	0:07	8.3	22:30	7.2	0.0	19.8	1.8	9.4	15:38	S
12	8.6	9.3	0:11	7.6	4:36	2.1	0.0	0.0	1.6	4.0	0:25	WNW
13												
14	17.2	18.2	19:53	16.5	23:04	0.2	0.0	0.0	1.9	4.9	00:00	N
15	18.0	22.7	9:56	14.6	3:27	1.3	0.9	0.0	2.7	8.9	14:23	S
16	18.0	23.1	14:00	13.7	4:47	1.4	1.1	0.0	2.6	9.4	11:12	S
17	20.8	28.0	12:52	14.9	1:48	0.6	3.0	0.0	2.3	8.0	13:25	S
18	20.9	27.2	10:13	15.5	2:55	0.5	3.1	0.0	3.0	9.8	12:00	SSW
19	19.8	26.5	10:51	16.4	21:37	0.6	2.1	0.0	2.5	8.9	13:44	S
20	20.6	27.0	11:25	16.5	00:00	0.2	2.4	0.0	2.9	10.7	14:29	S
21	19.6	25.6	9:16	15.4	4:49	0.8	2.1	0.0	2.5	8.9	11:27	S
22	19.9	27.8	11:00	15.9	4:54	0.7	2.2	0.0	2.7	11.6	15:00	SSE
23	21.4	29.3	11:27	16.1	5:37	0.4	3.4	0.0	2.7	9.8	11:05	SSE
24	23.4	29.8	14:10	17.6	1:02	0.1	5.2	0.0	3.0	10.7	14:46	ESE
25	22.8	28.9	11:15	18.7	0:42	0.0	4.5	0.0	4.6	12.1	3:42	ENE
26	27.0	33.4	11:02	21.6	0:12	0.0	8.7	0.0	3.7	12.5	6:13	NE
27	28.3	34.1	12:18	22.9	4:31	0.0	9.9	0.0	1.7	7.2	12:37	S
28	31.2	39.8	13:34	23.4	2:02	0.0	12.9	0.0	2.0	7.2	13:52	NW
29	29.6	34.1	10:54	24.0	22:06	0.0	11.2	0.0	2.6	8.0	13:36	S
30	26.5	32.0	10:52	22.5	23:47	0.0	8.2	0.0	2.2	7.6	14:19	S
	20.4	39.8	28	7.6	12	29.8	98.1	19.8	2.7	15.2	5	S

Max >= 32.0: 5

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 19.81 ON 11/06/19

Days of Rain: 1 (> .2 mm) 1 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 5. Junio (Fuente: Can Massuet)

## MONTHLY CLIMATOLOGICAL SUMMARY for JUL. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	24.2	29.5	10:51	19.3	3:30	0.0	5.8	0.0	2.2	8.5	23:27	S
2	24.3	29.6	11:42	20.5	21:52	0.0	6.0	0.0	2.8	8.5	12:08	S
3	25.5	30.0	17:33	21.1	0:01	0.0	7.2	0.0	2.2	9.4	13:16	NE
4	24.4	29.4	8:31	20.3	23:59	0.0	6.1	0.0	2.2	8.5	13:18	S
5	24.6	31.4	13:29	19.3	4:38	0.0	5.8	0.0	2.5	8.9	11:52	SSW
6	24.8	31.7	10:22	20.2	5:01	0.0	6.5	0.0	2.5	8.5	13:41	S
7	25.2	31.8	11:06	21.4	2:45	0.0	6.8	0.0	2.9	10.7	21:26	S
8	23.5	29.2	11:21	19.4	9:03	0.0	5.2	2.2	2.6	16.1	8:42	N
9	21.3	27.6	12:38	16.1	14:12	0.1	3.1	27.8	2.4	13.0	13:17	NNE
10	22.7	29.1	13:11	17.1	5:25	0.1	4.4	0.0	2.2	8.5	14:03	S
11	23.8	29.7	10:21	19.9	23:51	0.0	5.4	0.0	2.7	8.9	13:52	SE
12	24.1	28.2	9:14	19.9	0:01	0.0	5.8	0.0	2.1	8.9	13:40	S
13	23.8	29.3	12:05	20.2	1:34	0.0	5.5	0.0	2.2	11.2	15:20	S
14	21.2	27.1	8:52	17.4	14:05	0.1	2.9	20.0	2.1	9.8	6:33	NW
15	21.4	25.3	11:27	18.8	23:18	0.0	3.1	0.0	2.4	10.7	12:08	SSW
16	22.1	26.4	10:00	18.0	3:22	0.0	3.7	0.0	3.0	11.6	12:42	NW
17	20.9	28.6	12:33	16.8	20:47	0.2	2.7	7.2	2.2	10.7	17:44	WNW
18	21.3	25.8	11:17	17.6	0:44	0.1	2.9	3.0	2.6	8.9	13:03	S
19	21.5	25.4	11:42	18.8	5:20	0.0	3.2	0.0	2.1	8.9	13:37	S
20	22.4	29.2	10:50	18.1	5:12	0.0	4.1	0.0	2.6	8.9	11:37	S
21	24.3	28.1	14:05	20.1	0:01	0.0	5.9	0.0	2.4	7.6	12:56	NE
22	25.9	30.7	12:35	20.7	4:14	0.0	7.6	0.0	1.9	8.0	12:04	S
23	26.1	31.1	13:36	21.6	22:05	0.0	7.8	0.0	2.1	8.5	13:15	S
24	25.1	30.6	10:35	20.5	5:13	0.0	6.7	0.0	1.9	7.6	12:53	SSE
25	24.3	29.5	12:22	20.4	3:32	0.0	6.0	0.0	2.0	8.5	14:15	S
26	25.4	32.4	12:14	20.7	23:57	0.0	7.1	0.0	2.1	7.6	12:21	S
27	19.8	24.1	8:07	15.7	23:56	0.3	1.8	17.6	1.6	13.4	9:57	S
28	18.9	23.1	14:36	13.4	5:32	1.1	1.7	0.0	2.5	9.8	12:48	S
29	21.9	26.6	13:32	17.4	5:10	0.1	3.7	0.0	2.2	8.5	12:17	S
30	22.3	26.0	14:28	20.0	23:59	0.0	3.9	0.0	2.6	9.4	14:35	SSE
31	20.9	24.8	10:21	18.3	22:50	0.0	2.6	0.0	2.1	8.9	11:37	S
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	23.2	32.4	26	13.4	28	1.9	151.0	77.8	2.3	16.1	8	S

Max >= 32.0: 1

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 27.79 ON 09/07/19

Days of Rain: 6 (> .2 mm) 6 (> 2 mm) 1 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 6. Julio 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for AUG. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	23.2	29.0	11:08	18.4	0:10	0.0	4.9	0.0	3.0	9.4	5:45	NE
2	23.3	30.3	10:44	18.9	5:09	0.0	4.9	0.0	2.5	10.7	13:08	S
3	24.1	30.3	10:33	19.7	3:43	0.0	5.8	0.0	2.7	10.7	11:58	S
4	25.0	31.0	10:09	20.3	1:54	0.0	6.7	0.0	2.3	8.9	14:12	S
5	25.9	32.2	11:49	21.4	2:18	0.0	7.6	0.0	2.1	8.0	12:54	S
6	24.9	30.9	12:22	21.3	5:31	0.0	6.6	0.0	2.5	8.5	10:25	S
7	22.9	27.6	10:57	20.6	5:20	0.0	4.6	0.0	1.9	8.0	12:28	S
8	24.7	29.4	9:23	20.7	4:29	0.0	6.3	0.0	2.4	9.8	13:54	S
9	26.0	32.0	9:50	22.4	5:22	0.0	7.7	0.0	2.3	9.4	13:33	S
10	24.8	29.6	10:56	21.6	21:07	0.0	6.4	0.0	3.2	10.7	2:10	NE
11	24.1	30.1	16:00	20.3	2:40	0.0	5.8	0.0	2.3	8.9	12:51	E
12	20.8	26.7	13:31	17.2	4:45	0.1	2.6	1.6	3.0	8.9	14:25	NE
13	19.6	25.8	12:03	14.9	6:27	0.7	2.0	0.0	3.5	12.1	14:00	NE
14	20.1	25.0	9:45	16.4	6:14	0.3	2.2	0.0	2.1	9.4	12:57	S
15	21.2	27.4	12:22	18.4	2:26	0.0	2.8	0.0	2.5	9.8	13:33	S
16	21.6	27.5	15:33	18.9	0:01	0.0	3.3	0.0	2.0	7.6	14:45	SSW
17	23.5	29.8	10:41	18.9	5:05	0.0	5.2	0.0	2.6	9.4	15:10	SSW
18	23.6	30.4	11:21	19.6	4:26	0.0	5.2	0.0	2.7	9.4	13:14	S
19	22.4	27.9	10:19	19.9	22:46	0.0	4.1	0.0	3.7	9.8	6:19	SE
20	21.7	26.8	13:19	17.9	23:21	0.0	3.4	0.0	3.3	11.2	7:35	NE
21	20.7	26.1	12:27	16.7	5:35	0.2	2.6	0.0	2.2	9.4	13:24	S
22	21.9	27.6	10:28	18.4	5:06	0.0	3.6	0.0	2.3	9.8	11:35	S
23	22.7	28.2	10:42	18.7	0:42	0.0	4.4	0.0	2.0	8.5	11:18	S
24	23.3	29.5	10:55	19.0	5:06	0.0	4.9	0.0	2.0	9.8	11:17	S
25	23.4	30.4	10:05	19.3	3:04	0.0	5.1	0.0	2.1	9.4	11:58	W
26	23.1	29.7	10:45	18.6	4:17	0.0	4.7	0.0	1.9	7.6	12:04	S
27	19.9	22.1	16:15	18.5	11:29	0.0	1.6	31.2	1.7	7.2	6:47	NNE
28	21.5	27.3	12:10	17.8	5:12	0.0	3.2	0.0	2.1	7.2	14:04	S
29	23.2	29.8	11:26	19.7	1:42	0.0	4.9	0.0	2.2	8.5	13:22	N
30	24.7	29.4	11:11	21.3	0:19	0.0	6.4	0.0	2.0	7.6	12:17	S
31	24.2	30.1	10:42	20.6	23:55	0.0	5.9	0.0	2.4	8.9	13:01	NE
	23.0	32.2	5	14.9	13	1.3	145.1	32.8	2.4	12.1	13	S

Max >= 32.0: 2

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 31.19 ON 27/08/19

Days of Rain: 2 (> .2 mm) 1 (> 2 mm) 1 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 7. Agosto 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for SEP. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	22.6	28.1	12:55	16.6	23:53	0.1	4.3	20.0	2.2	17.4	23:46	S
2	19.2	23.7	9:38	16.1	0:21	0.3	1.2	3.0	2.5	10.3	13:56	SE
3	20.2	24.9	12:09	16.9	5:45	0.1	1.9	0.0	2.0	8.0	14:29	S
4	21.4	25.8	10:04	17.6	3:27	0.1	3.1	0.0	2.1	8.5	12:04	S
5	19.1	24.2	14:49	15.7	23:28	0.5	1.2	0.0	2.5	9.4	13:34	NE
6	17.6	22.0	11:04	12.8	6:14	1.6	0.8	0.0	2.8	8.5	13:12	S
7	18.4	24.3	11:54	14.5	6:05	1.0	1.1	0.0	2.5	9.4	13:35	S
8	17.7	21.6	12:31	15.8	5:29	1.2	0.4	0.0	2.7	9.8	12:32	SSE
9	18.4	21.8	12:34	15.3	5:54	0.8	0.9	0.2	2.4	9.4	14:17	NE
10	12.9	16.9	0:01	11.4	20:46	5.4	0.0	18.8	5.0	15.6	6:16	NE
11	17.6	21.6	15:12	12.6	0:01	1.6	0.8	4.0	5.6	17.0	2:13	NE
12	22.3	27.6	13:08	18.4	6:04	0.0	3.9	0.0	3.7	12.1	19:54	NE
13	21.6	24.2	15:34	18.4	23:46	0.0	3.3	0.0	4.2	14.3	8:42	ENE
14	22.6	26.4	11:53	17.9	1:29	0.0	4.2	0.0	4.5	12.5	22:12	NE
15	22.3	28.0	12:02	19.1	23:39	0.0	4.0	0.0	3.6	11.6	6:36	NE
16	22.3	25.9	9:40	19.2	0:01	0.0	4.0	0.0	1.7	6.3	5:19	NE
17	21.7	27.3	10:20	18.1	23:34	0.0	3.4	0.0	2.0	8.9	13:13	S
18	21.7	27.3	10:25	17.9	1:26	0.0	3.3	0.0	2.6	10.3	22:19	S
19												
20												
21	17.0	17.2	12:57	16.9	13:20	0.1	0.0	0.4	5.5	10.3	13:16	NE
22												
23												
24												
25	18.4	22.3	9:59	15.8	21:28	0.6	0.7	0.0	2.1	6.7	14:09	S
26	19.0	23.9	11:24	15.7	3:53	0.7	1.3	0.0	1.8	7.2	13:40	S
27	19.8	23.8	13:32	16.6	4:10	0.3	1.7	0.0	2.2	7.6	12:46	S
28	19.2	24.5	12:31	16.6	19:20	0.4	1.2	0.0	2.0	7.6	12:58	S
29	20.7	27.4	12:10	15.7	4:28	0.6	3.1	0.0	2.1	7.6	8:50	SW
30	19.9	25.4	12:05	16.5	23:51	0.3	1.9	0.0	2.5	8.9	14:03	SSW
	19.7	28.1	1	11.4	10	15.4	51.8	46.4	2.9	17.4	1	NE

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 19.99 ON 01/09/19

Days of Rain: 6 (> .2 mm) 4 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 8. Setiembre 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for OCT. 2019

NAME: CanMassuetDosrius CITY: STATE:  
ELEV: 392 m LAT: LONG:

TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)

DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	19.4	26.0	11:43	14.8	5:20	0.9	2.0	0.0	2.2	8.5	18:28	W
2	17.4	23.1	11:12	14.4	2:28	1.5	0.6	0.0	2.4	8.5	13:05	W
3	16.5	22.8	12:40	12.4	5:47	2.3	0.5	0.0	2.2	6.7	12:49	ESE
4	17.9	22.4	12:50	14.7	3:07	1.3	0.8	0.0	1.9	8.0	22:12	ESE
5	16.7	20.2	11:52	15.0	22:31	1.7	0.1	0.0	1.8	7.6	12:12	S
6	16.1	18.9	12:13	14.6	2:01	2.3	0.0	0.0	1.9	7.2	14:52	ESE
7	16.6	22.8	11:48	12.4	4:40	2.2	0.4	0.0	2.4	8.0	10:49	NE
8	18.2	23.8	15:27	14.5	4:38	1.3	1.2	0.0	2.4	9.4	10:14	WSW
9	16.4	20.3	12:11	14.0	17:50	2.2	0.2	0.0	1.8	8.9	17:59	W
10	15.5	19.0	13:26	14.1	2:39	2.8	0.0	0.0	1.7	6.7	13:31	W
11	17.6	22.2	14:26	14.9	0:39	1.3	0.6	0.0	1.8	9.4	12:46	W
12	17.7	21.2	13:15	16.3	1:16	1.0	0.3	0.0	2.0	7.2	13:03	S
13	17.2	17.7	0:49	16.8	5:59	0.3	0.0	0.0	1.4	3.6	3:15	ESE
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24	13.8	16.8	13:22	11.7	22:55	2.1	0.0	0.0	2.8	8.5	13:22	NE
25	14.2	19.5	15:20	9.6	4:01	4.2	0.1	0.0	2.0	6.3	7:55	NE
26	15.7	20.6	11:49	12.4	1:25	2.9	0.2	0.0	1.9	6.3	13:35	NE
27	15.8	20.9	12:30	13.3	6:35	2.9	0.3	0.0	1.6	6.3	15:52	W
28	14.4	16.9	14:40	12.3	5:30	3.9	0.0	0.0	2.1	7.2	9:59	WSW
29	15.4	20.4	12:22	11.7	4:12	3.0	0.1	0.0	1.3	6.7	1:45	SSW
30	17.3	21.3	12:35	14.6	23:40	1.6	0.5	0.0	1.7	6.7	12:16	N
31	15.8	18.9	14:26	13.6	23:09	2.6	0.0	0.0	1.5	5.8	15:29	NW
	16.5	26.0	1	9.6	25	44.2	7.8	0.0	1.9	9.4	8	W

Max >= 32.0: 0

Max <= 0.0: 0

Min <= 0.0: 0

Min <= -18.0: 0

Max Rain: 0.00 ON 01/10/19

Days of Rain: 0 (> .2 mm) 0 (> 2 mm) 0 (> 20 mm)

Heat Base: 18.3 Cool Base: 18.3 Method: Integration

Registro de viento 9. Octubre 2019 (Fuente: Can Massuet)

MONTHLY CLIMATOLOGICAL SUMMARY for NOV. 2019												
NAME: CanMassuetDosrius CITY: STATE:												
ELEV: 392 m LAT: LONG:												
TEMPERATURE (°C), RAIN (mm), WIND SPEED (m/s)												
DAY	MEAN TEMP	HIGH	TIME	LOW	TIME	HEAT DEG DAYS	COOL DEG DAYS	RAIN	AVG WIND SPEED	HIGH	TIME	DOM DIR
1	14.5	17.2	13:28	12.2	3:09	3.8	0.0	0.0	1.4	5.8	4:40	SSW
2	14.4	14.9	0:59	13.9	1:41	0.6	0.0	0.0	2.6	7.2	1:12	NE
3												
4												
5												
6												
7	10.1	14.8	13:46	6.6	21:10	7.1	0.0	0.0	2.8	11.2	6:09	W
8	7.1	10.4	13:44	4.5	6:39	11.2	0.0	0.0	4.1	12.5	16:40	WNW
9	8.1	13.1	12:33	3.7	2:08	10.2	0.0	0.0	2.6	10.3	19:19	NW
10	7.1	11.1	13:47	4.5	23:51	11.2	0.0	5.8	2.2	8.9	3:08	NE
11	7.3	14.3	13:07	3.3	2:43	9.7	0.0	0.0	2.2	7.2	8:39	NW
12	8.9	13.2	12:50	4.2	6:12	9.1	0.0	0.0	1.8	6.3	1:35	S
13	8.3	11.4	13:16	6.7	2:23	10.0	0.0	0.0	2.2	8.5	6:10	NE
14	6.7	10.1	10:06	3.4	18:45	11.7	0.0	2.2	2.2	10.7	10:38	W
15	5.3	8.6	11:43	3.2	23:58	13.0	0.0	0.0	3.0	11.6	17:02	NE
16	5.7	10.8	13:10	2.8	21:56	12.7	0.0	0.0	2.5	11.6	18:22	NW
17	6.2	10.1	13:05	3.1	2:13	12.1	0.0	0.0	2.2	8.9	9:13	NW
18	6.6	8.6	10:05	5.3	1:55	5.6	0.0	0.0	3.9	11.2	11:25	NE
19												
20												
21												
22												
23												
24												
25												
26												
27												
28												
29												
30												
	8.3	17.2	1	2.8	16	128.1	0.0	8.0	2.6	12.5	8	NW
Max >= 32.0: 0												
Max <= 0.0: 0												
Min <= 0.0: 0												
Min <= -18.0: 0												
Max Rain: 5.79 ON 10/11/19												
Days of Rain: 2 (> .2 mm) 2 (> 2 mm) 0 (> 20 mm)												
Heat Base: 18.3 Cool Base: 18.3 Method: Integration												

Registro de viento 10. Noviembre 2019 (Fuente: Can Massuet)



## Anexo D. Análisis Cype

En el último anexo del proyecto se presenta toda la información relevante a la estructura de los perfiles pertenecientes a la antena, incluyendo la respuesta frente al ataque de viento.

La fuente de información de los datos a continuación es el programa *Cype*, el cual presenta el estilo siguiente:

- 1. JOB DATA
  - 1.1. Codes considered
  - 1.2. Limit states
    - 1.2.1. Projects situation
- 2. STUCTIONE
  - 2.1. Geometry
    - 2.1.1. Nodes
    - 2.1.2. Bars
  - 2.2. Loads
    - 2.2.1. Nodes
    - 2.2.2. Bars
  - 2.3. Results
    - 2.3.1. Nodes
    - 2.3.2. Bars

## Reports



estructura de la antena objeto de estudio

## JOB DATA

### 1.1.- Codes considered

Rolled and welded steel: Eurocodes 3 and 4

### 1.2.- Limit states

Fracture U.L.S. Rolled steel	EC Snow: Remaining CEN Member States, $H \leq 1000$ m
Displacements	Characteristic loads

#### 1.2.1.- Project situations

The load combinations will be defined according to the following criteria for the different project situations:

- **With combination coefficients**

- **Without combination coefficients**

- Where:

$G_k$	Permanent load
$P_k$	Prestressing action
$Q_k$	Variable load
$\gamma_G$	Permanent load partial safety factor
$\gamma_P$	Partial safety coefficient for prestressing action
$\gamma_{Q,1}$	Main variable load partial safety factor
$\gamma_{Q,i}$	Accompanying variable load partial safety factor
$\psi_{p,1}$	Main variable load combination coefficient
$\psi_{a,i}$	Accompanying variable load combination coefficient

For each project situation and limit state, the loading coefficients will be determined by:

#### Fracture U.L.S. Rolled steel: Eurocodes 3 and 4

Persistent or transient				
	Partial safety factors ( $\gamma$ )		Combination coefficients ( $\psi$ )	
	Favourable	Unfavourable	Main ( $\psi_p$ )	Accompanying ( $\psi_a$ )
Dead load (G)	1.000	1.350	-	-
Wind (Q)	0.000	1.500	1.000	0.600

Variable loads without seismic loading		
	Partial safety factors ( $\gamma$ )	
	Favourable	Unfavourable
Dead load (G)	1.000	1.000
Wind (Q)	0.000	1.000

## 2.- STRUCTURE

### 2.1.- Geometry

#### 2.1.1.- Nodes

References:

$\Delta_x, \Delta_y, \Delta_z$ : Prescribed displacements in global axes.

$\theta_x, \theta_y, \theta_z$ : Prescribed rotations in global axes.

Each degree of freedom is marked with 'X' if it has external restrictions and, in the opposite case, with '-'.

Nodes										
Reference	Coordinates			External fixity						Internal fixity
	X (m)	Y (m)	Z (m)	$\Delta_x$	$\Delta_y$	$\Delta_z$	$\theta_x$	$\theta_y$	$\theta_z$	
N1	0.275	-0.275	11.590	-	-	-	-	-	-	Fixed
N2	0.275	0.275	11.590	-	-	-	-	-	-	Fixed
N3	-0.275	-0.275	11.590	-	-	-	-	-	-	Fixed
N4	-0.275	0.275	11.590	-	-	-	-	-	-	Fixed
N5	0.275	-0.275	16.115	-	-	-	-	-	-	Fixed
N6	0.275	0.275	16.115	-	-	-	-	-	-	Fixed
N7	-0.275	-0.275	16.115	-	-	-	-	-	-	Fixed
N8	-0.275	0.275	16.115	-	-	-	-	-	-	Fixed
N9	0.275	-0.275	12.090	-	-	-	-	-	-	Fixed
N10	0.275	0.275	12.090	-	-	-	-	-	-	Fixed
N11	-0.275	-0.275	12.090	-	-	-	-	-	-	Fixed
N12	-0.275	0.275	12.090	-	-	-	-	-	-	Fixed
N13	0.275	-0.275	12.665	-	-	-	-	-	-	Fixed
N14	0.275	0.275	12.665	-	-	-	-	-	-	Fixed
N15	-0.275	-0.275	12.665	-	-	-	-	-	-	Fixed
N16	-0.275	0.275	12.665	-	-	-	-	-	-	Fixed
N17	0.275	-0.275	13.240	-	-	-	-	-	-	Fixed
N18	0.275	0.275	13.240	-	-	-	-	-	-	Fixed
N19	-0.275	-0.275	13.240	-	-	-	-	-	-	Fixed
N20	-0.275	0.275	13.240	-	-	-	-	-	-	Fixed
N21	0.275	-0.275	13.815	-	-	-	-	-	-	Fixed
N22	0.275	0.275	13.815	-	-	-	-	-	-	Fixed
N23	-0.275	-0.275	13.815	-	-	-	-	-	-	Fixed
N24	-0.275	0.275	13.815	-	-	-	-	-	-	Fixed
N25	0.275	-0.275	14.390	-	-	-	-	-	-	Fixed
N26	0.275	0.275	14.390	-	-	-	-	-	-	Fixed

Nodes										
Reference	Coordinates			External fixity						Internal fixity
	X (m)	Y (m)	Z (m)	$\Delta_x$	$\Delta_y$	$\Delta_z$	$\theta_x$	$\theta_y$	$\theta_z$	
N27	-0.275	-0.275	14.390	-	-	-	-	-	-	Fixed
N28	-0.275	0.275	14.390	-	-	-	-	-	-	Fixed
N29	0.275	-0.275	14.965	-	-	-	-	-	-	Fixed
N30	0.275	0.275	14.965	-	-	-	-	-	-	Fixed
N31	-0.275	-0.275	14.965	-	-	-	-	-	-	Fixed
N32	-0.275	0.275	14.965	-	-	-	-	-	-	Fixed
N33	0.275	-0.275	15.540	-	-	-	-	-	-	Fixed
N34	0.275	0.275	15.540	-	-	-	-	-	-	Fixed
N35	-0.275	-0.275	15.540	-	-	-	-	-	-	Fixed
N36	-0.275	0.275	15.540	-	-	-	-	-	-	Fixed
N37	-0.522	0.522	0.000	X	X	X	-	-	-	Fixed
N38	0.522	0.522	0.000	X	X	X	-	-	-	Fixed
N39	-0.522	-0.522	0.000	X	X	X	-	-	-	Fixed
N40	0.522	-0.522	0.000	X	X	X	-	-	-	Fixed
N41	0.510	-0.510	0.580	-	-	-	-	-	-	Fixed
N42	0.498	-0.498	1.159	-	-	-	-	-	-	Fixed
N43	0.485	-0.485	1.739	-	-	-	-	-	-	Fixed
N44	0.473	-0.473	2.319	-	-	-	-	-	-	Fixed
N45	0.461	-0.461	2.899	-	-	-	-	-	-	Fixed
N46	0.448	-0.448	3.478	-	-	-	-	-	-	Fixed
N47	0.436	-0.436	4.058	-	-	-	-	-	-	Fixed
N48	0.423	-0.423	4.638	-	-	-	-	-	-	Fixed
N49	0.411	-0.411	5.218	-	-	-	-	-	-	Fixed
N50	0.399	-0.399	5.797	-	-	-	-	-	-	Fixed
N51	0.386	-0.386	6.377	-	-	-	-	-	-	Fixed
N52	0.374	-0.374	6.957	-	-	-	-	-	-	Fixed
N53	0.362	-0.362	7.537	-	-	-	-	-	-	Fixed
N54	0.349	-0.349	8.116	-	-	-	-	-	-	Fixed
N55	0.337	-0.337	8.696	-	-	-	-	-	-	Fixed
N56	0.324	-0.324	9.276	-	-	-	-	-	-	Fixed
N57	0.312	-0.312	9.856	-	-	-	-	-	-	Fixed
N58	0.300	-0.300	10.435	-	-	-	-	-	-	Fixed
N59	0.287	-0.287	11.015	-	-	-	-	-	-	Fixed
N60	0.510	0.510	0.580	-	-	-	-	-	-	Fixed
N61	0.498	0.498	1.159	-	-	-	-	-	-	Fixed
N62	0.485	0.485	1.739	-	-	-	-	-	-	Fixed
N63	0.473	0.473	2.319	-	-	-	-	-	-	Fixed
N64	0.461	0.461	2.899	-	-	-	-	-	-	Fixed
N65	0.448	0.448	3.478	-	-	-	-	-	-	Fixed
N66	0.436	0.436	4.058	-	-	-	-	-	-	Fixed
N67	0.423	0.423	4.638	-	-	-	-	-	-	Fixed
N68	0.411	0.411	5.218	-	-	-	-	-	-	Fixed
N69	0.399	0.399	5.797	-	-	-	-	-	-	Fixed
N70	0.386	0.386	6.377	-	-	-	-	-	-	Fixed
N71	0.374	0.374	6.957	-	-	-	-	-	-	Fixed
N72	0.362	0.362	7.537	-	-	-	-	-	-	Fixed

Nodes										
Reference	Coordinates			External fixity						Internal fixity
	X (m)	Y (m)	Z (m)	$\Delta_x$	$\Delta_y$	$\Delta_z$	$\theta_x$	$\theta_y$	$\theta_z$	
N73	0.349	0.349	8.116	-	-	-	-	-	-	Fixed
N74	0.337	0.337	8.696	-	-	-	-	-	-	Fixed
N75	0.324	0.324	9.276	-	-	-	-	-	-	Fixed
N76	0.312	0.312	9.856	-	-	-	-	-	-	Fixed
N77	0.300	0.300	10.435	-	-	-	-	-	-	Fixed
N78	0.287	0.287	11.015	-	-	-	-	-	-	Fixed
N79	-0.510	0.510	0.580	-	-	-	-	-	-	Fixed
N80	-0.498	0.498	1.159	-	-	-	-	-	-	Fixed
N81	-0.485	0.485	1.739	-	-	-	-	-	-	Fixed
N82	-0.473	0.473	2.319	-	-	-	-	-	-	Fixed
N83	-0.461	0.461	2.899	-	-	-	-	-	-	Fixed
N84	-0.448	0.448	3.478	-	-	-	-	-	-	Fixed
N85	-0.436	0.436	4.058	-	-	-	-	-	-	Fixed
N86	-0.423	0.423	4.638	-	-	-	-	-	-	Fixed
N87	-0.411	0.411	5.218	-	-	-	-	-	-	Fixed
N88	-0.399	0.399	5.797	-	-	-	-	-	-	Fixed
N89	-0.386	0.386	6.377	-	-	-	-	-	-	Fixed
N90	-0.374	0.374	6.957	-	-	-	-	-	-	Fixed
N91	-0.362	0.362	7.537	-	-	-	-	-	-	Fixed
N92	-0.349	0.349	8.116	-	-	-	-	-	-	Fixed
N93	-0.337	0.337	8.696	-	-	-	-	-	-	Fixed
N94	-0.324	0.324	9.276	-	-	-	-	-	-	Fixed
N95	-0.312	0.312	9.856	-	-	-	-	-	-	Fixed
N96	-0.300	0.300	10.435	-	-	-	-	-	-	Fixed
N97	-0.287	0.287	11.015	-	-	-	-	-	-	Fixed
N98	-0.510	-0.510	0.580	-	-	-	-	-	-	Fixed
N99	-0.498	-0.498	1.159	-	-	-	-	-	-	Fixed
N100	-0.485	-0.485	1.739	-	-	-	-	-	-	Fixed
N101	-0.473	-0.473	2.319	-	-	-	-	-	-	Fixed
N102	-0.461	-0.461	2.899	-	-	-	-	-	-	Fixed
N103	-0.448	-0.448	3.478	-	-	-	-	-	-	Fixed
N104	-0.436	-0.436	4.058	-	-	-	-	-	-	Fixed
N105	-0.423	-0.423	4.638	-	-	-	-	-	-	Fixed
N106	-0.411	-0.411	5.218	-	-	-	-	-	-	Fixed
N107	-0.399	-0.399	5.797	-	-	-	-	-	-	Fixed
N108	-0.386	-0.386	6.377	-	-	-	-	-	-	Fixed
N109	-0.374	-0.374	6.957	-	-	-	-	-	-	Fixed
N110	-0.362	-0.362	7.537	-	-	-	-	-	-	Fixed
N111	-0.349	-0.349	8.116	-	-	-	-	-	-	Fixed
N112	-0.337	-0.337	8.696	-	-	-	-	-	-	Fixed
N113	-0.324	-0.324	9.276	-	-	-	-	-	-	Fixed
N114	-0.312	-0.312	9.856	-	-	-	-	-	-	Fixed
N115	-0.300	-0.300	10.435	-	-	-	-	-	-	Fixed
N116	-0.287	-0.287	11.015	-	-	-	-	-	-	Fixed
N117	0.000	0.000	16.115	-	-	-	-	-	-	Fixed

**2.1.2.- Bars**

Materials used							
Material		E (MPa)	$\nu$	G (MPa)	$f_y$ (MPa)	$\alpha_t$ (m/m°C)	$\gamma$ (kN/m³)
Type	Designation						
Rolled steel	S275 (EN 1993-1-1)	210000.00	0.300	81000.00	275.00	0.000012	77.01
Notation: <i>E</i> : Modulus of Elasticity <i><math>\nu</math></i> : Poisson's ratio <i>G</i> : Shear Modulus <i><math>f_y</math></i> : Yield Strength <i><math>\alpha_t</math></i> : Coefficient of thermal expansion <i><math>\gamma</math></i> : Unit weight							

**2.1.2.2.- Description**

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
Rolled steel	S275 (EN 1993-1-1)	N1/N2	N1/N2	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N3/N1	N3/N1	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N3/N4	N3/N4	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N4/N2	N4/N2	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N5/N6	N5/N6	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N7/N5	N7/N5	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N7/N8	N7/N8	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N8/N6	N8/N6	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N2/N10	N2/N6	L 70 x 70 x 6 (L)	0.500	1.00	1.00	-	-
		N10/N14	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N14/N18	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N18/N22	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N22/N26	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N26/N30	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N30/N34	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N34/N6	N2/N6	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N1/N9	N1/N5	L 70 x 70 x 6 (L)	0.500	1.00	1.00	-	-
		N9/N13	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N13/N17	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N17/N21	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N21/N25	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N25/N29	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N29/N33	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N33/N5	N1/N5	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N4/N12	N4/N8	L 70 x 70 x 6 (L)	0.500	1.00	1.00	-	-
		N12/N16	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N16/N20	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N20/N24	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N24/N28	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N28/N32	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N32/N36	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N36/N8	N4/N8	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N3/N11	N3/N7	L 70 x 70 x 6 (L)	0.500	1.00	1.00	-	-
		N11/N15	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N15/N19	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N19/N23	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N23/N27	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N27/N31	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N31/N35	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N35/N7	N3/N7	L 70 x 70 x 6 (L)	0.575	1.00	1.00	-	-
		N9/N10	N9/N10	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N11/N9	N11/N9	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N11/N12	N11/N12	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N12/N10	N12/N10	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N13/N14	N13/N14	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N15/N13	N15/N13	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N15/N16	N15/N16	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N16/N14	N16/N14	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N17/N18	N17/N18	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N19/N17	N19/N17	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N19/N20	N19/N20	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N20/N18	N20/N18	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N21/N22	N21/N22	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N23/N21	N23/N21	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N23/N24	N23/N24	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N24/N22	N24/N22	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N25/N26	N25/N26	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N27/N25	N27/N25	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N27/N28	N27/N28	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N28/N26	N28/N26	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N29/N30	N29/N30	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N31/N29	N31/N29	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N31/N32	N31/N32	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N32/N30	N32/N30	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N33/N34	N33/N34	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N35/N33	N35/N33	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N35/N36	N35/N36	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-
		N36/N34	N36/N34	L 45 x 45 x 4 (L)	0.550	1.00	1.00	-	-



Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N4/N10	N4/N10	L 45 x 45 x 4 (L)	0.743	1.00	1.00	-	-
		N10/N16	N10/N16	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N16/N18	N16/N18	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N18/N24	N18/N24	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N24/N26	N24/N26	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N26/N32	N26/N32	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N32/N34	N32/N34	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N34/N8	N34/N8	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N2/N9	N2/N9	L 45 x 45 x 4 (L)	0.743	1.00	1.00	-	-
		N9/N14	N9/N14	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N14/N17	N14/N17	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N17/N22	N17/N22	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N22/N25	N22/N25	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N25/N30	N25/N30	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N30/N33	N30/N33	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N33/N6	N33/N6	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N3/N12	N3/N12	L 45 x 45 x 4 (L)	0.743	1.00	1.00	-	-
		N12/N15	N12/N15	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N15/N20	N15/N20	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N20/N23	N20/N23	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N23/N28	N23/N28	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N28/N31	N28/N31	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N31/N36	N31/N36	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N36/N7	N36/N7	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N1/N11	N1/N11	L 45 x 45 x 4 (L)	0.743	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N11/N13	N11/N13	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N13/N19	N13/N19	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N19/N21	N19/N21	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N21/N27	N21/N27	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N27/N29	N27/N29	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N29/N35	N29/N35	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N35/N5	N35/N5	L 45 x 45 x 4 (L)	0.796	1.00	1.00	-	-
		N39/N79	N39/N79	L 45 x 45 x 4 (L)	1.184	1.00	1.00	-	-
		N79/N99	N79/N99	L 45 x 45 x 4 (L)	1.163	1.00	1.00	-	-
		N99/N81	N99/N81	L 45 x 45 x 4 (L)	1.141	1.00	1.00	-	-
		N81/N101	N81/N101	L 45 x 45 x 4 (L)	1.120	1.00	1.00	-	-
		N101/N83	N101/N83	L 45 x 45 x 4 (L)	1.099	1.00	1.00	-	-
		N83/N103	N83/N103	L 45 x 45 x 4 (L)	1.078	1.00	1.00	-	-
		N103/N85	N103/N85	L 45 x 45 x 4 (L)	1.057	1.00	1.00	-	-
		N85/N105	N85/N105	L 45 x 45 x 4 (L)	1.037	1.00	1.00	-	-
		N105/N87	N105/N87	L 45 x 45 x 4 (L)	1.016	1.00	1.00	-	-
		N87/N107	N87/N107	L 45 x 45 x 4 (L)	0.996	1.00	1.00	-	-
		N107/N89	N107/N89	L 45 x 45 x 4 (L)	0.976	1.00	1.00	-	-
		N89/N109	N89/N109	L 45 x 45 x 4 (L)	0.956	1.00	1.00	-	-
		N109/N91	N109/N91	L 45 x 45 x 4 (L)	0.937	1.00	1.00	-	-
		N91/N111	N91/N111	L 45 x 45 x 4 (L)	0.917	1.00	1.00	-	-
		N111/N93	N111/N93	L 45 x 45 x 4 (L)	0.898	1.00	1.00	-	-
		N93/N113	N93/N113	L 45 x 45 x 4 (L)	0.879	1.00	1.00	-	-
		N113/N95	N113/N95	L 45 x 45 x 4 (L)	0.861	1.00	1.00	-	-
		N95/N115	N95/N115	L 45 x 45 x 4 (L)	0.843	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N115/N97	N115/N97	L 45 x 45 x 4 (L)	0.825	1.00	1.00	-	-
		N97/N3	N97/N3	L 45 x 45 x 4 (L)	0.804	1.00	1.00	-	-
		N37/N60	N37/N60	L 45 x 45 x 4 (L)	1.184	1.00	1.00	-	-
		N60/N80	N60/N80	L 45 x 45 x 4 (L)	1.163	1.00	1.00	-	-
		N80/N62	N80/N62	L 45 x 45 x 4 (L)	1.141	1.00	1.00	-	-
		N62/N82	N62/N82	L 45 x 45 x 4 (L)	1.120	1.00	1.00	-	-
		N82/N64	N82/N64	L 45 x 45 x 4 (L)	1.099	1.00	1.00	-	-
		N64/N84	N64/N84	L 45 x 45 x 4 (L)	1.078	1.00	1.00	-	-
		N84/N66	N84/N66	L 45 x 45 x 4 (L)	1.057	1.00	1.00	-	-
		N66/N86	N66/N86	L 45 x 45 x 4 (L)	1.037	1.00	1.00	-	-
		N86/N68	N86/N68	L 45 x 45 x 4 (L)	1.016	1.00	1.00	-	-
		N68/N88	N68/N88	L 45 x 45 x 4 (L)	0.996	1.00	1.00	-	-
		N88/N70	N88/N70	L 45 x 45 x 4 (L)	0.976	1.00	1.00	-	-
		N70/N90	N70/N90	L 45 x 45 x 4 (L)	0.956	1.00	1.00	-	-
		N90/N72	N90/N72	L 45 x 45 x 4 (L)	0.937	1.00	1.00	-	-
		N72/N92	N72/N92	L 45 x 45 x 4 (L)	0.917	1.00	1.00	-	-
		N92/N74	N92/N74	L 45 x 45 x 4 (L)	0.898	1.00	1.00	-	-
		N74/N94	N74/N94	L 45 x 45 x 4 (L)	0.879	1.00	1.00	-	-
		N94/N76	N94/N76	L 45 x 45 x 4 (L)	0.861	1.00	1.00	-	-
		N76/N96	N76/N96	L 45 x 45 x 4 (L)	0.843	1.00	1.00	-	-
		N96/N78	N96/N78	L 45 x 45 x 4 (L)	0.825	1.00	1.00	-	-
		N78/N4	N78/N4	L 45 x 45 x 4 (L)	0.804	1.00	1.00	-	-
		N38/N41	N38/N41	L 45 x 45 x 4 (L)	1.184	1.00	1.00	-	-
		N41/N61	N41/N61	L 45 x 45 x 4 (L)	1.163	1.00	1.00	-	-
		N61/N43	N61/N43	L 45 x 45 x 4 (L)	1.141	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N43/N63	N43/N63	L 45 x 45 x 4 (L)	1.120	1.00	1.00	-	-
		N63/N45	N63/N45	L 45 x 45 x 4 (L)	1.099	1.00	1.00	-	-
		N45/N65	N45/N65	L 45 x 45 x 4 (L)	1.078	1.00	1.00	-	-
		N65/N47	N65/N47	L 45 x 45 x 4 (L)	1.057	1.00	1.00	-	-
		N47/N67	N47/N67	L 45 x 45 x 4 (L)	1.037	1.00	1.00	-	-
		N67/N49	N67/N49	L 45 x 45 x 4 (L)	1.016	1.00	1.00	-	-
		N49/N69	N49/N69	L 45 x 45 x 4 (L)	0.996	1.00	1.00	-	-
		N69/N51	N69/N51	L 45 x 45 x 4 (L)	0.976	1.00	1.00	-	-
		N51/N71	N51/N71	L 45 x 45 x 4 (L)	0.956	1.00	1.00	-	-
		N71/N53	N71/N53	L 45 x 45 x 4 (L)	0.937	1.00	1.00	-	-
		N53/N73	N53/N73	L 45 x 45 x 4 (L)	0.917	1.00	1.00	-	-
		N73/N55	N73/N55	L 45 x 45 x 4 (L)	0.898	1.00	1.00	-	-
		N55/N75	N55/N75	L 45 x 45 x 4 (L)	0.879	1.00	1.00	-	-
		N75/N57	N75/N57	L 45 x 45 x 4 (L)	0.861	1.00	1.00	-	-
		N57/N77	N57/N77	L 45 x 45 x 4 (L)	0.843	1.00	1.00	-	-
		N77/N59	N77/N59	L 45 x 45 x 4 (L)	0.825	1.00	1.00	-	-
		N59/N2	N59/N2	L 45 x 45 x 4 (L)	0.804	1.00	1.00	-	-
		N40/N98	N40/N98	L 45 x 45 x 4 (L)	1.184	1.00	1.00	-	-
		N98/N42	N98/N42	L 45 x 45 x 4 (L)	1.163	1.00	1.00	-	-
		N42/N100	N42/N100	L 45 x 45 x 4 (L)	1.141	1.00	1.00	-	-
		N100/N44	N100/N44	L 45 x 45 x 4 (L)	1.120	1.00	1.00	-	-
		N44/N102	N44/N102	L 45 x 45 x 4 (L)	1.099	1.00	1.00	-	-
		N102/N46	N102/N46	L 45 x 45 x 4 (L)	1.078	1.00	1.00	-	-
		N46/N104	N46/N104	L 45 x 45 x 4 (L)	1.057	1.00	1.00	-	-
		N104/N48	N104/N48	L 45 x 45 x 4 (L)	1.037	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N48/N106	N48/N106	L 45 x 45 x 4 (L)	1.016	1.00	1.00	-	-
		N106/N50	N106/N50	L 45 x 45 x 4 (L)	0.996	1.00	1.00	-	-
		N50/N108	N50/N108	L 45 x 45 x 4 (L)	0.976	1.00	1.00	-	-
		N108/N52	N108/N52	L 45 x 45 x 4 (L)	0.956	1.00	1.00	-	-
		N52/N110	N52/N110	L 45 x 45 x 4 (L)	0.937	1.00	1.00	-	-
		N110/N54	N110/N54	L 45 x 45 x 4 (L)	0.917	1.00	1.00	-	-
		N54/N112	N54/N112	L 45 x 45 x 4 (L)	0.898	1.00	1.00	-	-
		N112/N56	N112/N56	L 45 x 45 x 4 (L)	0.879	1.00	1.00	-	-
		N56/N114	N56/N114	L 45 x 45 x 4 (L)	0.861	1.00	1.00	-	-
		N114/N58	N114/N58	L 45 x 45 x 4 (L)	0.843	1.00	1.00	-	-
		N58/N116	N58/N116	L 45 x 45 x 4 (L)	0.825	1.00	1.00	-	-
		N116/N1	N116/N1	L 45 x 45 x 4 (L)	0.804	1.00	1.00	-	-
		N40/N41	N40/N41	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N42/N43	N42/N43	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N43/N44	N43/N44	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N44/N45	N44/N45	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N45/N46	N45/N46	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N46/N47	N46/N47	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N47/N48	N47/N48	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N48/N49	N48/N49	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N49/N50	N49/N50	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N50/N51	N50/N51	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N51/N52	N51/N52	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N52/N53	N52/N53	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N53/N54	N53/N54	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N54/N55	N54/N55	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N55/N56	N55/N56	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N56/N57	N56/N57	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N57/N58	N57/N58	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N58/N59	N58/N59	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N59/N1	N59/N1	L 80 x 80 x 8 (L)	0.575	1.00	1.00	-	-
		N38/N60	N38/N60	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N61/N62	N61/N62	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N62/N63	N62/N63	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N63/N64	N63/N64	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N64/N65	N64/N65	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N65/N66	N65/N66	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N66/N67	N66/N67	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N67/N68	N67/N68	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N68/N69	N68/N69	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N69/N70	N69/N70	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N70/N71	N70/N71	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N71/N72	N71/N72	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N72/N73	N72/N73	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N73/N74	N73/N74	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N74/N75	N74/N75	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N75/N76	N75/N76	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N76/N77	N76/N77	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N77/N78	N77/N78	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N78/N2	N78/N2	L 80 x 80 x 8 (L)	0.575	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N37/N79	N37/N79	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N80/N81	N80/N81	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N81/N82	N81/N82	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N82/N83	N82/N83	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N83/N84	N83/N84	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N84/N85	N84/N85	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N85/N86	N85/N86	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N86/N87	N86/N87	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N87/N88	N87/N88	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N88/N89	N88/N89	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N89/N90	N89/N90	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N90/N91	N90/N91	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N91/N92	N91/N92	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N92/N93	N92/N93	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N93/N94	N93/N94	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N94/N95	N94/N95	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N95/N96	N95/N96	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N96/N97	N96/N97	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N97/N4	N97/N4	L 80 x 80 x 8 (L)	0.575	1.00	1.00	-	-
		N39/N98	N39/N98	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N99/N100	N99/N100	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N100/N101	N100/N101	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N101/N102	N101/N102	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N102/N103	N102/N103	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N103/N104	N103/N104	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-

Description									
Material		Bar (Ni/Nf)	Element (Ni/Nf)	Section(Series)	Length (m)	$\beta_{xy}$	$\beta_{xz}$	Lb <sub>Top</sub> (m)	Lb <sub>Bot.</sub> (m)
Type	Designation								
		N104/N105	N104/N105	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N105/N106	N105/N106	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N106/N107	N106/N107	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N107/N108	N107/N108	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N108/N109	N108/N109	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N109/N110	N109/N110	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N110/N111	N110/N111	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N111/N112	N111/N112	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N112/N113	N112/N113	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N113/N114	N113/N114	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N114/N115	N114/N115	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N115/N116	N115/N116	L 80 x 80 x 8 (L)	0.580	1.00	1.00	-	-
		N116/N3	N116/N3	L 80 x 80 x 8 (L)	0.575	1.00	1.00	-	-
		N98/N99	N98/N99	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N79/N80	N79/N80	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N60/N61	N60/N61	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N41/N42	N41/N42	2xL 90 x 90 x 9(T) (L)	0.580	1.00	1.00	-	-
		N5/N117	N5/N8	L 45 x 45 x 4 (L)	0.389	1.00	1.00	-	-
		N117/N8	N5/N8	L 45 x 45 x 4 (L)	0.389	1.00	1.00	-	-
		N7/N117	N7/N6	L 45 x 45 x 4 (L)	0.389	1.00	1.00	-	-
		N117/N6	N7/N6	L 45 x 45 x 4 (L)	0.389	1.00	1.00	-	-
<p>Notation:  Ni: Initial node  Nf: Final node  <math>\beta_{xy}</math>: Buckling coefficient in the 'XY' plane  <math>\beta_{xz}</math>: Buckling coefficient in the 'XZ' plane  Lb<sub>Top</sub>: Separation between bracings of the top flange  Lb<sub>Bot.</sub>: Separation between bracings of the bottom flange</p>									



Element types	
Ref.	Elements
1	N1/N2, N3/N1, N3/N4, N4/N2, N5/N6, N7/N5, N7/N8, N8/N6, N9/N10, N11/N9, N11/N12, N12/N10, N13/N14, N15/N13, N15/N16, N16/N14, N17/N18, N19/N17, N19/N20, N20/N18, N21/N22, N23/N21, N23/N24, N24/N22, N25/N26, N27/N25, N27/N28, N28/N26, N29/N30, N31/N29, N31/N32, N32/N30, N33/N34, N35/N33, N35/N36, N36/N34, N4/N10, N10/N16, N16/N18, N18/N24, N24/N26, N26/N32, N32/N34, N34/N8, N2/N9, N9/N14, N14/N17, N17/N22, N22/N25, N25/N30, N30/N33, N33/N6, N3/N12, N12/N15, N15/N20, N20/N23, N23/N28, N28/N31, N31/N36, N36/N7, N1/N11, N11/N13, N13/N19, N19/N21, N21/N27, N27/N29, N29/N35, N35/N5, N39/N79, N79/N99, N99/N81, N81/N101, N101/N83, N83/N103, N103/N85, N85/N105, N105/N87, N87/N107, N107/N89, N89/N109, N109/N91, N91/N111, N111/N93, N93/N113, N113/N95, N95/N115, N115/N97, N97/N3, N37/N60, N60/N80, N80/N62, N62/N82, N82/N64, N64/N84, N84/N66, N66/N86, N86/N68, N68/N88, N88/N70, N70/N90, N90/N72, N72/N92, N92/N74, N74/N94, N94/N76, N76/N96, N96/N78, N78/N4, N38/N41, N41/N61, N61/N43, N43/N63, N63/N45, N45/N65, N65/N47, N47/N67, N67/N49, N49/N69, N69/N51, N51/N71, N71/N53, N53/N73, N73/N55, N55/N75, N75/N57, N57/N77, N77/N59, N59/N2, N40/N98, N98/N42, N42/N100, N100/N44, N44/N102, N102/N46, N46/N104, N104/N48, N48/N106, N106/N50, N50/N108, N108/N52, N52/N110, N110/N54, N54/N112, N112/N56, N56/N114, N114/N58, N58/N116, N116/N1, N5/N8 and N7/N6
2	N2/N6, N1/N5, N4/N8 and N3/N7
3	N40/N41, N42/N43, N43/N44, N44/N45, N45/N46, N46/N47, N47/N48, N48/N49, N49/N50, N50/N51, N51/N52, N52/N53, N53/N54, N54/N55, N38/N60, N61/N62, N62/N63, N63/N64, N64/N65, N65/N66, N66/N67, N67/N68, N68/N69, N69/N70, N70/N71, N71/N72, N72/N73, N73/N74, N37/N79, N80/N81, N81/N82, N82/N83, N83/N84, N84/N85, N85/N86, N86/N87, N87/N88, N88/N89, N89/N90, N90/N91, N91/N92, N92/N93, N39/N98, N99/N100, N100/N101, N101/N102, N102/N103, N103/N104, N104/N105, N105/N106, N106/N107, N107/N108, N108/N109, N109/N110, N110/N111, N111/N112, N98/N99, N79/N80, N60/N61 and N41/N42
4	N55/N56, N56/N57, N57/N58, N58/N59, N59/N1, N74/N75, N75/N76, N76/N77, N77/N78, N78/N2, N93/N94, N94/N95, N95/N96, N96/N97, N97/N4, N112/N113, N113/N114, N114/N115, N115/N116 and N116/N3

Mechanical characteristics									
Material		Ref .	Description	A (cm <sup>2</sup> )	A <sub>vy</sub> (cm <sup>2</sup> )	A <sub>vz</sub> (cm <sup>2</sup> )	I <sub>yy</sub> (cm <sup>4</sup> )	I <sub>zz</sub> (cm <sup>4</sup> )	I <sub>t</sub> (cm <sup>4</sup> )
Type	Designation								
Rolled steel	S275 (EN 1993-1-1)	1	L 45 x 45 x 4, (L)	3.49	1.64	1.64	6.43	6.43	0.18
		2	L 70 x 70 x 6, (L)	8.13	3.84	3.84	36.88	36.88	0.96
		3	L 90 x 90 x 9, Double welded in T, (L) Continuous	31.00	14.58	14.58	231.60	431.60	20.12
		4	L 80 x 80 x 8, (L)	12.30	5.76	5.76	72.25	72.25	2.59
<p>Notation: Ref.: Reference A: Area of the transverse section A<sub>vy</sub>: Shear area of the section in the local 'Y' axis A<sub>vz</sub>: Shear area of the section in the local 'Z' axis I<sub>yy</sub>: Inertia of the section about the local 'Y' axis I<sub>zz</sub>: Inertia of the section about the local 'Z' axis I<sub>t</sub>: Torsional inertia</p> <p>The mechanical characteristics of the elements correspond to those of their cross section at their mid-point.</p>									

**2.1.2.4.- Takeoff table**

<b>Takeoff table</b>						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
Rolled steel	S275 (EN 1993-1-1)	N1/N2	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N3/N1	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N3/N4	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N4/N2	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N5/N6	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N7/N5	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N7/N8	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N8/N6	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N2/N6	L 70 x 70 x 6 (L)	4.525	0.004	28.88
		N1/N5	L 70 x 70 x 6 (L)	4.525	0.004	28.88
		N4/N8	L 70 x 70 x 6 (L)	4.525	0.004	28.88
		N3/N7	L 70 x 70 x 6 (L)	4.525	0.004	28.88
		N9/N10	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N11/N9	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N11/N12	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N12/N10	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N13/N14	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N15/N13	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N15/N16	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N16/N14	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N17/N18	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N19/N17	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N19/N20	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N20/N18	L 45 x 45 x 4 (L)	0.550	0.000	1.51

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N21/N22	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N23/N21	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N23/N24	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N24/N22	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N25/N26	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N27/N25	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N27/N28	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N28/N26	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N29/N30	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N31/N29	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N31/N32	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N32/N30	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N33/N34	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N35/N33	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N35/N36	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N36/N34	L 45 x 45 x 4 (L)	0.550	0.000	1.51
		N4/N10	L 45 x 45 x 4 (L)	0.743	0.000	2.04
		N10/N16	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N16/N18	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N18/N24	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N24/N26	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N26/N32	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N32/N34	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N34/N8	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N2/N9	L 45 x 45 x 4 (L)	0.743	0.000	2.04

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N9/N14	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N14/N17	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N17/N22	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N22/N25	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N25/N30	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N30/N33	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N33/N6	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N3/N12	L 45 x 45 x 4 (L)	0.743	0.000	2.04
		N12/N15	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N15/N20	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N20/N23	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N23/N28	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N28/N31	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N31/N36	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N36/N7	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N1/N11	L 45 x 45 x 4 (L)	0.743	0.000	2.04
		N11/N13	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N13/N19	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N19/N21	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N21/N27	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N27/N29	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N29/N35	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N35/N5	L 45 x 45 x 4 (L)	0.796	0.000	2.18
		N39/N79	L 45 x 45 x 4 (L)	1.184	0.000	3.24
		N79/N99	L 45 x 45 x 4 (L)	1.163	0.000	3.19

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N99/N81	L 45 x 45 x 4 (L)	1.141	0.000	3.13
		N81/N101	L 45 x 45 x 4 (L)	1.120	0.000	3.07
		N101/N83	L 45 x 45 x 4 (L)	1.099	0.000	3.01
		N83/N103	L 45 x 45 x 4 (L)	1.078	0.000	2.95
		N103/N85	L 45 x 45 x 4 (L)	1.057	0.000	2.90
		N85/N105	L 45 x 45 x 4 (L)	1.037	0.000	2.84
		N105/N87	L 45 x 45 x 4 (L)	1.016	0.000	2.78
		N87/N107	L 45 x 45 x 4 (L)	0.996	0.000	2.73
		N107/N89	L 45 x 45 x 4 (L)	0.976	0.000	2.67
		N89/N109	L 45 x 45 x 4 (L)	0.956	0.000	2.62
		N109/N91	L 45 x 45 x 4 (L)	0.937	0.000	2.57
		N91/N111	L 45 x 45 x 4 (L)	0.917	0.000	2.51
		N111/N93	L 45 x 45 x 4 (L)	0.898	0.000	2.46
		N93/N113	L 45 x 45 x 4 (L)	0.879	0.000	2.41
		N113/N95	L 45 x 45 x 4 (L)	0.861	0.000	2.36
		N95/N115	L 45 x 45 x 4 (L)	0.843	0.000	2.31
		N115/N97	L 45 x 45 x 4 (L)	0.825	0.000	2.26
		N97/N3	L 45 x 45 x 4 (L)	0.804	0.000	2.20
		N37/N60	L 45 x 45 x 4 (L)	1.184	0.000	3.24
		N60/N80	L 45 x 45 x 4 (L)	1.163	0.000	3.19
		N80/N62	L 45 x 45 x 4 (L)	1.141	0.000	3.13
		N62/N82	L 45 x 45 x 4 (L)	1.120	0.000	3.07
		N82/N64	L 45 x 45 x 4 (L)	1.099	0.000	3.01
		N64/N84	L 45 x 45 x 4 (L)	1.078	0.000	2.95
		N84/N66	L 45 x 45 x 4 (L)	1.057	0.000	2.90

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N66/N86	L 45 x 45 x 4 (L)	1.037	0.000	2.84
		N86/N68	L 45 x 45 x 4 (L)	1.016	0.000	2.78
		N68/N88	L 45 x 45 x 4 (L)	0.996	0.000	2.73
		N88/N70	L 45 x 45 x 4 (L)	0.976	0.000	2.67
		N70/N90	L 45 x 45 x 4 (L)	0.956	0.000	2.62
		N90/N72	L 45 x 45 x 4 (L)	0.937	0.000	2.57
		N72/N92	L 45 x 45 x 4 (L)	0.917	0.000	2.51
		N92/N74	L 45 x 45 x 4 (L)	0.898	0.000	2.46
		N74/N94	L 45 x 45 x 4 (L)	0.879	0.000	2.41
		N94/N76	L 45 x 45 x 4 (L)	0.861	0.000	2.36
		N76/N96	L 45 x 45 x 4 (L)	0.843	0.000	2.31
		N96/N78	L 45 x 45 x 4 (L)	0.825	0.000	2.26
		N78/N4	L 45 x 45 x 4 (L)	0.804	0.000	2.20
		N38/N41	L 45 x 45 x 4 (L)	1.184	0.000	3.24
		N41/N61	L 45 x 45 x 4 (L)	1.163	0.000	3.19
		N61/N43	L 45 x 45 x 4 (L)	1.141	0.000	3.13
		N43/N63	L 45 x 45 x 4 (L)	1.120	0.000	3.07
		N63/N45	L 45 x 45 x 4 (L)	1.099	0.000	3.01
		N45/N65	L 45 x 45 x 4 (L)	1.078	0.000	2.95
		N65/N47	L 45 x 45 x 4 (L)	1.057	0.000	2.90
		N47/N67	L 45 x 45 x 4 (L)	1.037	0.000	2.84
		N67/N49	L 45 x 45 x 4 (L)	1.016	0.000	2.78
		N49/N69	L 45 x 45 x 4 (L)	0.996	0.000	2.73
		N69/N51	L 45 x 45 x 4 (L)	0.976	0.000	2.67
		N51/N71	L 45 x 45 x 4 (L)	0.956	0.000	2.62

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N71/N53	L 45 x 45 x 4 (L)	0.937	0.000	2.57
		N53/N73	L 45 x 45 x 4 (L)	0.917	0.000	2.51
		N73/N55	L 45 x 45 x 4 (L)	0.898	0.000	2.46
		N55/N75	L 45 x 45 x 4 (L)	0.879	0.000	2.41
		N75/N57	L 45 x 45 x 4 (L)	0.861	0.000	2.36
		N57/N77	L 45 x 45 x 4 (L)	0.843	0.000	2.31
		N77/N59	L 45 x 45 x 4 (L)	0.825	0.000	2.26
		N59/N2	L 45 x 45 x 4 (L)	0.804	0.000	2.20
		N40/N98	L 45 x 45 x 4 (L)	1.184	0.000	3.24
		N98/N42	L 45 x 45 x 4 (L)	1.163	0.000	3.19
		N42/N100	L 45 x 45 x 4 (L)	1.141	0.000	3.13
		N100/N44	L 45 x 45 x 4 (L)	1.120	0.000	3.07
		N44/N102	L 45 x 45 x 4 (L)	1.099	0.000	3.01
		N102/N46	L 45 x 45 x 4 (L)	1.078	0.000	2.95
		N46/N104	L 45 x 45 x 4 (L)	1.057	0.000	2.90
		N104/N48	L 45 x 45 x 4 (L)	1.037	0.000	2.84
		N48/N106	L 45 x 45 x 4 (L)	1.016	0.000	2.78
		N106/N50	L 45 x 45 x 4 (L)	0.996	0.000	2.73
		N50/N108	L 45 x 45 x 4 (L)	0.976	0.000	2.67
		N108/N52	L 45 x 45 x 4 (L)	0.956	0.000	2.62
		N52/N110	L 45 x 45 x 4 (L)	0.937	0.000	2.57
		N110/N54	L 45 x 45 x 4 (L)	0.917	0.000	2.51
		N54/N112	L 45 x 45 x 4 (L)	0.898	0.000	2.46
		N112/N56	L 45 x 45 x 4 (L)	0.879	0.000	2.41
		N56/N114	L 45 x 45 x 4 (L)	0.861	0.000	2.36

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N114/N58	L 45 x 45 x 4 (L)	0.843	0.000	2.31
		N58/N116	L 45 x 45 x 4 (L)	0.825	0.000	2.26
		N116/N1	L 45 x 45 x 4 (L)	0.804	0.000	2.20
		N40/N41	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N42/N43	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N43/N44	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N44/N45	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N45/N46	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N46/N47	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N47/N48	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N48/N49	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N49/N50	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N50/N51	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N51/N52	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N52/N53	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N53/N54	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N54/N55	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N55/N56	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N56/N57	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N57/N58	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N58/N59	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N59/N1	L 80 x 80 x 8 (L)	0.575	0.001	5.55
		N38/N60	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N61/N62	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N62/N63	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11



Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N63/N64	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N64/N65	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N65/N66	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N66/N67	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N67/N68	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N68/N69	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N69/N70	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N70/N71	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N71/N72	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N72/N73	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N73/N74	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N74/N75	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N75/N76	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N76/N77	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N77/N78	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N78/N2	L 80 x 80 x 8 (L)	0.575	0.001	5.55
		N37/N79	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N80/N81	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N81/N82	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N82/N83	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N83/N84	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N84/N85	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N85/N86	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N86/N87	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N87/N88	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N88/N89	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N89/N90	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N90/N91	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N91/N92	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N92/N93	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N93/N94	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N94/N95	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N95/N96	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N96/N97	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N97/N4	L 80 x 80 x 8 (L)	0.575	0.001	5.55
		N39/N98	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N99/N100	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N100/N101	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N101/N102	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N102/N103	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N103/N104	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N104/N105	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N105/N106	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N106/N107	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N107/N108	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N108/N109	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N109/N110	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N110/N111	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N111/N112	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N112/N113	L 80 x 80 x 8 (L)	0.580	0.001	5.60

Takeoff table						
Material		Element (Ni/Nf)	Section(Series)	Length (m)	Volume (m³)	Weight (kg)
Type	Designation					
		N113/N114	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N114/N115	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N115/N116	L 80 x 80 x 8 (L)	0.580	0.001	5.60
		N116/N3	L 80 x 80 x 8 (L)	0.575	0.001	5.55
		N98/N99	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N79/N80	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N60/N61	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N41/N42	2xL 90 x 90 x 9(T) (L)	0.580	0.002	14.11
		N5/N8	L 45 x 45 x 4 (L)	0.778	0.000	2.13
		N7/N6	L 45 x 45 x 4 (L)	0.778	0.000	2.13
Notation: Ni: Initial node Nf: Final node						

### 2.1.2.5.- Takeoff summary

Takeoff summary												
Type	Material		Section	Length			Volume			Weight		
	Designation	Serie s		Section (m)	Series (m)	Material (m)	Section (m³)	Serie s (m³)	Material (m³)	Section (kg)	Serie s (kg)	Material (kg)
Rolled steel	S275 (EN 1993-1-1)	L	L 45 x 45 x 4	125.763			0.044			344.55		
			L 70 x 70 x 6	18.100			0.015			115.52		
			L 90 x 90 x 9, Double welded in T	34.800			0.108			846.86		
			L 80 x 80 x 8	11.581			0.014			111.82		
					190.244			0.181		1418.74		
						190.244			0.181			1418.74

### 2.1.2.6.- Surface area measurement

Rolled steel: Measurement of the surface areas to paint				
Series	Section	Unit surface area (m²/m)	Length (m)	Surface (m²)
L	L 45 x 45 x 4	0.180	125.763	22.637

Rolled steel: Measurement of the surface areas to paint				
Series	Section	Unit surface area (m <sup>2</sup> /m)	Length (m)	Surface (m <sup>2</sup> )
	L 70 x 70 x 6	0.280	18.100	5.068
	L 90 x 90 x 9, Double welded in T	0.540	34.800	18.792
	L 80 x 80 x 8	0.320	11.581	3.706
<b>Total</b>				<b>50.203</b>

## 2.2.- Loads

### 2.2.1.- Nodes

Loads on nodes					
Reference	Loadcase	Point loads (kN)	Direction		
			X	Y	Z
N117	Ft_1	1.42	-1.000	0.000	0.000
N117	Ft_2	1.57	-0.707	-0.707	0.000
N117	Ft_3	1.44	0.000	-1.000	0.000
N117	Ft_4	1.60	0.707	-0.707	0.000
N117	Ft_5	1.46	1.000	0.000	0.000
N117	Ft_6	1.61	0.707	0.707	0.000
N117	Ft_7	1.44	0.000	1.000	0.000
N117	Ft_8	1.60	-0.707	0.707	0.000

### 2.2.2.- Bars

References:

'P1', 'P2':

- Point moments, point, uniform and strip loads: 'P1' is the load value. 'P2' is not used.
- Trapezoidal loads: 'P1' is the value of the load at the point where it begins (L1) and 'P2' is the value of the load where it ends (L2).
- Triangular loads: 'P1' is the maximum value of the load. 'P2' is not used.
- Temperature increments: 'P1' and 'P2' are the temperature values on the external faces or surfaces of the element. The position of the temperature increment over the transverse section will depend on the selected direction.

'L1', 'L2':

- Point loads and moments: 'L1' is the distance between the initial node of the bar and the position where the load is applied. 'L2' is not used.
- Trapezoidal, strip and triangular loads: 'L1' is the distance between the initial node of the bar and the position where the load begins, 'L2' is the distance between the initial node of the bar and the position where the load ends.

Units:

- Point loads: kN
- Point moments: kN·m.
- Uniform, strip, triangular and trapezoidal loads: kN/m.
- Temperature increments: °C.

Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N1/N2	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N3/N1	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N3/N4	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N4/N2	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N5/N6	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N7/N5	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N7/N8	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N8/N6	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N2/N10	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N10/N14	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N14/N18	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N18/N22	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N22/N26	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N26/N30	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N30/N34	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N34/N6	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N1/N9	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N9/N13	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N13/N17	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N17/N21	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N21/N25	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N25/N29	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N29/N33	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N33/N5	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N4/N12	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N12/N16	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N16/N20	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N20/N24	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N24/N28	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N28/N32	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N32/N36	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N36/N8	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N3/N11	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N11/N15	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N15/N19	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N19/N23	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N23/N27	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N27/N31	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N31/N35	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N35/N7	Self weight	Uniform	0.063	-	-	-	Global	0.000	0.000	-1.000
N9/N10	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N11/N9	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N11/N12	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N12/N10	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N13/N14	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000

Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N15/N13	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N15/N16	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N16/N14	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N17/N18	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N19/N17	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N19/N20	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N20/N18	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N21/N22	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N23/N21	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N23/N24	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N24/N22	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N25/N26	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N27/N25	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N27/N28	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N28/N26	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N29/N30	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N31/N29	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N31/N32	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N32/N30	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N33/N34	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N35/N33	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N35/N36	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N36/N34	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N4/N10	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N10/N16	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N16/N18	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N18/N24	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N24/N26	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N26/N32	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N32/N34	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N34/N8	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N2/N9	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N9/N14	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N14/N17	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N17/N22	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N22/N25	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N25/N30	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N30/N33	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N33/N6	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N3/N12	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N12/N15	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N15/N20	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N20/N23	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N23/N28	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N28/N31	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N31/N36	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000

Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N36/N7	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N1/N11	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N11/N13	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N13/N19	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N19/N21	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N21/N27	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N27/N29	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N29/N35	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N35/N5	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N39/N79	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N79/N99	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N99/N81	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N81/N101	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N101/N83	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N83/N103	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N103/N85	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N85/N105	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N105/N87	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N87/N107	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N107/N89	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N89/N109	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N109/N91	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N91/N111	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N111/N93	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N93/N113	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N113/N95	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N95/N115	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N115/N97	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N97/N3	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N37/N60	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N60/N80	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N80/N62	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N62/N82	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N82/N64	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N64/N84	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N84/N66	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N66/N86	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N86/N68	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N68/N88	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N88/N70	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N70/N90	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N90/N72	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N72/N92	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N92/N74	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N74/N94	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N94/N76	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000

Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N76/N96	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N96/N78	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N78/N4	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N38/N41	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N41/N61	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N61/N43	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N43/N63	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N63/N45	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N45/N65	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N65/N47	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N47/N67	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N67/N49	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N49/N69	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N69/N51	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N51/N71	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N71/N53	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N53/N73	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N73/N55	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N55/N75	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N75/N57	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N57/N77	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N77/N59	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N59/N2	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N40/N98	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N98/N42	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N42/N100	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N100/N44	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N44/N102	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N102/N46	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N46/N104	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N104/N48	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N48/N106	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N106/N50	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N50/N108	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N108/N52	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N52/N110	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N110/N54	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N54/N112	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N112/N56	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N56/N114	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N114/N58	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N58/N116	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N116/N1	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N40/N41	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N42/N43	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N43/N44	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000



Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N44/N45	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N45/N46	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N46/N47	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N47/N48	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N48/N49	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N49/N50	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N50/N51	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N51/N52	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N52/N53	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N53/N54	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N54/N55	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N55/N56	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N56/N57	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N57/N58	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N58/N59	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N59/N1	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N38/N60	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N61/N62	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N62/N63	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N63/N64	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N64/N65	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N65/N66	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N66/N67	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N67/N68	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N68/N69	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N69/N70	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N70/N71	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N71/N72	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N72/N73	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N73/N74	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N74/N75	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N75/N76	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N76/N77	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N77/N78	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N78/N2	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N37/N79	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N80/N81	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N81/N82	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N82/N83	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N83/N84	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N84/N85	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N85/N86	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N86/N87	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N87/N88	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N88/N89	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N89/N90	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000

Loads on bars										
Bar	Loadcase	Type	Values		Position		Direction			
			P1	P2	L1 (m)	L2 (m)	Centre axis	X	Y	Z
N90/N91	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N91/N92	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N92/N93	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N93/N94	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N94/N95	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N95/N96	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N96/N97	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N97/N4	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N39/N98	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N99/N100	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N100/N101	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N101/N102	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N102/N103	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N103/N104	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N104/N105	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N105/N106	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N106/N107	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N107/N108	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N108/N109	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N109/N110	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N110/N111	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N111/N112	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N112/N113	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N113/N114	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N114/N115	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N115/N116	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N116/N3	Self weight	Uniform	0.095	-	-	-	Global	0.000	0.000	-1.000
N98/N99	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N79/N80	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N60/N61	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N41/N42	Self weight	Uniform	0.239	-	-	-	Global	0.000	0.000	-1.000
N5/N117	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N117/N8	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N7/N117	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000
N117/N6	Self weight	Uniform	0.027	-	-	-	Global	0.000	0.000	-1.000

## 2.3.- Results

### 2.3.1.- Nodes

#### 2.3.1.1.- Displacements

References:

Dx, Dy, Dz: Node displacements in global axes.

Gx, Gy, Gz: Node rotations in global axes.

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N1	Displacement s	Minimum envelope value	- 2.611	- 2.648	- 0.276	-	-	-
		Maximum envelope value	2.686	2.649	0.199	-	-	-
N2	Displacement s	Minimum envelope value	- 2.612	- 2.649	- 0.277	-	-	-
		Maximum envelope value	2.684	2.650	0.194	-	-	-
N3	Displacement s	Minimum envelope value	- 2.609	- 2.649	- 0.271	-	-	-
		Maximum envelope value	2.684	2.647	0.200	-	-	-
N4	Displacement s	Minimum envelope value	- 2.613	- 2.648	- 0.276	-	-	-
		Maximum envelope value	2.685	2.646	0.199	-	-	-
N5	Displacement s	Minimum envelope value	- 6.029	- 6.118	- 0.405	-0.851	-0.851	0.005
		Maximum envelope value	6.199	6.118	0.312	0.809	0.865	0.021
N6	Displacement s	Minimum envelope value	- 6.032	- 6.115	- 0.407	-0.809	-0.854	-0.020
		Maximum envelope value	6.202	6.116	0.306	0.851	0.873	-0.004
N7	Displacement s	Minimum envelope value	- 6.032	- 6.116	- 0.398	-	-	-
		Maximum envelope value	6.202	6.115	0.315	-	-	-
N8	Displacement s	Minimum envelope value	- 6.030	- 6.118	- 0.405	-	-	-
		Maximum envelope value	6.199	6.118	0.312	-	-	-
N9	Displacement s	Minimum envelope value	- 2.912	- 2.953	- 0.303	-	-	-
		Maximum envelope value	2.993	2.952	0.223	-	-	-
N10	Displacement s	Minimum envelope value	- 2.911	- 2.953	- 0.304	-	-	-
		Maximum envelope value	2.995	2.952	0.218	-	-	-
N11	Displacement s	Minimum envelope value	- 2.912	- 2.950	- 0.298	-	-	-
		Maximum envelope value	2.993	2.951	0.224	-	-	-
N12	Displacement s	Minimum envelope value	- 2.912	- 2.951	- 0.303	-	-	-
		Maximum envelope value	2.995	2.952	0.223	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N13	Displacement s	Minimum envelope value	- 3.288	- 3.337	- 0.330	-	-	-
		Maximum envelope value	3.382	3.339	0.246	-	-	-
N14	Displacement s	Minimum envelope value	- 3.290	- 3.337	- 0.332	-	-	-
		Maximum envelope value	3.381	3.338	0.241	-	-	-
N15	Displacement s	Minimum envelope value	- 3.288	- 3.337	- 0.325	-	-	-
		Maximum envelope value	3.382	3.336	0.248	-	-	-
N16	Displacement s	Minimum envelope value	- 3.290	- 3.337	- 0.330	-	-	-
		Maximum envelope value	3.381	3.336	0.246	-	-	-
N17	Displacement s	Minimum envelope value	- 3.700	- 3.752	- 0.353	-	-	-
		Maximum envelope value	3.804	3.752	0.267	-	-	-
N18	Displacement s	Minimum envelope value	- 3.700	- 3.752	- 0.355	-	-	-
		Maximum envelope value	3.805	3.751	0.261	-	-	-
N19	Displacement s	Minimum envelope value	- 3.700	- 3.750	- 0.347	-	-	-
		Maximum envelope value	3.803	3.751	0.269	-	-	-
N20	Displacement s	Minimum envelope value	- 3.700	- 3.751	- 0.353	-	-	-
		Maximum envelope value	3.805	3.751	0.267	-	-	-
N21	Displacement s	Minimum envelope value	- 4.134	- 4.194	- 0.371	-	-	-
		Maximum envelope value	4.251	4.195	0.283	-	-	-
N22	Displacement s	Minimum envelope value	- 4.135	- 4.194	- 0.374	-	-	-
		Maximum envelope value	4.250	4.195	0.277	-	-	-
N23	Displacement s	Minimum envelope value	- 4.133	- 4.194	- 0.366	-	-	-
		Maximum envelope value	4.251	4.193	0.285	-	-	-
N24	Displacement s	Minimum envelope value	- 4.135	- 4.194	- 0.371	-	-	-
		Maximum envelope value	4.250	4.193	0.283	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N25	Displacement s	Minimum envelope value	- 4.591	- 4.656	- 0.386	-	-	-
		Maximum envelope value	4.720	4.656	0.296	-	-	-
N26	Displacement s	Minimum envelope value	- 4.591	- 4.656	- 0.388	-	-	-
		Maximum envelope value	4.720	4.655	0.290	-	-	-
N27	Displacement s	Minimum envelope value	- 4.591	- 4.655	- 0.380	-	-	-
		Maximum envelope value	4.719	4.655	0.298	-	-	-
N28	Displacement s	Minimum envelope value	- 4.591	- 4.655	- 0.386	-	-	-
		Maximum envelope value	4.720	4.655	0.296	-	-	-
N29	Displacement s	Minimum envelope value	- 5.061	- 5.134	- 0.396	-	-	-
		Maximum envelope value	5.204	5.135	0.305	-	-	-
N30	Displacement s	Minimum envelope value	- 5.062	- 5.134	- 0.399	-	-	-
		Maximum envelope value	5.204	5.135	0.299	-	-	-
N31	Displacement s	Minimum envelope value	- 5.061	- 5.134	- 0.390	-	-	-
		Maximum envelope value	5.204	5.133	0.307	-	-	-
N32	Displacement s	Minimum envelope value	- 5.062	- 5.134	- 0.396	-	-	-
		Maximum envelope value	5.204	5.133	0.305	-	-	-
N33	Displacement s	Minimum envelope value	- 5.543	- 5.622	- 0.403	-	-	-
		Maximum envelope value	5.699	5.622	0.310	-	-	-
N34	Displacement s	Minimum envelope value	- 5.543	- 5.622	- 0.405	-	-	-
		Maximum envelope value	5.699	5.622	0.304	-	-	-
N35	Displacement s	Minimum envelope value	- 5.543	- 5.622	- 0.396	-	-	-
		Maximum envelope value	5.699	5.622	0.313	-	-	-
N36	Displacement s	Minimum envelope value	- 5.543	- 5.622	- 0.403	-	-	-
		Maximum envelope value	5.699	5.622	0.310	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N37	Displacement s	Minimum envelope value	0.000	0.000	0.000	-	-	-
		Maximum envelope value	0.000	0.000	0.000	-	-	-
N38	Displacement s	Minimum envelope value	0.000	0.000	0.000	-	-	-
		Maximum envelope value	0.000	0.000	0.000	-	-	-
N39	Displacement s	Minimum envelope value	0.000	0.000	0.000	-	-	-
		Maximum envelope value	0.000	0.000	0.000	-	-	-
N40	Displacement s	Minimum envelope value	0.000	0.000	0.000	-	-	-
		Maximum envelope value	0.000	0.000	0.000	-	-	-
N41	Displacement s	Minimum envelope value	- 0.014	- 0.015	- 0.018	-	-	-
		Maximum envelope value	0.015	0.012	0.012	-	-	-
N42	Displacement s	Minimum envelope value	- 0.034	- 0.036	- 0.035	-	-	-
		Maximum envelope value	0.035	0.032	0.024	-	-	-
N43	Displacement s	Minimum envelope value	- 0.066	- 0.069	- 0.052	-	-	-
		Maximum envelope value	0.067	0.066	0.035	-	-	-
N44	Displacement s	Minimum envelope value	- 0.110	- 0.113	- 0.068	-	-	-
		Maximum envelope value	0.113	0.110	0.045	-	-	-
N45	Displacement s	Minimum envelope value	- 0.165	- 0.168	- 0.083	-	-	-
		Maximum envelope value	0.169	0.165	0.056	-	-	-
N46	Displacement s	Minimum envelope value	- 0.231	- 0.235	- 0.097	-	-	-
		Maximum envelope value	0.237	0.233	0.065	-	-	-
N47	Displacement s	Minimum envelope value	- 0.308	- 0.314	- 0.111	-	-	-
		Maximum envelope value	0.317	0.311	0.075	-	-	-
N48	Displacement s	Minimum envelope value	- 0.398	- 0.405	- 0.123	-	-	-
		Maximum envelope value	0.409	0.402	0.083	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N49	Displacement s	Minimum envelope value	- 0.498	- 0.507	- 0.135	-	-	-
		Maximum envelope value	0.512	0.504	0.092	-	-	-
N50	Displacement s	Minimum envelope value	- 0.611	- 0.621	- 0.146	-	-	-
		Maximum envelope value	0.628	0.619	0.099	-	-	-
N51	Displacement s	Minimum envelope value	- 0.735	- 0.747	- 0.156	-	-	-
		Maximum envelope value	0.756	0.745	0.106	-	-	-
N52	Displacement s	Minimum envelope value	- 0.872	- 0.886	- 0.165	-	-	-
		Maximum envelope value	0.896	0.883	0.113	-	-	-
N53	Displacement s	Minimum envelope value	- 1.021	- 1.036	- 0.174	-	-	-
		Maximum envelope value	1.049	1.034	0.118	-	-	-
N54	Displacement s	Minimum envelope value	- 1.180	- 1.198	- 0.181	-	-	-
		Maximum envelope value	1.213	1.196	0.123	-	-	-
N55	Displacement s	Minimum envelope value	- 1.349	- 1.373	- 0.187	-	-	-
		Maximum envelope value	1.387	1.371	0.128	-	-	-
N56	Displacement s	Minimum envelope value	- 1.544	- 1.568	- 0.210	-	-	-
		Maximum envelope value	1.590	1.567	0.146	-	-	-
N57	Displacement s	Minimum envelope value	- 1.770	- 1.795	- 0.230	-	-	-
		Maximum envelope value	1.821	1.793	0.163	-	-	-
N58	Displacement s	Minimum envelope value	- 2.021	- 2.052	- 0.248	-	-	-
		Maximum envelope value	2.079	2.050	0.177	-	-	-
N59	Displacement s	Minimum envelope value	- 2.301	- 2.338	- 0.263	-	-	-
		Maximum envelope value	2.367	2.337	0.189	-	-	-
N60	Displacement s	Minimum envelope value	- 0.012	- 0.014	- 0.018	-	-	-
		Maximum envelope value	0.015	0.014	0.012	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N61	Displacement s	Minimum envelope value	- 0.032	- 0.034	- 0.035	-	-	-
		Maximum envelope value	0.036	0.034	0.023	-	-	-
N62	Displacement s	Minimum envelope value	- 0.065	- 0.067	- 0.052	-	-	-
		Maximum envelope value	0.070	0.066	0.034	-	-	-
N63	Displacement s	Minimum envelope value	- 0.108	- 0.111	- 0.068	-	-	-
		Maximum envelope value	0.114	0.111	0.044	-	-	-
N64	Displacement s	Minimum envelope value	- 0.163	- 0.167	- 0.083	-	-	-
		Maximum envelope value	0.171	0.167	0.054	-	-	-
N65	Displacement s	Minimum envelope value	- 0.229	- 0.234	- 0.098	-	-	-
		Maximum envelope value	0.239	0.234	0.064	-	-	-
N66	Displacement s	Minimum envelope value	- 0.307	- 0.313	- 0.111	-	-	-
		Maximum envelope value	0.318	0.313	0.073	-	-	-
N67	Displacement s	Minimum envelope value	- 0.396	- 0.403	- 0.124	-	-	-
		Maximum envelope value	0.410	0.403	0.081	-	-	-
N68	Displacement s	Minimum envelope value	- 0.497	- 0.506	- 0.136	-	-	-
		Maximum envelope value	0.514	0.505	0.089	-	-	-
N69	Displacement s	Minimum envelope value	- 0.610	- 0.620	- 0.147	-	-	-
		Maximum envelope value	0.629	0.620	0.097	-	-	-
N70	Displacement s	Minimum envelope value	- 0.734	- 0.746	- 0.157	-	-	-
		Maximum envelope value	0.757	0.746	0.104	-	-	-
N71	Displacement s	Minimum envelope value	- 0.871	- 0.885	- 0.166	-	-	-
		Maximum envelope value	0.898	0.884	0.110	-	-	-
N72	Displacement s	Minimum envelope value	- 1.019	- 1.036	- 0.175	-	-	-
		Maximum envelope value	1.050	1.035	0.116	-	-	-



Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N73	Displacement s	Minimum envelope value	- 1.179	- 1.197	- 0.182	-	-	-
		Maximum envelope value	1.214	1.197	0.121	-	-	-
N74	Displacement s	Minimum envelope value	- 1.351	- 1.368	- 0.188	-	-	-
		Maximum envelope value	1.391	1.368	0.125	-	-	-
N75	Displacement s	Minimum envelope value	- 1.545	- 1.567	- 0.211	-	-	-
		Maximum envelope value	1.590	1.568	0.143	-	-	-
N76	Displacement s	Minimum envelope value	- 1.768	- 1.797	- 0.231	-	-	-
		Maximum envelope value	1.820	1.799	0.159	-	-	-
N77	Displacement s	Minimum envelope value	- 2.021	- 2.050	- 0.249	-	-	-
		Maximum envelope value	2.080	2.052	0.173	-	-	-
N78	Displacement s	Minimum envelope value	- 2.304	- 2.329	- 0.265	-	-	-
		Maximum envelope value	2.370	2.330	0.185	-	-	-
N79	Displacement s	Minimum envelope value	- 0.014	- 0.012	- 0.018	-	-	-
		Maximum envelope value	0.014	0.015	0.012	-	-	-
N80	Displacement s	Minimum envelope value	- 0.034	- 0.032	- 0.035	-	-	-
		Maximum envelope value	0.035	0.036	0.024	-	-	-
N81	Displacement s	Minimum envelope value	- 0.066	- 0.066	- 0.052	-	-	-
		Maximum envelope value	0.068	0.069	0.035	-	-	-
N82	Displacement s	Minimum envelope value	- 0.110	- 0.110	- 0.068	-	-	-
		Maximum envelope value	0.113	0.113	0.045	-	-	-
N83	Displacement s	Minimum envelope value	- 0.165	- 0.165	- 0.083	-	-	-
		Maximum envelope value	0.169	0.168	0.056	-	-	-
N84	Displacement s	Minimum envelope value	- 0.231	- 0.232	- 0.097	-	-	-
		Maximum envelope value	0.237	0.235	0.065	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N85	Displacement s	Minimum envelope value	- 0.308	- 0.311	- 0.111	-	-	-
		Maximum envelope value	0.317	0.314	0.075	-	-	-
N86	Displacement s	Minimum envelope value	- 0.397	- 0.402	- 0.123	-	-	-
		Maximum envelope value	0.409	0.404	0.083	-	-	-
N87	Displacement s	Minimum envelope value	- 0.498	- 0.504	- 0.135	-	-	-
		Maximum envelope value	0.513	0.506	0.091	-	-	-
N88	Displacement s	Minimum envelope value	- 0.611	- 0.618	- 0.146	-	-	-
		Maximum envelope value	0.628	0.621	0.099	-	-	-
N89	Displacement s	Minimum envelope value	- 0.735	- 0.744	- 0.156	-	-	-
		Maximum envelope value	0.756	0.747	0.106	-	-	-
N90	Displacement s	Minimum envelope value	- 0.872	- 0.883	- 0.165	-	-	-
		Maximum envelope value	0.897	0.885	0.113	-	-	-
N91	Displacement s	Minimum envelope value	- 1.021	- 1.033	- 0.174	-	-	-
		Maximum envelope value	1.050	1.035	0.118	-	-	-
N92	Displacement s	Minimum envelope value	- 1.180	- 1.196	- 0.181	-	-	-
		Maximum envelope value	1.214	1.197	0.123	-	-	-
N93	Displacement s	Minimum envelope value	- 1.349	- 1.370	- 0.187	-	-	-
		Maximum envelope value	1.387	1.372	0.128	-	-	-
N94	Displacement s	Minimum envelope value	- 1.546	- 1.566	- 0.210	-	-	-
		Maximum envelope value	1.588	1.568	0.146	-	-	-
N95	Displacement s	Minimum envelope value	- 1.772	- 1.792	- 0.230	-	-	-
		Maximum envelope value	1.820	1.794	0.163	-	-	-
N96	Displacement s	Minimum envelope value	- 2.023	- 2.049	- 0.248	-	-	-
		Maximum envelope value	2.078	2.050	0.177	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N97	Displacement s	Minimum envelope value	- 2.301	- 2.336	- 0.263	-	-	-
		Maximum envelope value	2.366	2.337	0.189	-	-	-
N98	Displacement s	Minimum envelope value	- 0.015	- 0.014	- 0.018	-	-	-
		Maximum envelope value	0.012	0.014	0.012	-	-	-
N99	Displacement s	Minimum envelope value	- 0.035	- 0.034	- 0.035	-	-	-
		Maximum envelope value	0.033	0.034	0.024	-	-	-
N100	Displacement s	Minimum envelope value	- 0.068	- 0.066	- 0.051	-	-	-
		Maximum envelope value	0.066	0.067	0.035	-	-	-
N101	Displacement s	Minimum envelope value	- 0.111	- 0.111	- 0.067	-	-	-
		Maximum envelope value	0.111	0.111	0.046	-	-	-
N102	Displacement s	Minimum envelope value	- 0.166	- 0.167	- 0.081	-	-	-
		Maximum envelope value	0.168	0.167	0.056	-	-	-
N103	Displacement s	Minimum envelope value	- 0.232	- 0.234	- 0.096	-	-	-
		Maximum envelope value	0.236	0.234	0.066	-	-	-
N104	Displacement s	Minimum envelope value	- 0.310	- 0.312	- 0.109	-	-	-
		Maximum envelope value	0.316	0.313	0.075	-	-	-
N105	Displacement s	Minimum envelope value	- 0.399	- 0.403	- 0.121	-	-	-
		Maximum envelope value	0.407	0.403	0.084	-	-	-
N106	Displacement s	Minimum envelope value	- 0.500	- 0.505	- 0.133	-	-	-
		Maximum envelope value	0.511	0.505	0.092	-	-	-
N107	Displacement s	Minimum envelope value	- 0.612	- 0.619	- 0.144	-	-	-
		Maximum envelope value	0.627	0.620	0.100	-	-	-
N108	Displacement s	Minimum envelope value	- 0.737	- 0.745	- 0.154	-	-	-
		Maximum envelope value	0.755	0.746	0.107	-	-	-

Node displacement envelope								
Referenc e	Combination		Displacements in global axes					
	Type	Description	Dx (mm)	Dy (mm)	Dz (mm)	Rx (mRad )	Ry (mRad )	Rz (mRad )
N109	Displacement s	Minimum envelope value	- 0.873	- 0.884	- 0.163	-	-	-
		Maximum envelope value	0.895	0.884	0.113	-	-	-
N110	Displacement s	Minimum envelope value	- 1.021	- 1.034	- 0.171	-	-	-
		Maximum envelope value	1.048	1.035	0.119	-	-	-
N111	Displacement s	Minimum envelope value	- 1.181	- 1.196	- 0.178	-	-	-
		Maximum envelope value	1.212	1.197	0.124	-	-	-
N112	Displacement s	Minimum envelope value	- 1.353	- 1.367	- 0.184	-	-	-
		Maximum envelope value	1.389	1.367	0.129	-	-	-
N113	Displacement s	Minimum envelope value	- 1.546	- 1.568	- 0.207	-	-	-
		Maximum envelope value	1.588	1.566	0.147	-	-	-
N114	Displacement s	Minimum envelope value	- 1.769	- 1.798	- 0.226	-	-	-
		Maximum envelope value	1.817	1.796	0.164	-	-	-
N115	Displacement s	Minimum envelope value	- 2.022	- 2.051	- 0.244	-	-	-
		Maximum envelope value	2.077	2.049	0.178	-	-	-
N116	Displacement s	Minimum envelope value	- 2.305	- 2.327	- 0.259	-	-	-
		Maximum envelope value	2.368	2.327	0.191	-	-	-
N117	Displacement s	Minimum envelope value	- 6.036	- 6.122	- 0.056	-0.821	-0.821	-0.003
		Maximum envelope value	6.206	6.122	0.047	0.823	0.834	0.004

### 2.3.1.2.- Reactions

References:

Rx, Ry, Rz: Node reactions with displacements with external fixity (forces).

Mx, My, Mz: Node reactions with rotations with external fixity (moments).

**2.3.1.2.1.- Loadcase**

<b>Node reactions by loadcase</b>							
Reference	Description	Reactions in global axes					
		Rx (kN)	Ry (kN)	Rz (kN)	Mx (kN·m)	My (kN·m)	Mz (kN·m)
N37	Self weight	0.079	-0.079	3.479	0.00	0.00	0.00
	Ft_1	0.516	-0.259	10.951	0.00	0.00	0.00
	Ft_2	0.201	-0.051	0.004	0.00	0.00	0.00
	Ft_3	-0.263	0.197	-11.099	0.00	0.00	0.00
	Ft_4	-0.618	0.361	-17.445	0.00	0.00	0.00
	Ft_5	-0.531	0.267	-11.259	0.00	0.00	0.00
	Ft_6	-0.206	0.052	-0.004	0.00	0.00	0.00
	Ft_7	0.263	-0.197	11.099	0.00	0.00	0.00
	Ft_8	0.618	-0.361	17.445	0.00	0.00	0.00
N38	Self weight	-0.079	-0.079	3.480	0.00	0.00	0.00
	Ft_1	0.194	0.259	-10.951	0.00	0.00	0.00
	Ft_2	0.354	0.606	-17.124	0.00	0.00	0.00
	Ft_3	0.263	0.523	-11.107	0.00	0.00	0.00
	Ft_4	0.052	0.205	-0.002	0.00	0.00	0.00
	Ft_5	-0.200	-0.267	11.259	0.00	0.00	0.00
	Ft_6	-0.364	-0.622	17.560	0.00	0.00	0.00
	Ft_7	-0.263	-0.523	11.107	0.00	0.00	0.00
	Ft_8	-0.052	-0.205	0.002	0.00	0.00	0.00
N39	Self weight	0.079	0.079	3.480	0.00	0.00	0.00
	Ft_1	0.194	0.259	10.947	0.00	0.00	0.00
	Ft_2	0.354	0.606	17.116	0.00	0.00	0.00
	Ft_3	0.263	0.523	11.099	0.00	0.00	0.00
	Ft_4	0.052	0.204	-0.002	0.00	0.00	0.00
	Ft_5	-0.199	-0.267	-11.256	0.00	0.00	0.00
	Ft_6	-0.363	-0.621	-17.552	0.00	0.00	0.00
	Ft_7	-0.263	-0.523	-11.099	0.00	0.00	0.00
	Ft_8	-0.052	-0.204	0.002	0.00	0.00	0.00
N40	Self weight	-0.079	0.079	3.479	0.00	0.00	0.00
	Ft_1	0.516	-0.259	-10.947	0.00	0.00	0.00
	Ft_2	0.200	-0.051	0.004	0.00	0.00	0.00
	Ft_3	-0.263	0.197	11.107	0.00	0.00	0.00
	Ft_4	-0.618	0.361	17.449	0.00	0.00	0.00
	Ft_5	-0.530	0.267	11.256	0.00	0.00	0.00
	Ft_6	-0.206	0.052	-0.004	0.00	0.00	0.00
	Ft_7	0.263	-0.197	-11.107	0.00	0.00	0.00
	Ft_8	0.618	-0.361	-17.449	0.00	0.00	0.00

**2.3.2.- Bars**

References:

N: Axial force (kN)

Vy: Shear force in the local Y axis of the bar. (kN)

Vz: Shear force in the local Z axis of the bar. (kN)

Mt: Torsional moment (kN·m)

My: Bending moment in the 'XZ' plane (section rotation with respect to the local 'Y' axis of the bar). (kN·m)

Mz: Bending moment in the 'XY' plane (section rotation with respect to the local 'Z' axis of the bar). (kN·m)

### 2.3.2.1.1.- Envelope

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N1/N2	Rolled steel	N <sub>min</sub>	-0.219	-0.219	-0.219
		N <sub>max</sub>	0.212	0.212	0.212
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N3/N1	Rolled steel	N <sub>min</sub>	-0.293	-0.293	-0.293
		N <sub>max</sub>	0.279	0.279	0.279
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N3/N4	Rolled steel	$N_{min}$	-0.264	-0.264	-0.264
		$N_{max}$	0.249	0.249	0.249
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N4/N2	Rolled steel	$N_{min}$	-0.254	-0.254	-0.254
		$N_{max}$	0.235	0.235	0.235
		$V_{y_{min}}$	0.000	0.000	0.000

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N5/N6	Rolled steel	$N_{min}$	-0.850	-0.850	-0.850
		$N_{max}$	0.842	0.842	0.842
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N7/N5	Rolled steel	N <sub>min</sub>	-0.841	-0.841	-0.841
		N <sub>max</sub>	0.820	0.820	0.820
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N7/N8	Rolled steel	N <sub>min</sub>	-0.843	-0.843	-0.843
		N <sub>max</sub>	0.853	0.853	0.853
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N8/N6	Rolled steel	$N_{min}$	-0.820	-0.820	-0.820
		$N_{max}$	0.835	0.835	0.835
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
N2/N10	Rolled steel	$N_{min}$	-13.860	-13.839	-13.818
		$N_{max}$	12.208	12.224	12.239
		$V_{y_{min}}$	-0.086	-0.086	-0.086
		$V_{y_{max}}$	0.095	0.095	0.095
		$V_{z_{min}}$	-0.071	-0.071	-0.071
		$V_{z_{max}}$	0.068	0.068	0.068

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.03	-0.02	-0.03
		$M_{z_{max}}$	0.03	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N10/N14	Rolled steel	$N_{min}$	-12.088	-12.063	-12.039
		$N_{max}$	10.643	10.661	10.679
		$V_{y_{min}}$	-0.095	-0.095	-0.095
		$V_{y_{max}}$	0.089	0.089	0.089
		$V_{z_{min}}$	-0.082	-0.082	-0.082
		$V_{z_{max}}$	0.087	0.087	0.087
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.01	-0.03
		$M_{y_{max}}$	0.03	0.01	0.03
		$M_{z_{min}}$	-0.03	-0.01	-0.03
		$M_{z_{max}}$	0.03	0.01	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N14/N18	Rolled steel	$N_{min}$	-10.234	-10.210	-10.186
		$N_{max}$	9.001	9.019	9.037

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$V_{y_{min}}$	-0.077	-0.077	-0.077
		$V_{y_{max}}$	0.083	0.083	0.083
		$V_{z_{min}}$	-0.083	-0.083	-0.083
		$V_{z_{max}}$	0.078	0.078	0.078
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.01	-0.02
		$M_{y_{max}}$	0.03	0.01	0.02
		$M_{z_{min}}$	-0.03	-0.01	-0.02
		$M_{z_{max}}$	0.03	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N18/N22	Rolled steel	$N_{min}$	-8.380	-8.356	-8.331
		$N_{max}$	7.356	7.374	7.392
		$V_{y_{min}}$	-0.070	-0.070	-0.070
		$V_{y_{max}}$	0.066	0.066	0.066
		$V_{z_{min}}$	-0.063	-0.063	-0.063
		$V_{z_{max}}$	0.068	0.068	0.068
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.02
		$M_{y_{max}}$	0.02	0.01	0.02
		$M_{z_{min}}$	-0.02	-0.01	-0.02
		$M_{z_{max}}$	0.02	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N22/N26	Rolled steel	N <sub>min</sub>	-6.528	-6.503	-6.479
		N <sub>max</sub>	5.713	5.731	5.749
		Vy <sub>min</sub>	-0.049	-0.049	-0.049
		Vy <sub>max</sub>	0.053	0.053	0.053
		Vz <sub>min</sub>	-0.055	-0.055	-0.055
		Vz <sub>max</sub>	0.051	0.051	0.051
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.01	-0.01
		My <sub>max</sub>	0.02	0.01	0.01
		Mz <sub>min</sub>	-0.02	-0.01	-0.01
		Mz <sub>max</sub>	0.02	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N26/N30	Rolled steel	N <sub>min</sub>	-4.675	-4.651	-4.627
		N <sub>max</sub>	4.069	4.087	4.105
		Vy <sub>min</sub>	-0.039	-0.039	-0.039
		Vy <sub>max</sub>	0.037	0.037	0.037
		Vz <sub>min</sub>	-0.035	-0.035	-0.035
		Vz <sub>max</sub>	0.038	0.038	0.038
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.01	-0.01	-0.01
		My <sub>max</sub>	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$M_{z_{min}}$	-0.01	-0.01	-0.01
		$M_{z_{max}}$	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N30/N34	Rolled steel	$N_{min}$	-2.820	-2.796	-2.772
		$N_{max}$	2.423	2.441	2.459
		$V_{y_{min}}$	-0.021	-0.021	-0.021
		$V_{y_{max}}$	0.021	0.021	0.021
		$V_{z_{min}}$	-0.025	-0.025	-0.025
		$V_{z_{max}}$	0.022	0.022	0.022
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	-0.01
		$M_{y_{max}}$	0.01	0.00	0.01
		$M_{z_{min}}$	-0.01	-0.01	-0.01
		$M_{z_{max}}$	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N34/N6	Rolled steel	$N_{min}$	-1.222	-1.197	-1.173
		$N_{max}$	1.050	1.068	1.086
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.014	0.014	0.014
		$V_{z_{min}}$	-0.010	-0.010	-0.010
		$V_{z_{max}}$	0.017	0.017	0.017

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	0.00
		$M_{y_{max}}$	0.01	0.00	0.00
		$M_{z_{min}}$	-0.01	0.00	0.00
		$M_{z_{max}}$	0.01	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
N1/N9	Rolled steel	$N_{min}$	-13.780	-13.759	-13.738
		$N_{max}$	12.453	12.469	12.484
		$V_{y_{min}}$	-0.054	-0.054	-0.054
		$V_{y_{max}}$	0.042	0.042	0.042
		$V_{z_{min}}$	-0.110	-0.110	-0.110
		$V_{z_{max}}$	0.092	0.092	0.092
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.03
		$M_{y_{max}}$	0.02	0.01	0.04
		$M_{z_{min}}$	-0.01	-0.02	-0.03
		$M_{z_{max}}$	0.01	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N9/N13	Rolled steel	$N_{min}$	-11.987	-11.962	-11.938
		$N_{max}$	10.825	10.843	10.861

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$V_{y_{min}}$	-0.077	-0.077	-0.077
		$V_{y_{max}}$	0.095	0.095	0.095
		$V_{z_{min}}$	-0.083	-0.083	-0.083
		$V_{z_{max}}$	0.102	0.102	0.102
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.02	-0.03
		$M_{y_{max}}$	0.04	0.02	0.03
		$M_{z_{min}}$	-0.03	-0.02	-0.03
		$M_{z_{max}}$	0.03	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N13/N17	Rolled steel	$N_{min}$	-10.137	-10.113	-10.088
		$N_{max}$	9.143	9.161	9.179
		$V_{y_{min}}$	-0.088	-0.088	-0.088
		$V_{y_{max}}$	0.071	0.071	0.071
		$V_{z_{min}}$	-0.092	-0.092	-0.092
		$V_{z_{max}}$	0.075	0.075	0.075
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.01	-0.02
		$M_{y_{max}}$	0.03	0.01	0.03
		$M_{z_{min}}$	-0.03	-0.01	-0.02
		$M_{z_{max}}$	0.03	0.01	0.03



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N17/N21	Rolled steel	N <sub>min</sub>	-8.300	-8.276	-8.251
		N <sub>max</sub>	7.472	7.490	7.508
		Vy <sub>min</sub>	-0.061	-0.061	-0.061
		Vy <sub>max</sub>	0.075	0.075	0.075
		Vz <sub>min</sub>	-0.059	-0.059	-0.059
		Vz <sub>max</sub>	0.074	0.074	0.074
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.01	-0.02
		My <sub>max</sub>	0.03	0.01	0.02
		Mz <sub>min</sub>	-0.02	-0.01	-0.02
		Mz <sub>max</sub>	0.03	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N21/N25	Rolled steel	N <sub>min</sub>	-6.466	-6.442	-6.418
		N <sub>max</sub>	5.804	5.822	5.840
		Vy <sub>min</sub>	-0.057	-0.057	-0.057
		Vy <sub>max</sub>	0.046	0.046	0.046
		Vz <sub>min</sub>	-0.059	-0.059	-0.059
		Vz <sub>max</sub>	0.048	0.048	0.048
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.01	-0.01
		My <sub>max</sub>	0.02	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$M_{z_{min}}$	-0.02	-0.01	-0.01
		$M_{z_{max}}$	0.02	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N25/N29	Rolled steel	$N_{min}$	-4.632	-4.608	-4.583
		$N_{max}$	4.135	4.153	4.171
		$V_{y_{min}}$	-0.034	-0.034	-0.034
		$V_{y_{max}}$	0.043	0.043	0.043
		$V_{z_{min}}$	-0.031	-0.031	-0.031
		$V_{z_{max}}$	0.039	0.039	0.039
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	-0.01	-0.01
		$M_{y_{max}}$	0.02	0.01	0.01
		$M_{z_{min}}$	-0.01	-0.01	-0.01
		$M_{z_{max}}$	0.02	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N29/N33	Rolled steel	$N_{min}$	-2.800	-2.775	-2.751
		$N_{max}$	2.469	2.486	2.504
		$V_{y_{min}}$	-0.024	-0.024	-0.024
		$V_{y_{max}}$	0.018	0.018	0.018
		$V_{z_{min}}$	-0.020	-0.020	-0.020
		$V_{z_{max}}$	0.016	0.016	0.016

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	0.00
		$M_{y_{max}}$	0.01	0.00	0.00
		$M_{z_{min}}$	-0.01	0.00	0.00
		$M_{z_{max}}$	0.01	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N33/N5	Rolled steel	$N_{min}$	-1.225	-1.200	-1.176
		$N_{max}$	1.029	1.047	1.065
		$V_{y_{min}}$	-0.006	-0.006	-0.006
		$V_{y_{max}}$	0.013	0.013	0.013
		$V_{z_{min}}$	-0.010	-0.010	-0.010
		$V_{z_{max}}$	0.007	0.007	0.007
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
N4/N12	Rolled steel	$N_{min}$	-13.806	-13.785	-13.764
		$N_{max}$	12.475	12.491	12.507

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
		$V_{y_{min}}$	-0.030	-0.030	-0.030
		$V_{y_{max}}$	0.039	0.039	0.039
		$V_{z_{min}}$	-0.086	-0.086	-0.086
		$V_{z_{max}}$	0.095	0.095	0.095
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	-0.01	-0.04
		$M_{y_{max}}$	0.01	0.01	0.03
		$M_{z_{min}}$	-0.01	-0.02	-0.03
		$M_{z_{max}}$	0.01	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N12/N16	Rolled steel	$N_{min}$	-11.992	-11.968	-11.943
		$N_{max}$	10.831	10.849	10.867
		$V_{y_{min}}$	-0.094	-0.094	-0.094
		$V_{y_{max}}$	0.076	0.076	0.076
		$V_{z_{min}}$	-0.098	-0.098	-0.098
		$V_{z_{max}}$	0.079	0.079	0.079
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.04	-0.02	-0.03
		$M_{y_{max}}$	0.03	0.02	0.03
		$M_{z_{min}}$	-0.03	-0.02	-0.03
		$M_{z_{max}}$	0.03	0.02	0.03

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N16/N20	Rolled steel	N <sub>min</sub>	-10.140	-10.115	-10.091
		N <sub>max</sub>	9.146	9.164	9.182
		Vy <sub>min</sub>	-0.071	-0.071	-0.071
		Vy <sub>max</sub>	0.088	0.088	0.088
		Vz <sub>min</sub>	-0.074	-0.074	-0.074
		Vz <sub>max</sub>	0.091	0.091	0.091
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.01	-0.03
		My <sub>max</sub>	0.03	0.01	0.02
		Mz <sub>min</sub>	-0.03	-0.01	-0.03
		Mz <sub>max</sub>	0.03	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N20/N24	Rolled steel	N <sub>min</sub>	-8.304	-8.279	-8.255
		N <sub>max</sub>	7.476	7.494	7.512
		Vy <sub>min</sub>	-0.075	-0.075	-0.075
		Vy <sub>max</sub>	0.061	0.061	0.061
		Vz <sub>min</sub>	-0.073	-0.073	-0.073
		Vz <sub>max</sub>	0.059	0.059	0.059
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.01	-0.02
		My <sub>max</sub>	0.02	0.01	0.02
		Mz <sub>min</sub>	-0.03	-0.01	-0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$M_{z_{max}}$	0.02	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N24/N28	Rolled steel	$N_{min}$	-6.469	-6.445	-6.420
		$N_{max}$	5.806	5.824	5.842
		$V_{y_{min}}$	-0.046	-0.046	-0.046
		$V_{y_{max}}$	0.057	0.057	0.057
		$V_{z_{min}}$	-0.048	-0.048	-0.048
		$V_{z_{max}}$	0.059	0.059	0.059
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.02
		$M_{y_{max}}$	0.02	0.01	0.01
		$M_{z_{min}}$	-0.02	-0.01	-0.02
		$M_{z_{max}}$	0.02	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N28/N32	Rolled steel	$N_{min}$	-4.636	-4.612	-4.587
		$N_{max}$	4.139	4.157	4.175
		$V_{y_{min}}$	-0.042	-0.042	-0.042
		$V_{y_{max}}$	0.034	0.034	0.034
		$V_{z_{min}}$	-0.040	-0.040	-0.040
		$V_{z_{max}}$	0.031	0.031	0.031
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.01
		$M_{y_{max}}$	0.01	0.01	0.01
		$M_{z_{min}}$	-0.02	-0.01	-0.01
		$M_{z_{max}}$	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N32/N36	Rolled steel	$N_{min}$	-2.804	-2.780	-2.756
		$N_{max}$	2.471	2.489	2.507
		$V_{y_{min}}$	-0.018	-0.018	-0.018
		$V_{y_{max}}$	0.023	0.023	0.023
		$V_{z_{min}}$	-0.016	-0.016	-0.016
		$V_{z_{max}}$	0.022	0.022	0.022
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	0.00
		$M_{y_{max}}$	0.01	0.00	0.00
		$M_{z_{min}}$	-0.01	0.00	0.00
		$M_{z_{max}}$	0.01	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N36/N8	Rolled steel	$N_{min}$	-1.195	-1.170	-1.146
		$N_{max}$	1.058	1.076	1.094
		$V_{y_{min}}$	-0.006	-0.006	-0.006

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$V_{y_{max}}$	0.006	0.006	0.006
		$V_{z_{min}}$	-0.006	-0.006	-0.006
		$V_{z_{max}}$	0.006	0.006	0.006
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.250 m	0.500 m
N3/N11	Rolled steel	$N_{min}$	-13.561	-13.540	-13.519
		$N_{max}$	12.558	12.574	12.589
		$V_{y_{min}}$	-0.093	-0.093	-0.093
		$V_{y_{max}}$	0.089	0.089	0.089
		$V_{z_{min}}$	-0.068	-0.068	-0.068
		$V_{z_{max}}$	0.068	0.068	0.068
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.02	-0.01	-0.03
		$M_{z_{max}}$	0.02	0.01	0.03



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N11/N15	Rolled steel	$N_{min}$	-11.812	-11.788	-11.764
		$N_{max}$	10.934	10.952	10.970
		$V_{ymin}$	-0.090	-0.090	-0.090
		$V_{ymax}$	0.095	0.095	0.095
		$V_{zmin}$	-0.087	-0.087	-0.087
		$V_{zmax}$	0.082	0.082	0.082
		$M_{tmin}$	0.00	0.00	0.00
		$M_{tmax}$	0.00	0.00	0.00
		$M_{ymin}$	-0.03	-0.01	-0.03
		$M_{ymax}$	0.03	0.01	0.03
		$M_{zmin}$	-0.03	-0.01	-0.03
		$M_{zmax}$	0.03	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N15/N19	Rolled steel	$N_{min}$	-10.001	-9.977	-9.952
		$N_{max}$	9.248	9.266	9.284
		$V_{ymin}$	-0.083	-0.083	-0.083
		$V_{ymax}$	0.078	0.078	0.078
		$V_{zmin}$	-0.078	-0.078	-0.078
		$V_{zmax}$	0.083	0.083	0.083
		$M_{tmin}$	0.00	0.00	0.00
		$M_{tmax}$	0.00	0.00	0.00
		$M_{ymin}$	-0.03	-0.01	-0.02
		$M_{ymax}$	0.03	0.01	0.02
		$M_{zmin}$	-0.03	-0.01	-0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$M_{z_{max}}$	0.03	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N19/N23	Rolled steel	$N_{min}$	-8.191	-8.166	-8.142
		$N_{max}$	7.560	7.578	7.596
		$V_{y_{min}}$	-0.066	-0.066	-0.066
		$V_{y_{max}}$	0.070	0.070	0.070
		$V_{z_{min}}$	-0.068	-0.068	-0.068
		$V_{z_{max}}$	0.063	0.063	0.063
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.02
		$M_{y_{max}}$	0.02	0.01	0.02
		$M_{z_{min}}$	-0.02	-0.01	-0.02
		$M_{z_{max}}$	0.02	0.01	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N23/N27	Rolled steel	$N_{min}$	-6.382	-6.357	-6.333
		$N_{max}$	5.872	5.890	5.908
		$V_{y_{min}}$	-0.053	-0.053	-0.053
		$V_{y_{max}}$	0.049	0.049	0.049
		$V_{z_{min}}$	-0.051	-0.051	-0.051
		$V_{z_{max}}$	0.055	0.055	0.055
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.01	-0.01
		$M_{y_{max}}$	0.02	0.01	0.01
		$M_{z_{min}}$	-0.02	-0.01	-0.01
		$M_{z_{max}}$	0.02	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N27/N31	Rolled steel	$N_{min}$	-4.574	-4.549	-4.525
		$N_{max}$	4.187	4.205	4.223
		$V_{y_{min}}$	-0.037	-0.037	-0.037
		$V_{y_{max}}$	0.039	0.039	0.039
		$V_{z_{min}}$	-0.037	-0.037	-0.037
		$V_{z_{max}}$	0.035	0.035	0.035
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	-0.01	-0.01
		$M_{y_{max}}$	0.01	0.01	0.01
		$M_{z_{min}}$	-0.01	-0.01	-0.01
		$M_{z_{max}}$	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
N31/N35	Rolled steel	$N_{min}$	-2.763	-2.739	-2.714
		$N_{max}$	2.497	2.515	2.533
		$V_{y_{min}}$	-0.021	-0.021	-0.021

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.287 m	0.575 m
		$V_{y_{max}}$	0.021	0.021	0.021
		$V_{z_{min}}$	-0.023	-0.023	-0.023
		$V_{z_{max}}$	0.023	0.023	0.023
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	-0.01
		$M_{y_{max}}$	0.01	0.00	0.01
		$M_{z_{min}}$	-0.01	0.00	0.00
		$M_{z_{max}}$	0.01	0.01	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N35/N7	Rolled steel	$N_{min}$	-1.219	-1.195	-1.171
		$N_{max}$	1.057	1.075	1.093
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.009	0.009	0.009
		$V_{z_{min}}$	-0.010	-0.010	-0.010
		$V_{z_{max}}$	0.010	0.010	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.01	0.00	0.00
		$M_{y_{max}}$	0.01	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.01	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N9/N10	Rolled steel	N <sub>min</sub>	-0.150	-0.150	-0.150
		N <sub>max</sub>	0.159	0.159	0.159
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N11/N9	Rolled steel	N <sub>min</sub>	-0.119	-0.119	-0.119
		N <sub>max</sub>	0.150	0.150	0.150
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N11/N12	Rolled steel	N <sub>min</sub>	-0.150	-0.150	-0.150
		N <sub>max</sub>	0.157	0.157	0.157
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N12/N10	Rolled steel	N <sub>min</sub>	-0.106	-0.106	-0.106
		N <sub>max</sub>	0.133	0.133	0.133
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N13/N14	Rolled steel	$N_{min}$	-0.157	-0.157	-0.157
		$N_{max}$	0.194	0.194	0.194
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N15/N13	Rolled steel	$N_{min}$	-0.167	-0.167	-0.167
		$N_{max}$	0.178	0.178	0.178
		$V_{y_{min}}$	0.000	0.000	0.000

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N15/N16	Rolled steel	$N_{min}$	-0.153	-0.153	-0.153
		$N_{max}$	0.189	0.189	0.189
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N16/N14	Rolled steel	N <sub>min</sub>	-0.166	-0.166	-0.166
		N <sub>max</sub>	0.178	0.178	0.178
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N17/N18	Rolled steel	N <sub>min</sub>	-0.141	-0.141	-0.141
		N <sub>max</sub>	0.151	0.151	0.151
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N19/N17	Rolled steel	$N_{min}$	-0.132	-0.132	-0.132
		$N_{max}$	0.163	0.163	0.163
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N19/N20	Rolled steel	$N_{min}$	-0.141	-0.141	-0.141
		$N_{max}$	0.151	0.151	0.151
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N20/N18	Rolled steel	$N_{min}$	-0.132	-0.132	-0.132
		$N_{max}$	0.163	0.163	0.163
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N21/N22	Rolled steel	$N_{min}$	-0.107	-0.107	-0.107
		$N_{max}$	0.133	0.133	0.133
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		V <sub>z</sub> <sub>min</sub>	-0.010	0.000	0.007
		V <sub>z</sub> <sub>max</sub>	-0.007	0.000	0.010
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N23/N21	Rolled steel	N <sub>min</sub>	-0.115	-0.115	-0.115
		N <sub>max</sub>	0.123	0.123	0.123
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.010	0.000	0.007
		V <sub>z</sub> <sub>max</sub>	-0.007	0.000	0.010
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N23/N24	Rolled steel	N <sub>min</sub>	-0.107	-0.107	-0.107
		N <sub>max</sub>	0.132	0.132	0.132
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N24/N22	Rolled steel	N <sub>min</sub>	-0.115	-0.115	-0.115
		N <sub>max</sub>	0.123	0.123	0.123
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N25/N26	Rolled steel	$N_{min}$	-0.086	-0.086	-0.086
		$N_{max}$	0.092	0.092	0.092
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N27/N25	Rolled steel	$N_{min}$	-0.080	-0.080	-0.080
		$N_{max}$	0.100	0.100	0.100
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N27/N28	Rolled steel	$N_{min}$	-0.086	-0.086	-0.086
		$N_{max}$	0.092	0.092	0.092
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N28/N26	Rolled steel	$N_{min}$	-0.080	-0.080	-0.080
		$N_{max}$	0.099	0.099	0.099
		$V_{y_{min}}$	0.000	0.000	0.000

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N29/N30	Rolled steel	$N_{min}$	-0.048	-0.048	-0.048
		$N_{max}$	0.060	0.060	0.060
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N31/N29	Rolled steel	N <sub>min</sub>	-0.058	-0.058	-0.058
		N <sub>max</sub>	0.062	0.062	0.062
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N31/N32	Rolled steel	N <sub>min</sub>	-0.048	-0.048	-0.048
		N <sub>max</sub>	0.061	0.061	0.061
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	0.000	0.007
		Vz <sub>max</sub>	-0.007	0.000	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N32/N30	Rolled steel	$N_{min}$	-0.058	-0.058	-0.058
		$N_{max}$	0.061	0.061	0.061
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N33/N34	Rolled steel	$N_{min}$	-0.027	-0.027	-0.027
		$N_{max}$	0.037	0.037	0.037
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N35/N33	Rolled steel	$N_{min}$	-0.023	-0.023	-0.023
		$N_{max}$	0.036	0.036	0.036
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N35/N36	Rolled steel	$N_{min}$	-0.030	-0.030	-0.030
		$N_{max}$	0.030	0.030	0.030
		$V_{y_{min}}$	0.000	0.000	0.000

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.275 m	0.550 m
N36/N34	Rolled steel	$N_{min}$	-0.022	-0.022	-0.022
		$N_{max}$	0.029	0.029	0.029
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	0.000	0.007
		$V_{z_{max}}$	-0.007	0.000	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
N4/N10	Rolled steel	N <sub>min</sub>	-1.521	-1.517	-1.512	-1.508	-1.503
		N <sub>max</sub>	1.523	1.526	1.529	1.533	1.536
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N10/N16	Rolled steel	N <sub>min</sub>	-1.501	-1.496	-1.491	-1.485	-1.480
		N <sub>max</sub>	1.407	1.411	1.415	1.419	1.423
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N16/N18	Rolled steel	N <sub>min</sub>	-1.654	-1.649	-1.644	-1.639	-1.633
		N <sub>max</sub>	1.650	1.654	1.657	1.661	1.665
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N18/N24	Rolled steel	N <sub>min</sub>	-1.522	-1.517	-1.512	-1.507	-1.502
		N <sub>max</sub>	1.436	1.440	1.444	1.448	1.451
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N24/N26	Rolled steel	$N_{min}$	-1.615	-1.610	-1.604	-1.599	-1.594
		$N_{max}$	1.620	1.624	1.628	1.632	1.636
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N26/N32	Rolled steel	$N_{min}$	-1.550	-1.545	-1.540	-1.535	-1.530
		$N_{max}$	1.475	1.479	1.482	1.486	1.490
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N32/N34	Rolled steel	N <sub>min</sub>	-1.575	-1.570	-1.565	-1.560	-1.556
		N <sub>max</sub>	1.593	1.597	1.601	1.604	1.610
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N34/N8	Rolled steel	N <sub>min</sub>	-1.570	-1.564	-1.560	-1.556	-1.552
		N <sub>max</sub>	1.514	1.517	1.522	1.527	1.532
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
N2/N9	Rolled steel	N <sub>min</sub>	-1.424	-1.420	-1.415	-1.411	-1.406
		N <sub>max</sub>	1.383	1.386	1.389	1.393	1.396
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N9/N14	Rolled steel	N <sub>min</sub>	-1.684	-1.679	-1.674	-1.668	-1.663
		N <sub>max</sub>	1.630	1.634	1.638	1.642	1.646
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N14/N17	Rolled steel	N <sub>min</sub>	-1.488	-1.483	-1.478	-1.473	-1.467
		N <sub>max</sub>	1.438	1.442	1.446	1.450	1.453
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N17/N22	Rolled steel	$N_{min}$	-1.658	-1.652	-1.647	-1.642	-1.637
		$N_{max}$	1.612	1.616	1.620	1.624	1.628
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N22/N25	Rolled steel	$N_{min}$	-1.516	-1.510	-1.505	-1.500	-1.495
		$N_{max}$	1.476	1.480	1.484	1.488	1.492
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N25/N30	Rolled steel	$N_{min}$	-1.615	-1.610	-1.605	-1.599	-1.595
		$N_{max}$	1.581	1.585	1.589	1.593	1.597
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N30/N33	Rolled steel	N <sub>min</sub>	-1.551	-1.546	-1.541	-1.535	-1.532
		N <sub>max</sub>	1.523	1.527	1.531	1.535	1.540
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N33/N6	Rolled steel	N <sub>min</sub>	-1.561	-1.556	-1.550	-1.546	-1.542
		N <sub>max</sub>	1.537	1.541	1.545	1.550	1.555
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
N3/N12	Rolled steel	N <sub>min</sub>	-1.439	-1.434	-1.430	-1.425	-1.420
		N <sub>max</sub>	1.406	1.409	1.412	1.416	1.420
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N12/N15	Rolled steel	N <sub>min</sub>	-1.680	-1.675	-1.670	-1.665	-1.659
		N <sub>max</sub>	1.628	1.632	1.636	1.640	1.644
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N15/N20	Rolled steel	$N_{min}$	-1.488	-1.483	-1.477	-1.472	-1.467
		$N_{max}$	1.438	1.442	1.445	1.449	1.453
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N20/N23	Rolled steel	$N_{min}$	-1.657	-1.652	-1.646	-1.641	-1.636
		$N_{max}$	1.612	1.615	1.619	1.623	1.627
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N23/N28	Rolled steel	N <sub>min</sub>	-1.515	-1.510	-1.505	-1.499	-1.494
		N <sub>max</sub>	1.476	1.479	1.483	1.487	1.491
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N28/N31	Rolled steel	N <sub>min</sub>	-1.615	-1.610	-1.605	-1.599	-1.595
		N <sub>max</sub>	1.581	1.585	1.589	1.593	1.595
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N31/N36	Rolled steel	N <sub>min</sub>	-1.549	-1.544	-1.538	-1.533	-1.529
		N <sub>max</sub>	1.521	1.525	1.529	1.533	1.537
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N36/N7	Rolled steel	N <sub>min</sub>	-1.569	-1.564	-1.559	-1.554	-1.550
		N <sub>max</sub>	1.547	1.551	1.555	1.560	1.565
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
N1/N11	Rolled steel	N <sub>min</sub>	-1.598	-1.593	-1.589	-1.584	-1.580
		N <sub>max</sub>	1.517	1.520	1.524	1.527	1.531
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.186 m	0.372 m	0.557 m	0.743 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N11/N13	Rolled steel	$N_{min}$	-1.454	-1.448	-1.443	-1.438	-1.433
		$N_{max}$	1.441	1.445	1.449	1.452	1.456
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.007
		$V_{z_{max}}$	-0.007	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N13/N19	Rolled steel	$N_{min}$	-1.700	-1.695	-1.689	-1.684	-1.679
		$N_{max}$	1.604	1.608	1.612	1.615	1.619
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N19/N21	Rolled steel	N <sub>min</sub>	-1.480	-1.475	-1.470	-1.464	-1.459
		N <sub>max</sub>	1.476	1.480	1.483	1.487	1.491
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N21/N27	Rolled steel	N <sub>min</sub>	-1.659	-1.653	-1.648	-1.643	-1.638
		N <sub>max</sub>	1.574	1.578	1.582	1.586	1.590
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N27/N29	Rolled steel	N <sub>min</sub>	-1.508	-1.502	-1.497	-1.492	-1.488
		N <sub>max</sub>	1.515	1.519	1.523	1.527	1.530
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N29/N35	Rolled steel	N <sub>min</sub>	-1.619	-1.614	-1.609	-1.602	-1.599
		N <sub>max</sub>	1.546	1.550	1.554	1.558	1.563
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
N35/N5	Rolled steel	N <sub>min</sub>	-1.537	-1.532	-1.527	-1.521	-1.517
		N <sub>max</sub>	1.551	1.555	1.559	1.563	1.568
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.007
		Vz <sub>max</sub>	-0.007	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.199 m	0.398 m	0.597 m	0.796 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.197 m	0.395 m	0.592 m	0.790 m	0.987 m	1.184 m
N39/N7 9	Rolled steel	$N_{min}$	-0.564	-0.560	-0.557	-0.553	-0.550	-0.546	-0.543
		$N_{max}$	0.524	0.527	0.530	0.532	0.535	0.537	0.540
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.019	-0.012	-0.006	0.000	0.005	0.009	0.014
		$V_{z_{max}}$	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.019
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
N79/N9 9	Rolled steel	$N_{min}$	-0.508	-0.504	-0.501	-0.497	-0.494	-0.490	-0.486

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
		N <sub>max</sub>	0.471	0.473	0.476	0.478	0.481	0.484	0.486
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.005	0.009	0.014
		Vz <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.190 m	0.380 m	0.571 m	0.761 m	0.951 m	1.141 m
N99/N8 1	Rolled steel	N <sub>min</sub>	-0.459	-0.456	-0.452	-0.448	-0.446	-0.444	-0.441
		N <sub>max</sub>	0.440	0.443	0.446	0.448	0.452	0.455	0.459
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.004	0.009	0.013
		Vz <sub>max</sub>	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00



Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.190 m	0.380 m	0.571 m	0.761 m	0.951 m	1.141 m
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
N81/N10 1	Rolled steel	$N_{min}$	-0.481	-0.477	-0.474	-0.470	-0.467	-0.464	-0.461
		$N_{max}$	0.453	0.456	0.459	0.461	0.464	0.467	0.470
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.017	-0.012	-0.006	0.000	0.004	0.009	0.013
		$V_{z_{max}}$	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.017
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
N101/N8 3	Rolled steel	$N_{min}$	-0.511	-0.508	-0.504	-0.501	-0.497	-0.494	-0.491
		$N_{max}$	0.481	0.484	0.486	0.489	0.491	0.494	0.498
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
		V <sub>zmin</sub>	-0.017	-0.011	-0.006	0.000	0.004	0.008	0.013
		V <sub>zmax</sub>	-0.013	-0.008	-0.004	0.000	0.006	0.011	0.017
		M <sub>tmin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>tmax</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>ymin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y<sub>max</sub></sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>zmin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>z<sub>max</sub></sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.180 m	0.359 m	0.539 m	0.719 m	0.898 m	1.078 m
N83/N10 3	Rolled steel	N <sub>min</sub>	-0.527	-0.523	-0.520	-0.516	-0.513	-0.510	-0.507
		N <sub>max</sub>	0.498	0.501	0.504	0.506	0.509	0.510	0.515
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		V <sub>ymax</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		V <sub>zmin</sub>	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		V <sub>zmax</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		M <sub>tmin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>tmax</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>ymin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y<sub>max</sub></sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>zmin</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>z<sub>max</sub></sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
N103/N85	Rolled steel	N <sub>min</sub>	-0.542	-0.539	-0.535	-0.532	-0.528	-0.525	-0.522
		N <sub>max</sub>	0.514	0.517	0.519	0.522	0.525	0.528	0.531
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		Vz <sub>max</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.173 m	0.346 m	0.518 m	0.691 m	0.864 m	1.037 m
N85/N105	Rolled steel	N <sub>min</sub>	-0.562	-0.559	-0.555	-0.552	-0.548	-0.546	-0.542
		N <sub>max</sub>	0.534	0.536	0.539	0.542	0.544	0.546	0.551
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.016	-0.010	-0.005	0.000	0.004	0.008	0.012
		Vz <sub>max</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.010	0.016
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.173 m	0.346 m	0.518 m	0.691 m	0.864 m	1.037 m
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
N105/N87	Rolled steel	$N_{min}$	-0.584	-0.580	-0.577	-0.573	-0.570	-0.567	-0.564
		$N_{max}$	0.555	0.558	0.560	0.563	0.566	0.567	0.572
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.015	-0.010	-0.005	0.000	0.004	0.007	0.011
		$V_{z_{max}}$	-0.011	-0.007	-0.004	0.000	0.005	0.010	0.015
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
N87/N107	Rolled steel	$N_{min}$	-0.607	-0.602	-0.597	-0.591	-0.588
		$N_{max}$	0.579	0.583	0.587	0.591	0.596
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.015	-0.007	0.000	0.005	0.011

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
		V <sub>z</sub> <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.015
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.244 m	0.488 m	0.732 m	0.976 m
N107/N89	Rolled steel	N <sub>min</sub>	-0.635	-0.630	-0.625	-0.619	-0.616
		N <sub>max</sub>	0.607	0.611	0.615	0.619	0.624
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.011
		V <sub>z</sub> <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.014
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
N89/N109	Rolled steel	N <sub>min</sub>	-0.660	-0.655	-0.650	-0.644	-0.641

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
		N <sub>max</sub>	0.632	0.636	0.640	0.644	0.649
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.014
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.234 m	0.468 m	0.702 m	0.937 m
N109/N91	Rolled steel	N <sub>min</sub>	-0.675	-0.670	-0.665	-0.660	-0.655
		N <sub>max</sub>	0.645	0.649	0.653	0.657	0.661
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.007	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.234 m	0.468 m	0.702 m	0.937 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
N91/N111	Rolled steel	N <sub>min</sub>	-0.704	-0.699	-0.693	-0.688	-0.684
		N <sub>max</sub>	0.676	0.680	0.684	0.688	0.693
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.006	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.006	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
N111/N93	Rolled steel	N <sub>min</sub>	-0.728	-0.722	-0.717	-0.712	-0.708
		N <sub>max</sub>	0.701	0.705	0.709	0.712	0.718
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.005	0.009
		Vz <sub>max</sub>	-0.009	-0.005	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
N93/N113	Rolled steel	$N_{min}$	-0.769	-0.764	-0.758	-0.753	-0.749
		$N_{max}$	0.742	0.746	0.750	0.753	0.759
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.012	-0.006	0.000	0.004	0.009
		$V_{z_{max}}$	-0.009	-0.004	0.000	0.006	0.012
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
N113/N95	Rolled steel	$N_{min}$	-0.832	-0.827	-0.822	-0.817	-0.813
		$N_{max}$	0.810	0.814	0.817	0.822	0.827
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.012	-0.006	0.000	0.004	0.009
		V <sub>z</sub> <sub>max</sub>	-0.009	-0.004	0.000	0.006	0.012
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.211 m	0.421 m	0.632 m	0.843 m
N95/N115	Rolled steel	N <sub>min</sub>	-0.883	-0.877	-0.871	-0.868	-0.864
		N <sub>max</sub>	0.863	0.866	0.871	0.875	0.881
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.011	-0.006	0.000	0.004	0.008
		V <sub>z</sub> <sub>max</sub>	-0.008	-0.004	0.000	0.006	0.011
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
N115/N97	Rolled steel	N <sub>min</sub>	-0.964	-0.959	-0.954	-0.947	-0.944
		N <sub>max</sub>	0.935	0.939	0.943	0.947	0.952
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.011	-0.005	0.000	0.004	0.008
		Vz <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.201 m	0.402 m	0.603 m	0.804 m
N97/N3	Rolled steel	N <sub>min</sub>	-0.938	-0.932	-0.927	-0.922	-0.918
		N <sub>max</sub>	0.910	0.914	0.918	0.922	0.927
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.008
		Vz <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.201 m	0.402 m	0.603 m	0.804 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.197 m	0.395 m	0.592 m	0.790 m	0.987 m	1.184 m
N37/N60	Rolled steel	N <sub>min</sub>	-0.557	-0.553	-0.550	-0.546	-0.543	-0.539	-0.536
		N <sub>max</sub>	0.532	0.535	0.537	0.540	0.543	0.545	0.548
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.019	-0.012	-0.006	0.000	0.005	0.009	0.014
		Vz <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.019
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
N60/N80	Rolled steel	N <sub>min</sub>	-0.515	-0.511	-0.508	-0.504	-0.501	-0.497	-0.494
		N <sub>max</sub>	0.464	0.467	0.469	0.472	0.475	0.477	0.480
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.005	0.009	0.014

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
		Vz <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.190 m	0.380 m	0.571 m	0.761 m	0.951 m	1.141 m
N80/N6 2	Rolled steel	N <sub>min</sub>	-0.453	-0.450	-0.446	-0.443	-0.440	-0.438	-0.435
		N <sub>max</sub>	0.447	0.450	0.452	0.455	0.458	0.462	0.465
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.004	0.009	0.013
		Vz <sub>max</sub>	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
N62/N8 2	Rolled steel	N <sub>min</sub>	-0.488	-0.484	-0.481	-0.477	-0.474	-0.471	-0.468
		N <sub>max</sub>	0.447	0.450	0.452	0.455	0.458	0.461	0.464
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.017	-0.012	-0.006	0.000	0.004	0.009	0.013
		Vz <sub>max</sub>	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.017
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
N82/N6 4	Rolled steel	N <sub>min</sub>	-0.505	-0.501	-0.498	-0.494	-0.491	-0.487	-0.485
		N <sub>max</sub>	0.488	0.491	0.493	0.496	0.499	0.501	0.505
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.017	-0.011	-0.006	0.000	0.004	0.008	0.013
		Vz <sub>max</sub>	-0.013	-0.008	-0.004	0.000	0.006	0.011	0.017
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.180 m	0.359 m	0.539 m	0.719 m	0.898 m	1.078 m
N64/N8 4	Rolled steel	$N_{min}$	-0.534	-0.531	-0.527	-0.524	-0.520	-0.518	-0.514
		$N_{max}$	0.492	0.494	0.497	0.499	0.502	0.504	0.508
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
N84/N6 6	Rolled steel	$N_{min}$	-0.535	-0.532	-0.528	-0.525	-0.521	-0.518	-0.515
		$N_{max}$	0.522	0.524	0.527	0.530	0.532	0.535	0.539
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.173 m	0.346 m	0.518 m	0.691 m	0.864 m	1.037 m
N66/N86	Rolled steel	$N_{min}$	-0.570	-0.567	-0.563	-0.560	-0.556	-0.554	-0.550
		$N_{max}$	0.527	0.529	0.532	0.534	0.537	0.539	0.543
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.010	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.010	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
N86/N68	Rolled steel	N <sub>min</sub>	-0.576	-0.573	-0.569	-0.566	-0.562	-0.560	-0.556
		N <sub>max</sub>	0.563	0.566	0.569	0.571	0.574	0.576	0.580
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.015	-0.010	-0.005	0.000	0.004	0.007	0.011
		Vz <sub>max</sub>	-0.011	-0.007	-0.004	0.000	0.005	0.010	0.015
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
N68/N88	Rolled steel	N <sub>min</sub>	-0.616	-0.611	-0.606	-0.600	-0.596
		N <sub>max</sub>	0.571	0.575	0.579	0.583	0.588
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.015	-0.007	0.000	0.005	0.011
		Vz <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.015
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.244 m	0.488 m	0.732 m	0.976 m
N88/N70	Rolled steel	N <sub>min</sub>	-0.627	-0.622	-0.617	-0.611	-0.607
		N <sub>max</sub>	0.616	0.620	0.624	0.628	0.633
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.011
		V <sub>z</sub> <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.014
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
N70/N90	Rolled steel	$N_{min}$	-0.670	-0.664	-0.659	-0.653	-0.650
		$N_{max}$	0.623	0.627	0.631	0.635	0.640
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.014	-0.007	0.000	0.005	0.010

Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
		V <sub>z</sub> <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.014
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.234 m	0.468 m	0.702 m	0.937 m
N90/N72	Rolled steel	N <sub>min</sub>	-0.667	-0.662	-0.657	-0.652	-0.647
		N <sub>max</sub>	0.655	0.659	0.663	0.667	0.672
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.013	-0.007	0.000	0.005	0.010
		V <sub>z</sub> <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.013
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
N72/N92	Rolled steel	N <sub>min</sub>	-0.715	-0.710	-0.704	-0.699	-0.695

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
		N <sub>max</sub>	0.668	0.672	0.675	0.680	0.685
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.006	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.006	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
N92/N74	Rolled steel	N <sub>min</sub>	-0.717	-0.711	-0.706	-0.702	-0.697
		N <sub>max</sub>	0.710	0.714	0.718	0.721	0.727
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.005	0.009
		Vz <sub>max</sub>	-0.009	-0.005	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
N74/N94	Rolled steel	N <sub>min</sub>	-0.779	-0.774	-0.768	-0.763	-0.759
		N <sub>max</sub>	0.731	0.735	0.739	0.743	0.748
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.004	0.009
		Vz <sub>max</sub>	-0.009	-0.004	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
N94/N76	Rolled steel	N <sub>min</sub>	-0.825	-0.820	-0.815	-0.810	-0.806
		N <sub>max</sub>	0.826	0.830	0.833	0.838	0.843
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.004	0.009
		Vz <sub>max</sub>	-0.009	-0.004	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.211 m	0.421 m	0.632 m	0.843 m
N76/N96	Rolled steel	$N_{min}$	-0.897	-0.892	-0.885	-0.882	-0.878
		$N_{max}$	0.853	0.857	0.861	0.866	0.871
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.011	-0.006	0.000	0.004	0.008
		$V_{z_{max}}$	-0.008	-0.004	0.000	0.006	0.011
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
N96/N78	Rolled steel	$N_{min}$	-0.937	-0.931	-0.926	-0.920	-0.917
		$N_{max}$	0.933	0.937	0.941	0.946	0.950
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.011	-0.005	0.000	0.004	0.008
		V <sub>z</sub> <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.011
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.201 m	0.402 m	0.603 m	0.804 m
N78/N4	Rolled steel	N <sub>min</sub>	-0.974	-0.969	-0.964	-0.959	-0.954
		N <sub>max</sub>	0.914	0.918	0.922	0.926	0.930
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.008
		V <sub>z</sub> <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.010
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.197 m	0.395 m	0.592 m	0.790 m	0.987 m	1.184 m
N38/N4 1	Rolled steel	N <sub>min</sub>	-0.564	-0.561	-0.557	-0.554	-0.550	-0.547	-0.543
		N <sub>max</sub>	0.525	0.527	0.530	0.533	0.535	0.538	0.540
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.019	-0.012	-0.006	0.000	0.005	0.009	0.014
		Vz <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.019
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
N41/N6 1	Rolled steel	N <sub>min</sub>	-0.508	-0.505	-0.501	-0.498	-0.494	-0.491	-0.487
		N <sub>max</sub>	0.471	0.474	0.476	0.479	0.482	0.484	0.487
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.005	0.009	0.014
		Vz <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
		$M_{y_{max}}$	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.190 m	0.380 m	0.571 m	0.761 m	0.951 m	1.141 m
N61/N4 3	Rolled steel	$N_{min}$	-0.460	-0.456	-0.453	-0.449	-0.447	-0.444	-0.441
		$N_{max}$	0.441	0.443	0.446	0.449	0.452	0.456	0.459
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.018	-0.012	-0.006	0.000	0.004	0.009	0.013
		$V_{z_{max}}$	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.018
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
N43/N6 3	Rolled steel	$N_{min}$	-0.481	-0.478	-0.474	-0.471	-0.467	-0.464	-0.462
		$N_{max}$	0.454	0.456	0.459	0.462	0.464	0.467	0.471
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000



Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.017	-0.012	-0.006	0.000	0.004	0.009	0.013
		$V_{z_{max}}$	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.017
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
N63/N45	Rolled steel	$N_{min}$	-0.512	-0.508	-0.505	-0.501	-0.498	-0.494	-0.492
		$N_{max}$	0.482	0.484	0.487	0.489	0.492	0.494	0.498
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.017	-0.011	-0.006	0.000	0.004	0.008	0.013
		$V_{z_{max}}$	-0.013	-0.008	-0.004	0.000	0.006	0.011	0.017
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.180 m	0.359 m	0.539 m	0.719 m	0.898 m	1.078 m
N45/N6 5	Rolled steel	N <sub>min</sub>	-0.527	-0.524	-0.520	-0.517	-0.513	-0.511	-0.507
		N <sub>max</sub>	0.499	0.502	0.504	0.507	0.509	0.511	0.516
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		Vz <sub>max</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
N65/N4 7	Rolled steel	N <sub>min</sub>	-0.543	-0.539	-0.536	-0.532	-0.529	-0.525	-0.523
		N <sub>max</sub>	0.515	0.517	0.520	0.523	0.525	0.528	0.532
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		Vz <sub>max</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.173 m	0.346 m	0.518 m	0.691 m	0.864 m	1.037 m
N47/N6 7	Rolled steel	$N_{min}$	-0.563	-0.559	-0.556	-0.552	-0.549	-0.546	-0.543
		$N_{max}$	0.534	0.537	0.540	0.542	0.545	0.546	0.551
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.010	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.010	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
N67/N4 9	Rolled steel	$N_{min}$	-0.584	-0.581	-0.577	-0.574	-0.570	-0.568	-0.564
		$N_{max}$	0.556	0.558	0.561	0.563	0.566	0.568	0.572

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.015	-0.010	-0.005	0.000	0.004	0.007	0.011
		Vz <sub>max</sub>	-0.011	-0.007	-0.004	0.000	0.005	0.010	0.015
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
N49/N69	Rolled steel	N <sub>min</sub>	-0.608	-0.603	-0.598	-0.592	-0.588
		N <sub>max</sub>	0.580	0.584	0.587	0.592	0.596
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.015	-0.007	0.000	0.005	0.011
		Vz <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.015
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.244 m	0.488 m	0.732 m	0.976 m
N69/N51	Rolled steel	N <sub>min</sub>	-0.636	-0.631	-0.625	-0.620	-0.616
		N <sub>max</sub>	0.608	0.612	0.616	0.620	0.625
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.011
		Vz <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.014
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
N51/N71	Rolled steel	N <sub>min</sub>	-0.661	-0.656	-0.650	-0.645	-0.641
		N <sub>max</sub>	0.632	0.636	0.640	0.645	0.649
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.014
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.234 m	0.468 m	0.702 m	0.937 m
N71/N53	Rolled steel	N <sub>min</sub>	-0.676	-0.671	-0.666	-0.661	-0.656
		N <sub>max</sub>	0.646	0.650	0.653	0.657	0.662
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>ymax</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>zmin</sub>	-0.013	-0.007	0.000	0.005	0.010
		V <sub>zmax</sub>	-0.010	-0.005	0.000	0.007	0.013
		M <sub>tmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>tmax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmax</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
N53/N73	Rolled steel	N <sub>min</sub>	-0.705	-0.700	-0.694	-0.689	-0.685
		N <sub>max</sub>	0.677	0.681	0.685	0.689	0.694
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.006	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.006	0.013

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
N73/N55	Rolled steel	N <sub>min</sub>	-0.728	-0.723	-0.717	-0.713	-0.708
		N <sub>max</sub>	0.702	0.705	0.709	0.713	0.719
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.005	0.009
		Vz <sub>max</sub>	-0.009	-0.005	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
N55/N75	Rolled steel	N <sub>min</sub>	-0.770	-0.764	-0.759	-0.754	-0.750
		N <sub>max</sub>	0.743	0.747	0.750	0.754	0.760

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>ymax</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>zmin</sub>	-0.012	-0.006	0.000	0.004	0.009
		V <sub>zmax</sub>	-0.009	-0.004	0.000	0.006	0.012
		M <sub>tmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>tmax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmax</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
N75/N57	Rolled steel	N <sub>min</sub>	-0.835	-0.829	-0.824	-0.820	-0.816
		N <sub>max</sub>	0.812	0.816	0.820	0.824	0.830
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>ymax</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>zmin</sub>	-0.012	-0.006	0.000	0.004	0.009
		V <sub>zmax</sub>	-0.009	-0.004	0.000	0.006	0.012
		M <sub>tmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>tmax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>ymax</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmin</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>zmax</sub>	0.00	0.00	0.00	0.00	0.00



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.211 m	0.421 m	0.632 m	0.843 m
N57/N77	Rolled steel	N <sub>min</sub>	-0.883	-0.878	-0.872	-0.868	-0.864
		N <sub>max</sub>	0.863	0.867	0.872	0.876	0.882
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.011	-0.006	0.000	0.004	0.008
		Vz <sub>max</sub>	-0.008	-0.004	0.000	0.006	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
N77/N59	Rolled steel	N <sub>min</sub>	-0.959	-0.954	-0.948	-0.943	-0.939
		N <sub>max</sub>	0.931	0.935	0.938	0.943	0.947
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.011	-0.005	0.000	0.004	0.008
		Vz <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.201 m	0.402 m	0.603 m	0.804 m
N59/N2	Rolled steel	$N_{min}$	-0.964	-0.959	-0.953	-0.948	-0.943
		$N_{max}$	0.930	0.934	0.938	0.942	0.946
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.010	-0.005	0.000	0.004	0.008
		$V_{z_{max}}$	-0.008	-0.004	0.000	0.005	0.010
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.197 m	0.395 m	0.592 m	0.790 m	0.987 m	1.184 m
N40/N9 8	Rolled steel	$N_{min}$	-0.571	-0.568	-0.564	-0.561	-0.557	-0.554	-0.550
		$N_{max}$	0.517	0.520	0.522	0.525	0.527	0.530	0.533
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.019	-0.012	-0.006	0.000	0.005	0.009	0.014

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.197 m	0.395 m	0.592 m	0.790 m	0.987 m	1.184 m
		V <sub>z</sub> <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.019
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.194 m	0.388 m	0.581 m	0.775 m	0.969 m	1.163 m
N98/N4 2	Rolled steel	N <sub>min</sub>	-0.501	-0.498	-0.494	-0.491	-0.487	-0.484	-0.480
		N <sub>max</sub>	0.478	0.480	0.483	0.485	0.488	0.491	0.493
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.005	0.009	0.014
		V <sub>z</sub> <sub>max</sub>	-0.014	-0.009	-0.005	0.000	0.006	0.012	0.018
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.190 m	0.380 m	0.571 m	0.761 m	0.951 m	1.141 m
N42/N100	Rolled steel	N <sub>min</sub>	-0.466	-0.462	-0.459	-0.455	-0.452	-0.450	-0.447
		N <sub>max</sub>	0.434	0.437	0.439	0.442	0.445	0.449	0.452
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.018	-0.012	-0.006	0.000	0.004	0.009	0.013
		Vz <sub>max</sub>	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.018
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.01	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
N100/N44	Rolled steel	N <sub>min</sub>	-0.475	-0.471	-0.468	-0.464	-0.461	-0.457	-0.455
		N <sub>max</sub>	0.460	0.463	0.465	0.468	0.470	0.473	0.477
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.017	-0.012	-0.006	0.000	0.004	0.009	0.013
		Vz <sub>max</sub>	-0.013	-0.009	-0.004	0.000	0.006	0.012	0.017
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.187 m	0.373 m	0.560 m	0.747 m	0.933 m	1.120 m
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.183 m	0.366 m	0.550 m	0.733 m	0.916 m	1.099 m
N44/N102	Rolled steel	$N_{min}$	-0.518	-0.515	-0.511	-0.508	-0.504	-0.501	-0.498
		$N_{max}$	0.474	0.477	0.480	0.482	0.485	0.487	0.491
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.017	-0.011	-0.006	0.000	0.004	0.008	0.013
		$V_{z_{max}}$	-0.013	-0.008	-0.004	0.000	0.006	0.011	0.017
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.180 m	0.359 m	0.539 m	0.719 m	0.898 m	1.078 m
N102/N46	Rolled steel	$N_{min}$	-0.520	-0.516	-0.513	-0.509	-0.506	-0.503	-0.500
		$N_{max}$	0.506	0.508	0.511	0.513	0.516	0.518	0.522
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.180 m	0.359 m	0.539 m	0.719 m	0.898 m	1.078 m
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.176 m	0.352 m	0.529 m	0.705 m	0.881 m	1.057 m
N46/N104	Rolled steel	$N_{min}$	-0.550	-0.546	-0.543	-0.539	-0.535	-0.532	-0.530
		$N_{max}$	0.507	0.510	0.512	0.515	0.517	0.520	0.524
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.016	-0.011	-0.005	0.000	0.004	0.008	0.012
		$V_{z_{max}}$	-0.012	-0.008	-0.004	0.000	0.005	0.011	0.016
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.173 m	0.346 m	0.518 m	0.691 m	0.864 m	1.037 m
N104/N48	Rolled steel	N <sub>min</sub>	-0.555	-0.551	-0.548	-0.544	-0.541	-0.538	-0.535
		N <sub>max</sub>	0.542	0.544	0.547	0.549	0.552	0.554	0.558
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.016	-0.010	-0.005	0.000	0.004	0.008	0.012
		Vz <sub>max</sub>	-0.012	-0.008	-0.004	0.000	0.005	0.010	0.016
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
N48/N106	Rolled steel	N <sub>min</sub>	-0.592	-0.588	-0.585	-0.581	-0.578	-0.575	-0.572
		N <sub>max</sub>	0.547	0.550	0.553	0.555	0.558	0.560	0.564
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.015	-0.010	-0.005	0.000	0.004	0.007	0.011
		Vz <sub>max</sub>	-0.011	-0.007	-0.004	0.000	0.005	0.010	0.015
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes									
Bar	Combination type	Force	Positions on the bar						
			0.000 m	0.169 m	0.339 m	0.508 m	0.677 m	0.847 m	1.016 m
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.249 m	0.498 m	0.747 m	0.996 m
N106/N50	Rolled steel	$N_{min}$	-0.599	-0.594	-0.589	-0.583	-0.580
		$N_{max}$	0.587	0.591	0.595	0.600	0.604
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.015	-0.007	0.000	0.005	0.011
		$V_{z_{max}}$	-0.011	-0.005	0.000	0.007	0.015
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.244 m	0.488 m	0.732 m	0.976 m
N50/N108	Rolled steel	N <sub>min</sub>	-0.644	-0.639	-0.633	-0.628	-0.624
		N <sub>max</sub>	0.599	0.602	0.606	0.611	0.615
		V <sub>ymin</sub>	0.000	0.000	0.000	0.000	0.000



Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.244 m	0.488 m	0.732 m	0.976 m
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.011
		V <sub>z</sub> <sub>max</sub>	-0.011	-0.005	0.000	0.007	0.014
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.239 m	0.478 m	0.717 m	0.956 m
N108/N52	Rolled steel	N <sub>min</sub>	-0.652	-0.646	-0.641	-0.635	-0.632
		N <sub>max</sub>	0.641	0.645	0.649	0.653	0.658
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.014	-0.007	0.000	0.005	0.010
		V <sub>z</sub> <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.014
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.234 m	0.468 m	0.702 m	0.937 m
N52/N110	Rolled steel	N <sub>min</sub>	-0.686	-0.681	-0.675	-0.670	-0.666
		N <sub>max</sub>	0.637	0.641	0.645	0.649	0.653
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.007	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.007	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
N110/N54	Rolled steel	N <sub>min</sub>	-0.696	-0.690	-0.685	-0.680	-0.676
		N <sub>max</sub>	0.687	0.691	0.695	0.699	0.704
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.013	-0.006	0.000	0.005	0.010
		Vz <sub>max</sub>	-0.010	-0.005	0.000	0.006	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.229 m	0.459 m	0.688 m	0.917 m
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.225 m	0.449 m	0.674 m	0.898 m
N54/N112	Rolled steel	N <sub>min</sub>	-0.736	-0.731	-0.725	-0.721	-0.716
		N <sub>max</sub>	0.690	0.694	0.698	0.701	0.707
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.005	0.009
		Vz <sub>max</sub>	-0.009	-0.005	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
N112/N56	Rolled steel	N <sub>min</sub>	-0.757	-0.752	-0.747	-0.741	-0.737
		N <sub>max</sub>	0.751	0.755	0.759	0.762	0.768
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.012	-0.006	0.000	0.004	0.009
		Vz <sub>max</sub>	-0.009	-0.004	0.000	0.006	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.220 m	0.440 m	0.660 m	0.879 m
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.215 m	0.431 m	0.646 m	0.861 m
N56/N114	Rolled steel	$N_{min}$	-0.848	-0.843	-0.838	-0.833	-0.829
		$N_{max}$	0.803	0.807	0.810	0.815	0.820
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000
		$V_{y_{max}}$	0.000	0.000	0.000	0.000	0.000
		$V_{z_{min}}$	-0.012	-0.006	0.000	0.004	0.009
		$V_{z_{max}}$	-0.009	-0.004	0.000	0.006	0.012
		$M_{t_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.211 m	0.421 m	0.632 m	0.843 m
N114/N58	Rolled steel	$N_{min}$	-0.874	-0.869	-0.863	-0.860	-0.856
		$N_{max}$	0.879	0.883	0.887	0.892	0.897
		$V_{y_{min}}$	0.000	0.000	0.000	0.000	0.000

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.211 m	0.421 m	0.632 m	0.843 m
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.011	-0.006	0.000	0.004	0.008
		V <sub>z</sub> <sub>max</sub>	-0.008	-0.004	0.000	0.006	0.011
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.206 m	0.413 m	0.619 m	0.825 m
N58/N116	Rolled steel	N <sub>min</sub>	-0.958	-0.953	-0.948	-0.943	-0.939
		N <sub>max</sub>	0.906	0.909	0.913	0.917	0.923
		V <sub>y</sub> <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>y</sub> <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		V <sub>z</sub> <sub>min</sub>	-0.011	-0.005	0.000	0.004	0.008
		V <sub>z</sub> <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.011
		M <sub>t</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>t</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>y</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		M <sub>z</sub> <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes							
Bar	Combination type	Force	Positions on the bar				
			0.000 m	0.201 m	0.402 m	0.603 m	0.804 m
N116/N1	Rolled steel	N <sub>min</sub>	-0.916	-0.911	-0.906	-0.900	-0.896
		N <sub>max</sub>	0.911	0.915	0.919	0.923	0.928
		Vy <sub>min</sub>	0.000	0.000	0.000	0.000	0.000
		Vy <sub>max</sub>	0.000	0.000	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.010	-0.005	0.000	0.004	0.008
		Vz <sub>max</sub>	-0.008	-0.004	0.000	0.005	0.010
		Mt <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		My <sub>max</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N40/N41	Rolled steel	N <sub>min</sub>	-30.635	-30.542	-30.448
		N <sub>max</sub>	22.503	22.572	22.641
		Vy <sub>min</sub>	-0.075	-0.075	-0.075
		Vy <sub>max</sub>	0.090	0.090	0.090
		Vz <sub>min</sub>	-0.034	-0.032	-0.030
		Vz <sub>max</sub>	0.037	0.040	0.042
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	-0.01	-0.02
		My <sub>max</sub>	0.00	0.01	0.02
		Mz <sub>min</sub>	0.00	-0.03	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.00	0.02	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N42/N43	Rolled steel	$N_{min}$	-29.431	-29.337	-29.244
		$N_{max}$	22.087	22.156	22.225
		$V_{y_{min}}$	-0.014	-0.014	-0.014
		$V_{y_{max}}$	0.014	0.014	0.014
		$V_{z_{min}}$	-0.008	-0.005	-0.003
		$V_{z_{max}}$	-0.001	0.001	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.06	-0.05
		$M_{z_{max}}$	0.06	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N43/N44	Rolled steel	$N_{min}$	-28.829	-28.736	-28.642
		$N_{max}$	21.887	21.956	22.025
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.009	-0.007	-0.004
		$V_{z_{max}}$	0.006	0.007	0.011
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N44/N45	Rolled steel	$N_{min}$	-28.205	-28.111	-28.018
		$N_{max}$	21.659	21.728	21.798
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.008	0.008	0.008
		$V_{z_{min}}$	-0.002	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N45/N46	Rolled steel	$N_{min}$	-27.558	-27.464	-27.371
		$N_{max}$	21.406	21.475	21.544
		$V_{y_{min}}$	-0.006	-0.006	-0.006



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.005	-0.002	0.000
		$V_{z_{max}}$	-0.001	0.002	0.004
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N46/N47	Rolled steel	$N_{min}$	-26.889	-26.796	-26.703
		$N_{max}$	21.130	21.199	21.268
		$V_{y_{min}}$	0.002	0.002	0.002
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N47/N48	Rolled steel	N <sub>min</sub>	-26.197	-26.104	-26.010
		N <sub>max</sub>	20.830	20.899	20.968
		Vy <sub>min</sub>	-0.003	-0.003	-0.003
		Vy <sub>max</sub>	-0.003	-0.003	-0.003
		Vz <sub>min</sub>	-0.003	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05
		Mz <sub>max</sub>	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N48/N49	Rolled steel	N <sub>min</sub>	-25.478	-25.385	-25.291
		N <sub>max</sub>	20.501	20.571	20.640
		Vy <sub>min</sub>	0.003	0.003	0.003
		Vy <sub>max</sub>	0.003	0.003	0.003
		Vz <sub>min</sub>	-0.003	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N49/N50	Rolled steel	$N_{min}$	-24.730	-24.636	-24.543
		$N_{max}$	20.142	20.211	20.281
		$V_{y_{min}}$	-0.003	-0.003	-0.003
		$V_{y_{max}}$	-0.003	-0.003	-0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N50/N51	Rolled steel	$N_{min}$	-23.948	-23.854	-23.761
		$N_{max}$	19.748	19.817	19.886
		$V_{y_{min}}$	-0.001	-0.001	-0.001
		$V_{y_{max}}$	0.007	0.007	0.007
		$V_{z_{min}}$	-0.005	-0.002	0.000
		$V_{z_{max}}$	0.000	0.002	0.005
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.06	-0.06
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N51/N52	Rolled steel	$N_{min}$	-23.126	-23.033	-22.939
		$N_{max}$	19.313	19.382	19.452
		$V_{y_{min}}$	-0.005	-0.005	-0.005
		$V_{y_{max}}$	-0.001	-0.001	-0.001
		$V_{z_{min}}$	-0.006	-0.004	-0.001
		$V_{z_{max}}$	0.002	0.004	0.007
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.06	-0.06
		$M_{z_{max}}$	0.05	0.06	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N52/N53	Rolled steel	$N_{min}$	-22.271	-22.177	-22.084
		$N_{max}$	18.845	18.914	18.983
		$V_{y_{min}}$	-0.010	-0.010	-0.010

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.017	0.017	0.017
		$V_{z_{min}}$	-0.014	-0.011	-0.009
		$V_{z_{max}}$	0.009	0.011	0.013
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.05	-0.05
		$M_{z_{max}}$	0.06	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N53/N54	Rolled steel	$N_{min}$	-21.398	-21.305	-21.212
		$N_{max}$	18.355	18.424	18.493
		$V_{y_{min}}$	-0.021	-0.021	-0.021
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.010	-0.006	-0.005
		$V_{z_{max}}$	0.004	0.006	0.009
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.04	-0.04
		$M_{z_{max}}$	0.05	0.04	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N54/N55	Rolled steel	N <sub>min</sub>	-20.478	-20.385	-20.291
		N <sub>max</sub>	17.816	17.886	17.955
		Vy <sub>min</sub>	-0.017	-0.017	-0.017
		Vy <sub>max</sub>	0.021	0.021	0.021
		Vz <sub>min</sub>	-0.012	-0.009	-0.007
		Vz <sub>max</sub>	0.008	0.009	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.04	-0.03	-0.03
		Mz <sub>max</sub>	0.04	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N55/N56	Rolled steel	N <sub>min</sub>	-19.496	-19.459	-19.422
		N <sub>max</sub>	17.216	17.244	17.271
		Vy <sub>min</sub>	-0.021	-0.021	-0.021
		Vy <sub>max</sub>	0.016	0.016	0.016
		Vz <sub>min</sub>	-0.009	-0.009	-0.008
		Vz <sub>max</sub>	0.009	0.009	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.02	-0.02
		My <sub>max</sub>	0.03	0.02	0.02
		Mz <sub>min</sub>	-0.03	-0.03	-0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.03	0.03	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N56/N57	Rolled steel	$N_{min}$	-18.574	-18.537	-18.500
		$N_{max}$	16.476	16.503	16.531
		$V_{y_{min}}$	-0.003	-0.003	-0.003
		$V_{y_{max}}$	0.006	0.006	0.006
		$V_{z_{min}}$	-0.008	-0.006	-0.006
		$V_{z_{max}}$	0.004	0.006	0.006
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.02
		$M_{z_{max}}$	0.02	0.02	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N57/N58	Rolled steel	$N_{min}$	-17.576	-17.539	-17.502
		$N_{max}$	15.658	15.686	15.713
		$V_{y_{min}}$	-0.014	-0.014	-0.014
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.012	-0.012	-0.010
		$V_{z_{max}}$	0.012	0.012	0.014
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.03
		$M_{z_{max}}$	0.02	0.02	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N58/N59	Rolled steel	$N_{min}$	-16.453	-16.416	-16.379
		$N_{max}$	14.722	14.750	14.777
		$V_{y_{min}}$	-0.012	-0.012	-0.012
		$V_{y_{max}}$	0.017	0.017	0.017
		$V_{z_{min}}$	-0.012	-0.012	-0.011
		$V_{z_{max}}$	0.013	0.013	0.015
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.03	-0.03	-0.04
		$M_{z_{max}}$	0.02	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N59/N1	Rolled steel	$N_{min}$	-15.262	-15.225	-15.188
		$N_{max}$	13.717	13.744	13.771
		$V_{y_{min}}$	-0.056	-0.056	-0.056



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$V_{y_{max}}$	0.047	0.047	0.047
		$V_{z_{min}}$	-0.063	-0.061	-0.060
		$V_{z_{max}}$	0.054	0.055	0.056
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.04	-0.02	-0.01
		$M_{z_{max}}$	0.03	0.02	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N38/N60	Rolled steel	$N_{min}$	-30.802	-30.708	-30.615
		$N_{max}$	22.019	22.089	22.158
		$V_{y_{min}}$	-0.076	-0.076	-0.076
		$V_{y_{max}}$	0.089	0.089	0.089
		$V_{z_{min}}$	-0.034	-0.032	-0.030
		$V_{z_{max}}$	0.036	0.039	0.042
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	-0.01	-0.02
		$M_{y_{max}}$	0.00	0.01	0.02
		$M_{z_{min}}$	0.00	-0.03	-0.05
		$M_{z_{max}}$	0.00	0.02	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N61/N62	Rolled steel	N <sub>min</sub>	-29.592	-29.499	-29.405
		N <sub>max</sub>	21.617	21.686	21.755
		Vy <sub>min</sub>	-0.014	-0.014	-0.014
		Vy <sub>max</sub>	0.014	0.014	0.014
		Vz <sub>min</sub>	-0.008	-0.005	-0.003
		Vz <sub>max</sub>	-0.001	0.001	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.06	-0.06	-0.05
		Mz <sub>max</sub>	0.06	0.06	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N62/N63	Rolled steel	N <sub>min</sub>	-28.988	-28.895	-28.802
		N <sub>max</sub>	21.424	21.493	21.562
		Vy <sub>min</sub>	-0.008	-0.008	-0.008
		Vy <sub>max</sub>	0.003	0.003	0.003
		Vz <sub>min</sub>	-0.009	-0.007	-0.005
		Vz <sub>max</sub>	0.006	0.007	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N63/N64	Rolled steel	$N_{min}$	-28.361	-28.268	-28.174
		$N_{max}$	21.203	21.273	21.342
		$V_{y_{min}}$	0.000	0.000	0.000
		$V_{y_{max}}$	0.007	0.007	0.007
		$V_{z_{min}}$	-0.002	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N64/N65	Rolled steel	$N_{min}$	-27.711	-27.618	-27.524
		$N_{max}$	20.958	21.027	21.096
		$V_{y_{min}}$	-0.006	-0.006	-0.006
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.005	-0.002	0.000
		$V_{z_{max}}$	-0.001	0.002	0.004
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N65/N66	Rolled steel	$N_{min}$	-27.040	-26.947	-26.853
		$N_{max}$	20.690	20.759	20.829
		$V_{y_{min}}$	0.002	0.002	0.002
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N66/N67	Rolled steel	$N_{min}$	-26.345	-26.251	-26.158
		$N_{max}$	20.399	20.468	20.537
		$V_{y_{min}}$	-0.003	-0.003	-0.003

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	-0.003	-0.003	-0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N67/N68	Rolled steel	$N_{min}$	-25.622	-25.529	-25.435
		$N_{max}$	20.079	20.148	20.218
		$V_{y_{min}}$	0.003	0.003	0.003
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N68/N69	Rolled steel	N <sub>min</sub>	-24.870	-24.777	-24.683
		N <sub>max</sub>	19.730	19.799	19.868
		Vy <sub>min</sub>	-0.003	-0.003	-0.003
		Vy <sub>max</sub>	-0.003	-0.003	-0.003
		Vz <sub>min</sub>	-0.003	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05
		Mz <sub>max</sub>	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N69/N70	Rolled steel	N <sub>min</sub>	-24.084	-23.991	-23.897
		N <sub>max</sub>	19.346	19.415	19.484
		Vy <sub>min</sub>	-0.001	-0.001	-0.001
		Vy <sub>max</sub>	0.007	0.007	0.007
		Vz <sub>min</sub>	-0.005	-0.002	0.000
		Vz <sub>max</sub>	0.000	0.002	0.005
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.05	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N70/N71	Rolled steel	$N_{min}$	-23.259	-23.165	-23.072
		$N_{max}$	18.922	18.991	19.060
		$V_{y_{min}}$	-0.005	-0.005	-0.005
		$V_{y_{max}}$	-0.001	-0.001	-0.001
		$V_{z_{min}}$	-0.006	-0.004	-0.001
		$V_{z_{max}}$	0.002	0.004	0.007
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.06	-0.06
		$M_{z_{max}}$	0.06	0.06	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N71/N72	Rolled steel	$N_{min}$	-22.400	-22.306	-22.213
		$N_{max}$	18.465	18.535	18.604
		$V_{y_{min}}$	-0.010	-0.010	-0.010
		$V_{y_{max}}$	0.017	0.017	0.017
		$V_{z_{min}}$	-0.014	-0.011	-0.009
		$V_{z_{max}}$	0.009	0.011	0.013
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.05	-0.05
		$M_{z_{max}}$	0.06	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N72/N73	Rolled steel	$N_{min}$	-21.522	-21.429	-21.335
		$N_{max}$	17.987	18.056	18.125
		$V_{y_{min}}$	-0.021	-0.021	-0.021
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.010	-0.006	-0.005
		$V_{z_{max}}$	0.004	0.006	0.009
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.04	-0.04
		$M_{z_{max}}$	0.05	0.04	0.04

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N73/N74	Rolled steel	$N_{min}$	-20.597	-20.504	-20.410
		$N_{max}$	17.461	17.530	17.600
		$V_{y_{min}}$	-0.016	-0.016	-0.016



Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{\max}}$	0.020	0.020	0.020
		$V_{z_{\min}}$	-0.011	-0.008	-0.006
		$V_{z_{\max}}$	0.007	0.009	0.012
		$M_{t_{\min}}$	0.00	0.00	0.00
		$M_{t_{\max}}$	0.00	0.00	0.00
		$M_{y_{\min}}$	-0.03	-0.03	-0.03
		$M_{y_{\max}}$	0.03	0.03	0.03
		$M_{z_{\min}}$	-0.04	-0.03	-0.03
		$M_{z_{\max}}$	0.04	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N74/N75	Rolled steel	$N_{\min}$	-19.611	-19.574	-19.537
		$N_{\max}$	16.876	16.904	16.931
		$V_{y_{\min}}$	-0.021	-0.021	-0.021
		$V_{y_{\max}}$	0.016	0.016	0.016
		$V_{z_{\min}}$	-0.008	-0.008	-0.007
		$V_{z_{\max}}$	0.008	0.008	0.010
		$M_{t_{\min}}$	0.00	0.00	0.00
		$M_{t_{\max}}$	0.00	0.00	0.00
		$M_{y_{\min}}$	-0.03	-0.02	-0.02
		$M_{y_{\max}}$	0.03	0.02	0.02
		$M_{z_{\min}}$	-0.03	-0.03	-0.02
		$M_{z_{\max}}$	0.03	0.03	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N75/N76	Rolled steel	N <sub>min</sub>	-18.684	-18.647	-18.610
		N <sub>max</sub>	16.152	16.179	16.207
		Vy <sub>min</sub>	-0.005	-0.005	-0.005
		Vy <sub>max</sub>	0.005	0.005	0.005
		Vz <sub>min</sub>	-0.006	-0.004	-0.004
		Vz <sub>max</sub>	0.003	0.004	0.004
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.02	-0.02
		My <sub>max</sub>	0.02	0.02	0.02
		Mz <sub>min</sub>	-0.02	-0.02	-0.02
		Mz <sub>max</sub>	0.02	0.02	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N76/N77	Rolled steel	N <sub>min</sub>	-17.678	-17.641	-17.604
		N <sub>max</sub>	15.349	15.376	15.404
		Vy <sub>min</sub>	-0.014	-0.014	-0.014
		Vy <sub>max</sub>	0.014	0.014	0.014
		Vz <sub>min</sub>	-0.015	-0.015	-0.013
		Vz <sub>max</sub>	0.015	0.015	0.017
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.02	-0.02
		My <sub>max</sub>	0.02	0.02	0.02
		Mz <sub>min</sub>	-0.02	-0.02	-0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.02	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N77/N78	Rolled steel	$N_{min}$	-16.541	-16.504	-16.467
		$N_{max}$	14.426	14.453	14.480
		$V_{y_{min}}$	-0.020	-0.020	-0.020
		$V_{y_{max}}$	0.025	0.025	0.025
		$V_{z_{min}}$	-0.007	-0.007	-0.005
		$V_{z_{max}}$	0.007	0.007	0.009
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.03	-0.03	-0.04
		$M_{z_{max}}$	0.03	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N78/N2	Rolled steel	$N_{min}$	-15.334	-15.298	-15.261
		$N_{max}$	13.431	13.458	13.485
		$V_{y_{min}}$	-0.063	-0.063	-0.063
		$V_{y_{max}}$	0.055	0.055	0.055
		$V_{z_{min}}$	-0.074	-0.073	-0.072
		$V_{z_{max}}$	0.067	0.067	0.068
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.04	-0.02	-0.01
		$M_{z_{max}}$	0.03	0.02	0.01

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N37/N79	Rolled steel	$N_{min}$	-30.630	-30.536	-30.443
		$N_{max}$	22.498	22.567	22.636
		$V_{y_{min}}$	-0.077	-0.077	-0.077
		$V_{y_{max}}$	0.088	0.088	0.088
		$V_{z_{min}}$	-0.034	-0.032	-0.030
		$V_{z_{max}}$	0.037	0.040	0.042
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	-0.01	-0.02
		$M_{y_{max}}$	0.00	0.01	0.02
		$M_{z_{min}}$	0.00	-0.03	-0.05
		$M_{z_{max}}$	0.00	0.02	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N80/N81	Rolled steel	$N_{min}$	-29.426	-29.332	-29.239
		$N_{max}$	22.082	22.151	22.220
		$V_{y_{min}}$	-0.014	-0.014	-0.014

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.014	0.014	0.014
		$V_{z_{min}}$	-0.008	-0.005	-0.003
		$V_{z_{max}}$	-0.001	0.001	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.05	-0.05
		$M_{z_{max}}$	0.06	0.06	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N81/N82	Rolled steel	$N_{min}$	-28.825	-28.731	-28.638
		$N_{max}$	21.882	21.951	22.020
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.009	-0.007	-0.005
		$V_{z_{max}}$	0.006	0.007	0.011
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N82/N83	Rolled steel	N <sub>min</sub>	-28.200	-28.107	-28.013
		N <sub>max</sub>	21.655	21.724	21.793
		Vy <sub>min</sub>	0.000	0.000	0.000
		Vy <sub>max</sub>	0.007	0.007	0.007
		Vz <sub>min</sub>	-0.002	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05
		Mz <sub>max</sub>	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N83/N84	Rolled steel	N <sub>min</sub>	-27.553	-27.460	-27.367
		N <sub>max</sub>	21.401	21.471	21.540
		Vy <sub>min</sub>	-0.006	-0.006	-0.006
		Vy <sub>max</sub>	0.000	0.000	0.000
		Vz <sub>min</sub>	-0.005	-0.002	0.000
		Vz <sub>max</sub>	-0.001	0.002	0.004
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N84/N85	Rolled steel	$N_{min}$	-26.885	-26.792	-26.699
		$N_{max}$	21.126	21.195	21.265
		$V_{y_{min}}$	0.002	0.002	0.002
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N85/N86	Rolled steel	$N_{min}$	-26.194	-26.100	-26.007
		$N_{max}$	20.826	20.895	20.965
		$V_{y_{min}}$	-0.003	-0.003	-0.003
		$V_{y_{max}}$	-0.003	-0.003	-0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N86/N87	Rolled steel	$N_{min}$	-25.475	-25.381	-25.288
		$N_{max}$	20.498	20.567	20.636
		$V_{y_{min}}$	0.003	0.003	0.003
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N87/N88	Rolled steel	$N_{min}$	-24.727	-24.633	-24.540
		$N_{max}$	20.139	20.209	20.278
		$V_{y_{min}}$	-0.003	-0.003	-0.003



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	-0.003	-0.003	-0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N88/N89	Rolled steel	$N_{min}$	-23.945	-23.851	-23.758
		$N_{max}$	19.745	19.814	19.884
		$V_{y_{min}}$	-0.001	-0.001	-0.001
		$V_{y_{max}}$	0.007	0.007	0.007
		$V_{z_{min}}$	-0.004	-0.002	0.000
		$V_{z_{max}}$	0.000	0.002	0.005
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.06	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N89/N90	Rolled steel	N <sub>min</sub>	-23.124	-23.030	-22.937
		N <sub>max</sub>	19.311	19.380	19.449
		Vy <sub>min</sub>	-0.005	-0.005	-0.005
		Vy <sub>max</sub>	-0.001	-0.001	-0.001
		Vz <sub>min</sub>	-0.006	-0.003	-0.001
		Vz <sub>max</sub>	0.002	0.004	0.007
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.06	-0.06
		Mz <sub>max</sub>	0.06	0.06	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N90/N91	Rolled steel	N <sub>min</sub>	-22.269	-22.176	-22.082
		N <sub>max</sub>	18.843	18.912	18.981
		Vy <sub>min</sub>	-0.010	-0.010	-0.010
		Vy <sub>max</sub>	0.017	0.017	0.017
		Vz <sub>min</sub>	-0.014	-0.011	-0.009
		Vz <sub>max</sub>	0.008	0.011	0.013
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.06	-0.05	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.06	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N91/N92	Rolled steel	$N_{min}$	-21.397	-21.304	-21.210
		$N_{max}$	18.353	18.423	18.492
		$V_{y_{min}}$	-0.020	-0.020	-0.020
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.010	-0.006	-0.005
		$V_{z_{max}}$	0.004	0.006	0.008
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.04	-0.04
		$M_{z_{max}}$	0.05	0.04	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N92/N93	Rolled steel	$N_{min}$	-20.477	-20.384	-20.290
		$N_{max}$	17.815	17.884	17.954
		$V_{y_{min}}$	-0.017	-0.017	-0.017
		$V_{y_{max}}$	0.021	0.021	0.021
		$V_{z_{min}}$	-0.011	-0.009	-0.006
		$V_{z_{max}}$	0.007	0.009	0.012
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.04	-0.03	-0.03
		$M_{z_{max}}$	0.04	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N93/N94	Rolled steel	$N_{min}$	-19.496	-19.459	-19.422
		$N_{max}$	17.216	17.244	17.271
		$V_{y_{min}}$	-0.020	-0.020	-0.020
		$V_{y_{max}}$	0.016	0.016	0.016
		$V_{z_{min}}$	-0.009	-0.009	-0.008
		$V_{z_{max}}$	0.009	0.009	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.02	-0.02
		$M_{y_{max}}$	0.03	0.02	0.02
		$M_{z_{min}}$	-0.03	-0.03	-0.02
		$M_{z_{max}}$	0.03	0.03	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N94/N95	Rolled steel	$N_{min}$	-18.575	-18.538	-18.501
		$N_{max}$	16.477	16.504	16.532
		$V_{y_{min}}$	-0.004	-0.004	-0.004

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.004	0.004	0.004
		$V_{z_{min}}$	-0.007	-0.005	-0.005
		$V_{z_{max}}$	0.004	0.005	0.005
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.02
		$M_{z_{max}}$	0.02	0.02	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N95/N96	Rolled steel	$N_{min}$	-17.576	-17.539	-17.502
		$N_{max}$	15.659	15.687	15.714
		$V_{y_{min}}$	-0.014	-0.014	-0.014
		$V_{y_{max}}$	0.014	0.014	0.014
		$V_{z_{min}}$	-0.012	-0.012	-0.011
		$V_{z_{max}}$	0.012	0.012	0.014
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.03
		$M_{z_{max}}$	0.02	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N96/N97	Rolled steel	N <sub>min</sub>	-16.448	-16.411	-16.374
		N <sub>max</sub>	14.720	14.747	14.774
		Vy <sub>min</sub>	-0.014	-0.014	-0.014
		Vy <sub>max</sub>	0.019	0.019	0.019
		Vz <sub>min</sub>	-0.010	-0.010	-0.009
		Vz <sub>max</sub>	0.010	0.010	0.012
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.02	-0.02
		My <sub>max</sub>	0.02	0.02	0.02
		Mz <sub>min</sub>	-0.03	-0.03	-0.03
		Mz <sub>max</sub>	0.03	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N97/N4	Rolled steel	N <sub>min</sub>	-15.283	-15.246	-15.209
		N <sub>max</sub>	13.734	13.761	13.788
		Vy <sub>min</sub>	-0.060	-0.060	-0.060
		Vy <sub>max</sub>	0.056	0.056	0.056
		Vz <sub>min</sub>	-0.063	-0.062	-0.060
		Vz <sub>max</sub>	0.060	0.060	0.062
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.01	-0.02
		My <sub>max</sub>	0.02	0.01	0.02
		Mz <sub>min</sub>	-0.03	-0.02	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
		Mz <sub>max</sub>	0.03	0.02	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N39/N98	Rolled steel	N <sub>min</sub>	-30.140	-30.047	-29.953
		N <sub>max</sub>	22.656	22.725	22.794
		Vy <sub>min</sub>	-0.076	-0.076	-0.076
		Vy <sub>max</sub>	0.089	0.089	0.089
		Vz <sub>min</sub>	-0.033	-0.031	-0.029
		Vz <sub>max</sub>	0.037	0.040	0.043
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	-0.01	-0.02
		My <sub>max</sub>	0.00	0.01	0.02
		Mz <sub>min</sub>	0.00	-0.03	-0.05
		Mz <sub>max</sub>	0.00	0.02	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N99/N100	Rolled steel	N <sub>min</sub>	-28.950	-28.857	-28.763
		N <sub>max</sub>	22.235	22.305	22.374
		Vy <sub>min</sub>	-0.014	-0.014	-0.014
		Vy <sub>max</sub>	0.014	0.014	0.014
		Vz <sub>min</sub>	-0.008	-0.005	-0.003
		Vz <sub>max</sub>	-0.001	0.001	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.06	-0.05
		$M_{z_{max}}$	0.06	0.06	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N100/N101	Rolled steel	$N_{min}$	-28.356	-28.263	-28.169
		$N_{max}$	22.033	22.103	22.172
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.009	-0.007	-0.005
		$V_{z_{max}}$	0.006	0.007	0.011
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N101/N102	Rolled steel	$N_{min}$	-27.740	-27.646	-27.553
		$N_{max}$	21.804	21.873	21.942
		$V_{y_{min}}$	0.000	0.000	0.000



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.007	0.007	0.007
		$V_{z_{min}}$	-0.002	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N102/N103	Rolled steel	$N_{min}$	-27.101	-27.007	-26.914
		$N_{max}$	21.548	21.617	21.687
		$V_{y_{min}}$	-0.006	-0.006	-0.006
		$V_{y_{max}}$	0.000	0.000	0.000
		$V_{z_{min}}$	-0.005	-0.002	0.000
		$V_{z_{max}}$	-0.001	0.002	0.004
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N103/N104	Rolled steel	N <sub>min</sub>	-26.441	-26.348	-26.254
		N <sub>max</sub>	21.270	21.340	21.409
		Vy <sub>min</sub>	0.002	0.002	0.002
		Vy <sub>max</sub>	0.003	0.003	0.003
		Vz <sub>min</sub>	-0.003	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05
		Mz <sub>max</sub>	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N104/N105	Rolled steel	N <sub>min</sub>	-25.758	-25.665	-25.571
		N <sub>max</sub>	20.968	21.037	21.106
		Vy <sub>min</sub>	-0.003	-0.003	-0.003
		Vy <sub>max</sub>	-0.003	-0.003	-0.003
		Vz <sub>min</sub>	-0.003	0.000	0.002
		Vz <sub>max</sub>	-0.002	0.000	0.003
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N105/N106	Rolled steel	$N_{min}$	-25.049	-24.955	-24.862
		$N_{max}$	20.637	20.706	20.775
		$V_{y_{min}}$	0.003	0.003	0.003
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N106/N107	Rolled steel	$N_{min}$	-24.311	-24.218	-24.124
		$N_{max}$	20.275	20.344	20.413
		$V_{y_{min}}$	-0.003	-0.003	-0.003
		$V_{y_{max}}$	-0.002	-0.002	-0.002
		$V_{z_{min}}$	-0.003	0.000	0.002
		$V_{z_{max}}$	-0.002	0.000	0.003
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.05
		$M_{z_{max}}$	0.05	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N107/N108	Rolled steel	$N_{min}$	-23.540	-23.446	-23.353
		$N_{max}$	19.878	19.947	20.016
		$V_{y_{min}}$	-0.001	-0.001	-0.001
		$V_{y_{max}}$	0.007	0.007	0.007
		$V_{z_{min}}$	-0.005	-0.002	0.000
		$V_{z_{max}}$	0.000	0.002	0.005
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.05	-0.05	-0.06
		$M_{z_{max}}$	0.05	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N108/N109	Rolled steel	$N_{min}$	-22.730	-22.637	-22.543
		$N_{max}$	19.440	19.509	19.578
		$V_{y_{min}}$	-0.005	-0.005	-0.005

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	-0.001	-0.001	-0.001
		$V_{z_{min}}$	-0.006	-0.004	-0.001
		$V_{z_{max}}$	0.002	0.004	0.007
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.06	-0.06
		$M_{z_{max}}$	0.06	0.06	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N109/N110	Rolled steel	$N_{min}$	-21.888	-21.794	-21.701
		$N_{max}$	18.969	19.038	19.107
		$V_{y_{min}}$	-0.010	-0.010	-0.010
		$V_{y_{max}}$	0.017	0.017	0.017
		$V_{z_{min}}$	-0.014	-0.011	-0.009
		$V_{z_{max}}$	0.009	0.011	0.013
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.03	-0.03
		$M_{y_{max}}$	0.03	0.03	0.03
		$M_{z_{min}}$	-0.06	-0.05	-0.05
		$M_{z_{max}}$	0.06	0.05	0.05

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N110/N111	Rolled steel	N <sub>min</sub>	-21.028	-20.934	-20.841
		N <sub>max</sub>	18.475	18.544	18.613
		Vy <sub>min</sub>	-0.021	-0.021	-0.021
		Vy <sub>max</sub>	0.015	0.015	0.015
		Vz <sub>min</sub>	-0.010	-0.006	-0.005
		Vz <sub>max</sub>	0.004	0.006	0.009
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.05	-0.04	-0.04
		Mz <sub>max</sub>	0.05	0.04	0.04

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N111/N112	Rolled steel	N <sub>min</sub>	-20.121	-20.028	-19.934
		N <sub>max</sub>	17.933	18.002	18.071
		Vy <sub>min</sub>	-0.016	-0.016	-0.016
		Vy <sub>max</sub>	0.020	0.020	0.020
		Vz <sub>min</sub>	-0.010	-0.008	-0.006
		Vz <sub>max</sub>	0.006	0.008	0.011
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.03	-0.03	-0.03
		My <sub>max</sub>	0.03	0.03	0.03
		Mz <sub>min</sub>	-0.04	-0.03	-0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.04	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N112/N113	Rolled steel	$N_{min}$	-19.155	-19.117	-19.080
		$N_{max}$	17.330	17.357	17.384
		$V_{y_{min}}$	-0.020	-0.020	-0.020
		$V_{y_{max}}$	0.016	0.016	0.016
		$V_{z_{min}}$	-0.008	-0.008	-0.007
		$V_{z_{max}}$	0.008	0.008	0.010
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.03	-0.02	-0.02
		$M_{y_{max}}$	0.03	0.02	0.02
		$M_{z_{min}}$	-0.03	-0.03	-0.02
		$M_{z_{max}}$	0.03	0.03	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N113/N114	Rolled steel	$N_{min}$	-18.251	-18.214	-18.177
		$N_{max}$	16.587	16.614	16.642
		$V_{y_{min}}$	-0.006	-0.006	-0.006
		$V_{y_{max}}$	0.006	0.006	0.006
		$V_{z_{min}}$	-0.005	-0.004	-0.004
		$V_{z_{max}}$	0.003	0.004	0.004
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.02
		$M_{z_{max}}$	0.02	0.02	0.02

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N114/N115	Rolled steel	$N_{min}$	-17.269	-17.232	-17.195
		$N_{max}$	15.763	15.790	15.818
		$V_{y_{min}}$	-0.013	-0.013	-0.013
		$V_{y_{max}}$	0.013	0.013	0.013
		$V_{z_{min}}$	-0.015	-0.015	-0.013
		$V_{z_{max}}$	0.015	0.015	0.017
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.02	-0.02	-0.03
		$M_{z_{max}}$	0.02	0.02	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N115/N116	Rolled steel	$N_{min}$	-16.154	-16.117	-16.080
		$N_{max}$	14.811	14.838	14.866
		$V_{y_{min}}$	-0.021	-0.021	-0.021



Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$V_{y_{max}}$	0.026	0.026	0.026
		$V_{z_{min}}$	-0.006	-0.006	-0.004
		$V_{z_{max}}$	0.006	0.006	0.007
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.02
		$M_{y_{max}}$	0.02	0.02	0.02
		$M_{z_{min}}$	-0.03	-0.03	-0.04
		$M_{z_{max}}$	0.03	0.03	0.03

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.288 m	0.575 m
N116/N3	Rolled steel	$N_{min}$	-14.997	-14.960	-14.923
		$N_{max}$	13.810	13.837	13.864
		$V_{y_{min}}$	-0.063	-0.063	-0.063
		$V_{y_{max}}$	0.058	0.058	0.058
		$V_{z_{min}}$	-0.075	-0.074	-0.072
		$V_{z_{max}}$	0.069	0.070	0.072
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.04	-0.02	0.00
		$M_{z_{max}}$	0.03	0.02	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N98/N99	Rolled steel	N <sub>min</sub>	-29.522	-29.429	-29.335
		N <sub>max</sub>	22.427	22.496	22.565
		Vy <sub>min</sub>	-0.027	-0.027	-0.027
		Vy <sub>max</sub>	0.015	0.015	0.015
		Vz <sub>min</sub>	-0.040	-0.037	-0.034
		Vz <sub>max</sub>	0.030	0.032	0.034
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.02	-0.03
		My <sub>max</sub>	0.02	0.02	0.03
		Mz <sub>min</sub>	-0.05	-0.06	-0.06
		Mz <sub>max</sub>	0.04	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N79/N80	Rolled steel	N <sub>min</sub>	-30.004	-29.911	-29.818
		N <sub>max</sub>	22.271	22.340	22.410
		Vy <sub>min</sub>	-0.027	-0.027	-0.027
		Vy <sub>max</sub>	0.015	0.015	0.015
		Vz <sub>min</sub>	-0.039	-0.036	-0.034
		Vz <sub>max</sub>	0.031	0.033	0.035
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	-0.02	-0.02	-0.03
		My <sub>max</sub>	0.02	0.02	0.03
		Mz <sub>min</sub>	-0.05	-0.05	-0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{z_{max}}$	0.04	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N60/N61	Rolled steel	$N_{min}$	-30.173	-30.080	-29.987
		$N_{max}$	21.800	21.869	21.938
		$V_{y_{min}}$	-0.027	-0.027	-0.027
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.040	-0.037	-0.034
		$V_{z_{max}}$	0.030	0.032	0.034
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.05	-0.06	-0.06
		$M_{z_{max}}$	0.04	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
N41/N42	Rolled steel	$N_{min}$	-30.009	-29.916	-29.823
		$N_{max}$	22.276	22.345	22.415
		$V_{y_{min}}$	-0.026	-0.026	-0.026
		$V_{y_{max}}$	0.015	0.015	0.015
		$V_{z_{min}}$	-0.040	-0.037	-0.035
		$V_{z_{max}}$	0.030	0.032	0.034
		$M_{t_{min}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.290 m	0.580 m
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	-0.02	-0.02	-0.03
		$M_{y_{max}}$	0.02	0.02	0.03
		$M_{z_{min}}$	-0.05	-0.06	-0.06
		$M_{z_{max}}$	0.04	0.05	0.06

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.194 m	0.389 m
N5/N117	Rolled steel	$N_{min}$	-1.193	-1.193	-1.193
		$N_{max}$	1.198	1.198	1.198
		$V_{y_{min}}$	-0.008	-0.008	-0.008
		$V_{y_{max}}$	0.004	0.004	0.004
		$V_{z_{min}}$	-0.020	-0.013	-0.006
		$V_{z_{max}}$	-0.007	-0.002	0.003
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.194 m	0.389 m
N117/N8	Rolled steel	$N_{min}$	-1.198	-1.198	-1.198
		$N_{max}$	1.192	1.192	1.192
		$V_{y_{min}}$	-0.003	-0.003	-0.003

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.194 m	0.389 m
		$V_{y_{max}}$	0.009	0.009	0.009
		$V_{z_{min}}$	-0.003	0.003	0.008
		$V_{z_{max}}$	-0.002	0.004	0.011
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.194 m	0.389 m
N7/N117	Rolled steel	$N_{min}$	-1.175	-1.175	-1.175
		$N_{max}$	1.199	1.199	1.199
		$V_{y_{min}}$	-0.010	-0.010	-0.010
		$V_{y_{max}}$	0.003	0.003	0.003
		$V_{z_{min}}$	-0.014	-0.007	-0.001
		$V_{z_{max}}$	-0.006	-0.001	0.005
		$M_{t_{min}}$	0.00	0.00	0.00
		$M_{t_{max}}$	0.00	0.00	0.00
		$M_{y_{min}}$	0.00	0.00	0.00
		$M_{y_{max}}$	0.00	0.00	0.00
		$M_{z_{min}}$	0.00	0.00	0.00
		$M_{z_{max}}$	0.00	0.00	0.00

Bar force envelopes					
Bar	Combination type	Force	Positions on the bar		
			0.000 m	0.194 m	0.389 m
N117/N6	Rolled steel	N <sub>min</sub>	-1.200	-1.200	-1.200
		N <sub>max</sub>	1.174	1.174	1.174
		Vy <sub>min</sub>	-0.004	-0.004	-0.004
		Vy <sub>max</sub>	0.007	0.007	0.007
		Vz <sub>min</sub>	-0.003	0.002	0.008
		Vz <sub>max</sub>	0.009	0.016	0.023
		Mt <sub>min</sub>	0.00	0.00	0.00
		Mt <sub>max</sub>	0.00	0.00	0.00
		My <sub>min</sub>	0.00	0.00	-0.01
		My <sub>max</sub>	0.00	0.00	0.00
		Mz <sub>min</sub>	0.00	0.00	0.00
		Mz <sub>max</sub>	0.00	0.00	0.00

### 2.3.2.2.- U.L.S. Checks (Summarised)

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>y</sub>	M <sub>z</sub>	V <sub>z</sub>	V <sub>y</sub>	M <sub>y</sub> V <sub>z</sub>	M <sub>z</sub> V <sub>y</sub>	NM <sub>y</sub> M <sub>z</sub>	NM <sub>y</sub> M <sub>z</sub> V <sub>y</sub> V <sub>z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>z</sub>	M <sub>t</sub> V <sub>y</sub>	
N1/N2	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.6	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.6
N3/N1	η = 0.3	η = 0.3	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.6	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.6
N3/N4	η = 0.3	η = 0.3	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.6	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.6
N4/N2	η = 0.2	η = 0.3	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.6	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.6
N5/N6	η = 0.9	η = 0.9	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 1.2	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.2
N7/N5	η = 0.9	η = 0.9	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 1.2	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.2
N7/N8	η = 0.9	η = 0.9	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 1.2	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.2
N8/N6	η = 0.9	η = 0.9	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 1.2	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.2
N2/N10	x: 0.5 m η = 5.5	x: 0 m η = 6.2	x: 0.5 m η = 1.8	x: 0 m η = 2.2	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 9.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 9.3

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>y</sub>	M <sub>z</sub>	V <sub>z</sub>	V <sub>y</sub>	M <sub>y</sub> V <sub>z</sub>	M <sub>z</sub> V <sub>y</sub>	NM <sub>y</sub> M <sub>z</sub>	NM <sub>y</sub> M <sub>z</sub> zV <sub>y</sub> V <sub>z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>z</sub>	M <sub>t</sub> V <sub>y</sub>	
N10/N14	x: 0.575 m η = 4.8	x: 0 m η = 5.4	x: 0 m η = 1.8	x: 0 m η = 2.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 7.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 7.3
N14/N18	x: 0.575 m η = 4.0	x: 0 m η = 4.6	x: 0 m η = 1.8	x: 0 m η = 1.8	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 6.4	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 6.4
N18/N22	x: 0.575 m η = 3.3	x: 0 m η = 3.7	x: 0 m η = 1.5	x: 0 m η = 1.6	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 5.2
N22/N26	x: 0.575 m η = 2.6	x: 0 m η = 2.9	x: 0 m η = 1.2	x: 0 m η = 1.2	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 4.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 4.1
N26/N30	x: 0.575 m η = 1.8	x: 0 m η = 2.1	x: 0 m η = 0.9	x: 0 m η = 0.9	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 3.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 3.0
N30/N34	x: 0.575 m η = 1.1	x: 0 m η = 1.3	x: 0 m η = 0.6	x: 0 m η = 0.6	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.288 m η = 1.8	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.8
N34/N6	x: 0.575 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 0.4	x: 0 m η = 0.3	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 1.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.0
N1/N9	x: 0.5 m η = 5.6	x: 0 m η = 6.2	x: 0.5 m η = 2.0	x: 0.5 m η = 2.0	η = 0.2	η = 0.1	η < 0.1	η < 0.1	x: 0.5 m η = 9.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 9.9
N9/N13	x: 0.575 m η = 4.9	x: 0 m η = 5.4	x: 0.575 m η = 2.1	x: 0 m η = 2.0	η = 0.2	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 9.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 9.1
N13/N17	x: 0.575 m η = 4.1	x: 0 m η = 4.5	x: 0 m η = 2.1	x: 0.575 m η = 1.7	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 8.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 8.2
N17/N21	x: 0.575 m η = 3.4	x: 0 m η = 3.7	x: 0 m η = 1.4	x: 0 m η = 1.7	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 6.8	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 6.8
N21/N25	x: 0.575 m η = 2.6	x: 0 m η = 2.9	x: 0 m η = 1.4	x: 0 m η = 1.1	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.4	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 5.4
N25/N29	x: 0.575 m η = 1.9	x: 0 m η = 2.1	x: 0 m η = 0.8	x: 0 m η = 1.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 3.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 3.9
N29/N33	x: 0.575 m η = 1.1	x: 0 m η = 1.3	x: 0 m η = 0.6	x: 0 m η = 0.6	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 2.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 2.3
N33/N5	x: 0.575 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 0.3	x: 0 m η = 0.3	η < 0.1	η < 0.1	η < 0.1	x: 0 m η < 0.1	x: 0 m η = 0.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.9
N4/N12	x: 0.5 m η = 5.6	x: 0 m η = 6.2	x: 0.5 m η = 2.3	x: 0.5 m η = 1.6	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0.5 m η = 9.7	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 9.7
N12/N16	x: 0.575 m η = 4.9	x: 0 m η = 5.4	x: 0 m η = 2.3	x: 0.575 m η = 2.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0.575 m η = 9.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 9.0
N16/N20	x: 0.575 m η = 4.1	x: 0 m η = 4.5	x: 0 m η = 1.7	x: 0 m η = 2.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 8.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 8.1
N20/N24	x: 0.575 m η = 3.4	x: 0 m η = 3.7	x: 0 m η = 1.7	x: 0 m η = 1.4	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 6.8	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 6.8
N24/N28	x: 0.575 m η = 2.6	x: 0 m η = 2.9	x: 0 m η = 1.1	x: 0 m η = 1.4	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.4	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 5.4
N28/N32	x: 0.575 m η = 1.9	x: 0 m η = 2.1	x: 0 m η = 1.0	x: 0 m η = 0.9	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 3.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 3.9
N32/N36	x: 0.575 m η = 1.1	x: 0 m η = 1.3	x: 0 m η = 0.6	x: 0 m η = 0.6	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 2.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 2.3
N36/N8	x: 0.575 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 0.2	x: 0 m η = 0.2	η < 0.1	η < 0.1	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 0.9	x: 0 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.9
N3/N11	x: 0.5 m η = 5.6	x: 0 m η = 6.1	x: 0.5 m η = 1.8	x: 0.5 m η = 2.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 8.5	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 8.5
N11/N15	x: 0.575 m η = 4.9	x: 0 m η = 5.3	x: 0.575 m η = 1.8	x: 0 m η = 2.0	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 7.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 7.3

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>y</sub>	M <sub>z</sub>	V <sub>z</sub>	V <sub>y</sub>	M <sub>y</sub> V <sub>z</sub>	M <sub>z</sub> V <sub>y</sub>	NM <sub>y</sub> M <sub>z</sub>	NM <sub>y</sub> M <sub>z</sub> zV <sub>y</sub> V <sub>z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>z</sub>	M <sub>t</sub> V <sub>y</sub>	
N15/N19	x: 0.575 m η = 4.2	x: 0 m η = 4.5	x: 0 m η = 1.8	x: 0 m η = 1.8	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 6.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 6.3
N19/N23	x: 0.575 m η = 3.4	x: 0 m η = 3.7	x: 0 m η = 1.5	x: 0 m η = 1.6	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 5.1
N23/N27	x: 0.575 m η = 2.6	x: 0 m η = 2.9	x: 0 m η = 1.2	x: 0 m η = 1.2	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 4.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 4.0
N27/N31	x: 0.575 m η = 1.9	x: 0 m η = 2.0	x: 0 m η = 0.9	x: 0 m η = 0.9	η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0 m η = 2.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 2.9
N31/N35	x: 0.575 m η = 1.1	x: 0 m η = 1.2	x: 0 m η = 0.6	x: 0 m η = 0.6	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.288 m η = 1.7	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.7
N35/N7	x: 0.575 m η = 0.5	x: 0 m η = 0.5	x: 0 m η = 0.4	x: 0 m η = 0.3	η < 0.1	η < 0.1	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 1.0	x: 0 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 1.0
N9/N10	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N11/N9	η = 0.2	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.4	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.4
N11/N12	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N12/N10	η = 0.1	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.4	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.4
N13/N14	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N15/N13	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N15/N16	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N16/N14	η = 0.2	η = 0.2	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N17/N18	η = 0.2	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N19/N17	η = 0.2	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N19/N20	η = 0.2	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N20/N18	η = 0.2	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.5	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.5
N21/N22	η = 0.1	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.4	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.4
N23/N21	η = 0.1	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.4	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.4
N23/N24	η = 0.1	η = 0.1	x: 0.275 m η = 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	x: 0.275 m η = 0.4	D.N.P. <sup>(4)</sup>	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED η = 0.4



Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>	
N24/N22	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N25/N26	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N27/N25	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N27/N28	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N28/N26	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N29/N30	$\eta = 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N31/N29	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N31/N32	$\eta = 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> $\eta = 0.4$
N32/N30	$\eta = 0.1$	$\eta = 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.4$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N33/N34	$\eta < 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.3$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N35/N33	$\eta < 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.2$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N35/N36	$\eta < 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.3$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N36/N34	$\eta < 0.1$	$\eta < 0.1$	$x: 0.275 \text{ m}$ $\eta = 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	D.N.P. <sup>(3)</sup>	D.N.P. <sup>(3)</sup>	$x: 0.275 \text{ m}$ $\eta = 0.2$	D.N.P. <sup>(4)</sup>	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N4/N10	$x: 0.743 \text{ m}$ $\eta = 1.6$	$x: 0 \text{ m}$ $\eta = 1.6$	$x: 0.372 \text{ m}$ $\eta = 0.2$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	$x: 0.186 \text{ m}$ $\eta < 0.1$	D.N.P. <sup>(3)</sup>	$x: 0.372 \text{ m}$ $\eta = 2.0$	$x: 0.186 \text{ m}$ $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N10/N16	$x: 0.796 \text{ m}$ $\eta = 1.5$	$x: 0 \text{ m}$ $\eta = 1.6$	$x: 0.398 \text{ m}$ $\eta = 0.2$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	$x: 0.199 \text{ m}$ $\eta < 0.1$	D.N.P. <sup>(3)</sup>	$x: 0.398 \text{ m}$ $\eta = 2.0$	$x: 0.199 \text{ m}$ $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N16/N18	$x: 0.796 \text{ m}$ $\eta = 1.7$	$x: 0 \text{ m}$ $\eta = 1.7$	$x: 0.398 \text{ m}$ $\eta = 0.2$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	$x: 0.199 \text{ m}$ $\eta < 0.1$	D.N.P. <sup>(3)</sup>	$x: 0.398 \text{ m}$ $\eta = 2.2$	$x: 0.199 \text{ m}$ $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N18/N24	$x: 0.796 \text{ m}$ $\eta = 1.5$	$x: 0 \text{ m}$ $\eta = 1.6$	$x: 0.398 \text{ m}$ $\eta = 0.2$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	$x: 0.199 \text{ m}$ $\eta < 0.1$	D.N.P. <sup>(3)</sup>	$x: 0.398 \text{ m}$ $\eta = 2.1$	$x: 0.199 \text{ m}$ $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N24/N26	$x: 0.796 \text{ m}$ $\eta = 1.7$	$x: 0 \text{ m}$ $\eta = 1.7$	$x: 0.398 \text{ m}$ $\eta = 0.2$	$M_{Ed} = 0.00$ D.N.P. <sup>(1)</sup>	$x: 0 \text{ m}$ $\eta < 0.1$	$V_{Ed} = 0.00$ D.N.P. <sup>(2)</sup>	$x: 0.199 \text{ m}$ $\eta < 0.1$	D.N.P. <sup>(3)</sup>	$x: 0.398 \text{ m}$ $\eta = 2.2$	$x: 0.199 \text{ m}$ $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>		
N26/N32	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N32/N34	x: 0.796 m η = 1.7	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N34/N8	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N2/N9	x: 0.743 m η = 1.5	x: 0 m η = 1.5	x: 0.372 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.186 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.37 2 m η = 1.9	x: 0.186 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N9/N14	x: 0.796 m η = 1.7	x: 0 m η = 1.8	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N14/N17	x: 0.796 m η = 1.5	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N17/N22	x: 0.796 m η = 1.7	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N22/N25	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N25/N30	x: 0.796 m η = 1.7	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N30/N33	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N33/N6	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N3/N12	x: 0.743 m η = 1.5	x: 0 m η = 1.5	x: 0.372 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.186 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.37 2 m η = 1.9	x: 0.186 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N12/N15	x: 0.796 m η = 1.7	x: 0 m η = 1.8	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N15/N20	x: 0.796 m η = 1.5	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N20/N23	x: 0.796 m η = 1.7	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N23/N28	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>		
N28/N31	x: 0.796 m η = 1.7	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N31/N36	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N36/N7	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N1/N11	x: 0.743 m η = 1.6	x: 0 m η = 1.7	x: 0.372 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.186 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.37 2 m η = 2.1	x: 0.186 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N11/N13	x: 0.796 m η = 1.5	x: 0 m η = 1.5	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N13/N19	x: 0.796 m η = 1.7	x: 0 m η = 1.8	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N19/N21	x: 0.796 m η = 1.6	x: 0 m η = 1.5	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N21/N27	x: 0.796 m η = 1.7	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N27/N29	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.0	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N29/N35	x: 0.796 m η = 1.6	x: 0 m η = 1.7	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.2	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N35/N5	x: 0.796 m η = 1.6	x: 0 m η = 1.6	x: 0.398 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.199 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.39 8 m η = 2.1	x: 0.199 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N39/N79	x: 1.184 m η = 0.6	x: 0 m η = 0.6	x: 0.592 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.197 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.59 2 m η = 1.9	x: 0.197 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N79/N99	x: 1.163 m η = 0.5	x: 0 m η = 0.5	x: 0.581 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.194 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.58 1 m η = 1.8	x: 0.194 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N99/N81	x: 1.141 m η = 0.5	x: 0 m η = 0.5	x: 0.571 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.19 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.57 1 m η = 1.7	x: 0.19 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N81/N101	x: 1.12 m η = 0.5	x: 0 m η = 0.5	x: 0.56 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.187 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.56 m η = 1.7	x: 0.187 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N101/N83	x: 1.099 m η = 0.5	x: 0 m η = 0.5	x: 0.55 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.183 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.55 m η = 1.6	x: 0.183 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>	
N83/N103	x: 1.078 m η = 0.5	x: 0 m η = 0.5	x: 0.539 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.18 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.53 9 m η = 1.6	x: 0.18 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N103/N85	x: 1.057 m η = 0.6	x: 0 m η = 0.6	x: 0.529 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.176 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.52 9 m η = 1.6	x: 0.176 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N85/N105	x: 1.037 m η = 0.6	x: 0 m η = 0.6	x: 0.518 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.173 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.51 8 m η = 1.5	x: 0.173 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N105/N87	x: 1.016 m η = 0.6	x: 0 m η = 0.6	x: 0.508 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.169 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.50 8 m η = 1.5	x: 0.169 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N87/N107	x: 0.996 m η = 0.6	x: 0 m η = 0.6	x: 0.498 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.249 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.49 8 m η = 1.5	x: 0.249 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N107/N89	x: 0.976 m η = 0.7	x: 0 m η = 0.7	x: 0.488 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.244 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.48 8 m η = 1.5	x: 0.244 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N89/N109	x: 0.956 m η = 0.7	x: 0 m η = 0.7	x: 0.478 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.239 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.47 8 m η = 1.5	x: 0.239 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N109/N91	x: 0.937 m η = 0.7	x: 0 m η = 0.7	x: 0.468 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.234 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.46 8 m η = 1.4	x: 0.234 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N91/N111	x: 0.917 m η = 0.7	x: 0 m η = 0.7	x: 0.459 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.229 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.45 9 m η = 1.4	x: 0.229 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N111/N93	x: 0.898 m η = 0.7	x: 0 m η = 0.8	x: 0.449 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.225 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.44 9 m η = 1.4	x: 0.225 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N93/N113	x: 0.879 m η = 0.8	x: 0 m η = 0.8	x: 0.44 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.22 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.44 m η = 1.4	x: 0.22 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N113/N95	x: 0.861 m η = 0.9	x: 0 m η = 0.9	x: 0.431 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.215 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.43 1 m η = 1.5	x: 0.215 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N95/N115	x: 0.843 m η = 0.9	x: 0 m η = 0.9	x: 0.421 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.211 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.42 1 m η = 1.5	x: 0.211 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N115/N97	x: 0.825 m η = 1.0	x: 0 m η = 1.0	x: 0.413 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.206 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.41 3 m η = 1.5	x: 0.206 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N97/N3	x: 0.804 m η = 1.0	x: 0 m η = 1.0	x: 0.402 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.201 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.40 2 m η = 1.5	x: 0.201 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N37/N60	x: 1.184 m η = 0.6	x: 0 m η = 0.6	x: 0.592 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.197 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.59 2 m η = 1.9	x: 0.197 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>		
N60/N80	x: 1.163 m η = 0.5	x: 0 m η = 0.5	x: 0.581 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.194 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.58 1 m η = 1.8	x: 0.194 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N80/N62	x: 1.141 m η = 0.5	x: 0 m η = 0.5	x: 0.571 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.19 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.57 1 m η = 1.7	x: 0.19 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N62/N82	x: 1.12 m η = 0.5	x: 0 m η = 0.5	x: 0.56 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.187 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.56 m η = 1.7	x: 0.187 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N82/N64	x: 1.099 m η = 0.5	x: 0 m η = 0.5	x: 0.55 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.183 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.55 m η = 1.6	x: 0.183 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N64/N84	x: 1.078 m η = 0.5	x: 0 m η = 0.6	x: 0.539 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.18 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.53 9 m η = 1.6	x: 0.18 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N84/N66	x: 1.057 m η = 0.6	x: 0 m η = 0.6	x: 0.529 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.176 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.52 9 m η = 1.6	x: 0.176 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N66/N86	x: 1.037 m η = 0.6	x: 0 m η = 0.6	x: 0.518 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.173 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.51 8 m η = 1.6	x: 0.173 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N86/N68	x: 1.016 m η = 0.6	x: 0 m η = 0.6	x: 0.508 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.169 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.50 8 m η = 1.5	x: 0.169 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N68/N88	x: 0.996 m η = 0.6	x: 0 m η = 0.6	x: 0.498 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.249 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.49 8 m η = 1.5	x: 0.249 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N88/N70	x: 0.976 m η = 0.7	x: 0 m η = 0.7	x: 0.488 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.244 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.48 8 m η = 1.5	x: 0.244 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N70/N90	x: 0.956 m η = 0.7	x: 0 m η = 0.7	x: 0.478 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.239 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.47 8 m η = 1.5	x: 0.239 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N90/N72	x: 0.937 m η = 0.7	x: 0 m η = 0.7	x: 0.468 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.234 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.46 8 m η = 1.4	x: 0.234 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N72/N92	x: 0.917 m η = 0.7	x: 0 m η = 0.7	x: 0.459 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.229 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.45 9 m η = 1.4	x: 0.229 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N92/N74	x: 0.898 m η = 0.8	x: 0 m η = 0.7	x: 0.449 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.225 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 9 m η = 1.4	x: 0.225 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N74/N94	x: 0.879 m η = 0.8	x: 0 m η = 0.8	x: 0.44 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.22 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 m η = 1.4	x: 0.22 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N94/N76	x: 0.861 m η = 0.9	x: 0 m η = 0.9	x: 0.431 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.215 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.43 1 m η = 1.4	x: 0.215 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>		
N76/N96	x: 0.843 m η = 0.9	x: 0 m η = 0.9	x: 0.421 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.211 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.42 1 m η = 1.5	x: 0.211 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N96/N78	x: 0.825 m η = 1.0	x: 0 m η = 1.0	x: 0.413 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.206 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.41 3 m η = 1.5	x: 0.206 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N78/N4	x: 0.804 m η = 1.0	x: 0 m η = 1.0	x: 0.402 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.201 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.40 2 m η = 1.5	x: 0.201 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N38/N41	x: 1.184 m η = 0.6	x: 0 m η = 0.6	x: 0.592 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.197 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.59 2 m η = 1.9	x: 0.197 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N41/N61	x: 1.163 m η = 0.5	x: 0 m η = 0.5	x: 0.581 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.194 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.58 1 m η = 1.8	x: 0.194 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N61/N43	x: 1.141 m η = 0.5	x: 0 m η = 0.5	x: 0.571 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.19 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.57 1 m η = 1.7	x: 0.19 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N43/N63	x: 1.12 m η = 0.5	x: 0 m η = 0.5	x: 0.56 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.187 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.56 m η = 1.7	x: 0.187 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N63/N45	x: 1.099 m η = 0.5	x: 0 m η = 0.5	x: 0.55 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.183 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.55 m η = 1.6	x: 0.183 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N45/N65	x: 1.078 m η = 0.5	x: 0 m η = 0.5	x: 0.539 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.18 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.53 9 m η = 1.6	x: 0.18 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N65/N47	x: 1.057 m η = 0.6	x: 0 m η = 0.6	x: 0.529 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.176 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.52 9 m η = 1.6	x: 0.176 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N47/N67	x: 1.037 m η = 0.6	x: 0 m η = 0.6	x: 0.518 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.173 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.51 8 m η = 1.5	x: 0.173 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N67/N49	x: 1.016 m η = 0.6	x: 0 m η = 0.6	x: 0.508 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.169 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.50 8 m η = 1.5	x: 0.169 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N49/N69	x: 0.996 m η = 0.6	x: 0 m η = 0.6	x: 0.498 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.249 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.49 8 m η = 1.5	x: 0.249 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N69/N51	x: 0.976 m η = 0.7	x: 0 m η = 0.7	x: 0.488 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.244 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.48 8 m η = 1.5	x: 0.244 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N51/N71	x: 0.956 m η = 0.7	x: 0 m η = 0.7	x: 0.478 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.239 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.47 8 m η = 1.5	x: 0.239 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N71/N53	x: 0.937 m η = 0.7	x: 0 m η = 0.7	x: 0.468 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.234 m η < 0.1		D.N.P. <sup>(3)</sup>	x: 0.46 8 m η = 1.4	x: 0.234 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>		
N53/N73	x: 0.917 m η = 0.7	x: 0 m η = 0.7	x: 0.459 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.229 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.45 9 m η = 1.4	x: 0.229 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N73/N55	x: 0.898 m η = 0.7	x: 0 m η = 0.8	x: 0.449 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.225 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 9 m η = 1.4	x: 0.225 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N55/N75	x: 0.879 m η = 0.8	x: 0 m η = 0.8	x: 0.44 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.22 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 m η = 1.4	x: 0.22 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N75/N57	x: 0.861 m η = 0.9	x: 0 m η = 0.9	x: 0.431 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.215 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.43 1 m η = 1.5	x: 0.215 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N57/N77	x: 0.843 m η = 0.9	x: 0 m η = 0.9	x: 0.421 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.211 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.42 1 m η = 1.5	x: 0.211 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N77/N59	x: 0.825 m η = 1.0	x: 0 m η = 1.0	x: 0.413 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.206 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.41 3 m η = 1.5	x: 0.206 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N59/N2	x: 0.804 m η = 1.0	x: 0 m η = 1.0	x: 0.402 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.201 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.40 2 m η = 1.5	x: 0.201 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N40/N98	x: 1.184 m η = 0.6	x: 0 m η = 0.6	x: 0.592 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.197 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.59 2 m η = 1.9	x: 0.197 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N98/N42	x: 1.163 m η = 0.5	x: 0 m η = 0.5	x: 0.581 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.194 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.58 1 m η = 1.8	x: 0.194 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N42/N100	x: 1.141 m η = 0.5	x: 0 m η = 0.5	x: 0.571 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.19 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.57 1 m η = 1.7	x: 0.19 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N100/N44	x: 1.12 m η = 0.5	x: 0 m η = 0.5	x: 0.56 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.187 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.56 m η = 1.7	x: 0.187 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N44/N102	x: 1.099 m η = 0.5	x: 0 m η = 0.5	x: 0.55 m η = 0.5	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.183 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.55 m η = 1.7	x: 0.183 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N102/N46	x: 1.078 m η = 0.5	x: 0 m η = 0.5	x: 0.539 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.18 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.53 9 m η = 1.6	x: 0.18 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N46/N104	x: 1.057 m η = 0.5	x: 0 m η = 0.6	x: 0.529 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.176 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.52 9 m η = 1.6	x: 0.176 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N104/N48	x: 1.037 m η = 0.6	x: 0 m η = 0.6	x: 0.518 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.173 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.51 8 m η = 1.5	x: 0.173 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		
N48/N106	x: 1.016 m η = 0.6	x: 0 m η = 0.6	x: 0.508 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.169 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.50 8 m η = 1.5	x: 0.169 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>		

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>	
N106/N50	x: 0.996 m η = 0.6	x: 0 m η = 0.6	x: 0.498 m η = 0.4	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η = 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.249 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.49 8 m η = 1.5	x: 0.249 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N50/N108	x: 0.976 m η = 0.6	x: 0 m η = 0.7	x: 0.488 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.244 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.48 8 m η = 1.5	x: 0.244 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N108/N52	x: 0.956 m η = 0.7	x: 0 m η = 0.7	x: 0.478 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.239 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.47 8 m η = 1.5	x: 0.239 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N52/N110	x: 0.937 m η = 0.7	x: 0 m η = 0.7	x: 0.468 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.234 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.46 8 m η = 1.5	x: 0.234 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N110/N54	x: 0.917 m η = 0.7	x: 0 m η = 0.7	x: 0.459 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.229 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.45 9 m η = 1.4	x: 0.229 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N54/N112	x: 0.898 m η = 0.7	x: 0 m η = 0.8	x: 0.449 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.225 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 9 m η = 1.4	x: 0.225 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N112/N56	x: 0.879 m η = 0.8	x: 0 m η = 0.8	x: 0.44 m η = 0.3	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.22 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.44 m η = 1.4	x: 0.22 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N56/N114	x: 0.861 m η = 0.9	x: 0 m η = 0.9	x: 0.431 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.215 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.43 1 m η = 1.5	x: 0.215 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N114/N58	x: 0.843 m η = 0.9	x: 0 m η = 0.9	x: 0.421 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.211 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.42 1 m η = 1.5	x: 0.211 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N58/N116	x: 0.825 m η = 1.0	x: 0 m η = 1.0	x: 0.413 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.206 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.41 3 m η = 1.5	x: 0.206 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N116/N1	x: 0.804 m η = 1.0	x: 0 m η = 1.0	x: 0.402 m η = 0.2	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(1)</sup>	x: 0 m η < 0.1	V <sub>Ed</sub> = 0.00 D.N.P. <sup>(2)</sup>	x: 0.201 m η < 0.1	D.N.P. <sup>(3)</sup>	x: 0.40 2 m η = 1.4	x: 0.201 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N55/N56	x: 0.58 m η = 5.1	x: 0 m η = 5.8	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N56/N57	x: 0.58 m η = 4.9	x: 0 m η = 5.5	x: 0.58 m η = 0.4	x: 0 m η = 0.4	x: 0 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N57/N58	x: 0.58 m η = 4.6	x: 0 m η = 5.2	x: 0 m η = 0.4	x: 0.58 m η = 0.4	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.8	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N58/N59	x: 0.58 m η = 4.4	x: 0 m η = 4.9	x: 0 m η = 0.4	x: 0.58 m η = 0.6	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	
N59/N1	x: 0.575 m η = 4.1	x: 0 m η = 4.5	x: 0 m η = 0.3	x: 0 m η = 0.6	x: 0 m η = 0.1	η = 0.1	η < 0.1	η < 0.1	x: 0.57 5 m η = 5.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	



Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> V <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>	
N74/N75	x: 0.58 m η = 5.0	x: 0 m η = 5.8	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.4	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N75/N76	x: 0.58 m η = 4.8	x: 0 m η = 5.5	x: 0.58 m η = 0.4	x: 0 m η = 0.4	x: 0 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N76/N77	x: 0.58 m η = 4.6	x: 0 m η = 5.2	x: 0 m η = 0.4	x: 0.58 m η = 0.4	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.9	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N77/N78	x: 0.58 m η = 4.3	x: 0 m η = 4.9	x: 0 m η = 0.4	x: 0.58 m η = 0.6	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N78/N2	x: 0.575 m η = 4.0	x: 0 m η = 4.5	x: 0.575 m η = 0.5	x: 0 m η = 0.6	x: 0 m η = 0.1	η = 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.57 5 m η = 5.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N93/N94	x: 0.58 m η = 5.1	x: 0 m η = 5.8	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N94/N95	x: 0.58 m η = 4.9	x: 0 m η = 5.5	x: 0.58 m η = 0.4	x: 0 m η = 0.4	x: 0 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.1	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N95/N96	x: 0.58 m η = 4.6	x: 0 m η = 5.2	x: 0 m η = 0.4	x: 0.58 m η = 0.4	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.8	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N96/N97	x: 0.58 m η = 4.4	x: 0 m η = 4.9	x: 0.58 m η = 0.4	x: 0.58 m η = 0.5	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.3	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N97/N4	x: 0.575 m η = 4.1	x: 0 m η = 4.5	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0 m η = 0.1	η = 0.1	η < 0.1	x: 0 m η < 0.1	η < 0.1	x: 0.57 5 m η = 5.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N112/N113	x: 0.58 m η = 5.1	x: 0 m η = 5.7	x: 0 m η = 0.4	x: 0 m η = 0.5	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N113/N114	x: 0.58 m η = 4.9	x: 0 m η = 5.4	x: 0.58 m η = 0.4	x: 0 m η = 0.4	x: 0 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0.58 m η = 6.0	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N114/N115	x: 0.58 m η = 4.7	x: 0 m η = 5.1	x: 0 m η = 0.4	x: 0.58 m η = 0.4	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.7	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N115/N116	x: 0.58 m η = 4.4	x: 0 m η = 4.8	x: 0.58 m η = 0.4	x: 0.58 m η = 0.6	x: 0.58 m η < 0.1	η < 0.1	η < 0.1	η < 0.1	η < 0.1	x: 0 m η = 5.2	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N116/N3	x: 0.575 m η = 4.1	x: 0 m η = 4.4	x: 0.575 m η = 0.5	x: 0 m η = 0.6	x: 0 m η = 0.1	η = 0.1	η < 0.1	x: 0 m η < 0.1	η < 0.1	x: 0.57 5 m η = 5.4	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N5/N117	η = 1.2	η = 1.2	x: 0 m η = 1.0	x: 0.389 m η = 0.5	x: 0 m η = 0.1	η < 0.1	x: 0 m η < 0.1	x: 0.389 m η < 0.1	x: 0 m η = 2.1	x: 0 m η < 0.1	x: 0 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N117/N8	η = 1.2	η = 1.2	x: 0 m η = 0.2	x: 0 m η = 0.9	x: 0.389 m η < 0.1	η < 0.1	x: 0 m η < 0.1	x: 0 m η < 0.1	x: 0 m η = 2.0	x: 0 m η = 2.0	x: 0 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>
N7/N117	η = 1.2	η = 1.2	x: 0.389 m η = 0.2	x: 0.389 m η = 0.9	x: 0 m η < 0.1	η < 0.1	x: 0.194 m η < 0.1	x: 0.389 m η < 0.1	x: 0.38 9 m η = 2.4	x: 0.194 m η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)													Status
	N <sub>t</sub>	N <sub>c</sub>	M <sub>Y</sub>	M <sub>Z</sub>	V <sub>Z</sub>	V <sub>Y</sub>	M <sub>Y</sub> V <sub>Z</sub>	M <sub>Z</sub> V <sub>Y</sub>	NM <sub>Y</sub> M <sub>Z</sub>	NM <sub>Y</sub> M <sub>Z</sub> zV <sub>Y</sub> V <sub>Z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>Z</sub>	M <sub>t</sub> V <sub>Y</sub>	
N117/N6	η = 1.2	η = 1.3	x: 0.389 m η = 1.3	x: 0 m η = 0.5	x: 0.389 m η = 0.1	η < 0.1	η < 0.1	x: 0 m η < 0.1	x: 0.38 9 m η = 2.6	η < 0.1	M <sub>Ed</sub> = 0.00 D.N.P. (5)	D.N.P.(6)	D.N.P.(6)	

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	$\lambda_w$	N <sub>t</sub>	N <sub>c</sub>	M <sub>y</sub>	M <sub>z</sub>	V <sub>z</sub>	V <sub>y</sub>	M <sub>y</sub> V <sub>z</sub>	M <sub>z</sub> V <sub>y</sub>	NM <sub>y</sub> M <sub>z</sub> z	NM <sub>y</sub> M <sub>z</sub> V <sub>y</sub> V <sub>z</sub>	M <sub>t</sub>	M <sub>t</sub> V <sub>z</sub>	M <sub>t</sub> V <sub>y</sub>	
N40/N41	x: 0.29 m $\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.7$	x: 0 m $\eta = 3.6$	x: 0.58 m $\eta = 0.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.58 m $\eta = 3.7$	x: 0.29 m $\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.7$
N42/N43	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.7$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.7$
N43/N44	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.6$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.6$
N44/N45	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.5$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.5$
N45/N46	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.4$
N46/N47	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.3$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.3$
N47/N48	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.3$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.3$
N48/N49	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 3.0$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.2$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.2$
N49/N50	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 2.9$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.1$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.1$
N50/N51	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.8$	$\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.0$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.0$
N51/N52	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.7$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.9$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 2.9$
N52/N53	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.6$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.8$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 2.8$
N53/N54	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.7$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 2.7$
N54/N55	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.1$	x: 0 m $\eta = 2.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.6$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 2.6$
N38/N60	x: 0.29 m $\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.6$	x: 0.58 m $\eta = 0.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.58 m $\eta = 3.7$	x: 0.29 m $\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.7$
N61/N62	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.7$	$\eta < 0.1$	M <sub>Ed</sub> = 0.00 D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup> )	D.N.P. <sup>(6)</sup> )	VERIFIED D $\eta = 3.7$

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	$\lambda_w$	$N_t$	$N_c$	$M_y$	$M_z$	$V_z$	$V_y$	$M_y V_z$	$M_z V_y$	$N M_y M_z$	$N M_y M_z V_y$	$M_t$	$M_t V_z$	$M_t V_y$	
N62/N63	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.6$
N63/N64	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.4$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.5$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.5$
N64/N65	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.4$
N65/N66	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.4$
N66/N67	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 3.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.3$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.3$
N67/N68	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 3.0$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.2$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.2$
N68/N69	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.9$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.1$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.1$
N69/N70	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.8$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.0$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.0$
N70/N71	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.7$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.9$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.9$
N71/N72	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.6$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.8$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.8$
N72/N73	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.1$	x: 0 m $\eta = 2.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.7$
N73/N74	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.1$	x: 0 m $\eta = 2.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.6$
N37/N79	x: 0.29 m $\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.7$	x: 0 m $\eta = 3.6$	x: 0.58 m $\eta = 0.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.58 m $\eta = 3.7$	x: 0.29 m $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.7$
N80/N81	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.7$
N81/N82	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.6$
N82/N83	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.5$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.5$
N83/N84	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.4$
N84/N85	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.3$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.3$
N85/N86	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.2$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.2$
N86/N87	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 3.0$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.2$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.2$

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	$\lambda_w$	$N_t$	$N_c$	$M_y$	$M_z$	$V_z$	$V_y$	$M_y V_z$	$M_z V_y$	$N M_y M_z$	$N M_y M_z V_y$	$M_t$	$M_t V_z$	$M_t V_y$	
N87/N88	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 2.9$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.1$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.1$
N88/N89	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.8$	$\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.0$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.0$
	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.7$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.9$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.9$
N90/N91	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.6$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.8$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.8$
N91/N92	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.7$
N92/N93	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.1$	x: 0 m $\eta = 2.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.6$
N39/N98	x: 0.29 m $\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.7$	x: 0 m $\eta = 3.6$	x: 0.58 m $\eta = 0.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.29 m $\eta < 0.1$	x: 0.58 m $\eta = 3.6$	x: 0.29 m $\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.6$
	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.4$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.6$
N100/N101	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.5$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.5$
N101/N102	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.3$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.4$
N102/N103	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.2$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.4$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.4$
N103/N104	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.1$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.3$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.3$
N104/N105	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.0$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.2$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.2$
N105/N106	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.5$	x: 0 m $\eta = 3.0$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.1$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.1$
N106/N107	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 2.9$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 3.0$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 3.0$
	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.4$	x: 0 m $\eta = 2.8$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.9$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.9$
N108/N109	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.7$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.8$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.8$
N109/N110	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.3$	x: 0 m $\eta = 2.6$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.7$
N110/N111	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.2$	x: 0 m $\eta = 2.5$	x: 0.58 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.6$
N111/N112	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.1$	x: 0 m $\eta = 2.4$	x: 0 m $\eta = 0.2$	x: 0 m $\eta = 0.2$	x: 0.58 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0 m $\eta = 2.5$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	VERIFIED D $\eta = 2.5$

Bars	CHECKS (EUROCODE 3 EN 1993-1-1: 2005)														Status
	$\lambda_w$	$N_t$	$N_c$	$M_y$	$M_z$	$V_z$	$V_y$	$M_y V_z$	$M_z V_y$	$N M_y M_z$	$N M_y M_z V_y V_z$	$M_t$	$M_t V_z$	$M_t V_y$	
N98/N99	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.7$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0.58 m $\eta = 3.6$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> <b>D</b> <b><math>\eta = 3.6</math></b>
N79/N80	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0.58 m $\eta = 3.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> <b>D</b> <b><math>\eta = 3.7</math></b>
N60/N61	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.6$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0.58 m $\eta = 3.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> <b>D</b> <b><math>\eta = 3.7</math></b>
N41/N42	$\lambda_w \leq \lambda_{w,max}$ Verified	x: 0.58 m $\eta = 2.6$	x: 0 m $\eta = 3.5$	x: 0.58 m $\eta = 0.2$	x: 0.58 m $\eta = 0.3$	x: 0 m $\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	$\eta < 0.1$	x: 0.58 m $\eta = 3.7$	$\eta < 0.1$	$M_{Ed} = 0.00$ D.N.P. <sup>(5)</sup>	D.N.P. <sup>(6)</sup>	D.N.P. <sup>(6)</sup>	<b>VERIFIED</b> <b>D</b> <b><math>\eta = 3.7</math></b>

**Notation:**

$N_t$ : Resistance to axial tension  
 $N_c$ : Compression resistance  
 $M_y$ : Y - Axis bending resistance  
 $M_z$ : Z - Axis bending resistance  
 $V_z$ : Resistance to shear in the Z direction  
 $V_y$ : Resistance to shear in the Y direction  
 $M_y V_z$ : Combined bending moment Y and shear force Z resistance  
 $M_z V_y$ : Combined bending moment Z and shear force Y resistance  
 $N M_y M_z$ : Combined bending and axial resistance  
 $N M_y M_z V_y V_z$ : Combined bending, axial and shear resistance  
 $M_t$ : Torsional resistance  
 $M_t V_z$ : Combined Z shear and torsional resistance  
 $M_t V_y$ : Combined Y shear and torsional resistance  
 $x$ : Distance to the origin of the bar  
 $\eta$ : Usage coefficient (%)  
D.N.P.: Not applicable  
 $\lambda_w$ : Crushing of the web induced by the compressed flange

**Checks that do not proceed (D.N.P.):**

- <sup>(1)</sup> The check does not proceed, as there is no bending moment.  
<sup>(2)</sup> The check does not proceed, as there is no shear force.  
<sup>(3)</sup> The check does not proceed, as there is no interaction between shear forces and bending moments for any loadcase combination.  
<sup>(4)</sup> There is no interaction between the bending moment, axial force and shear for any combination. Therefore, the check does not proceed.  
<sup>(5)</sup> The check does not proceed, as there is no torsional moment.  
<sup>(6)</sup> There is no interaction between torsional moment and shear force for any combination. Therefore the check does not proceed.

